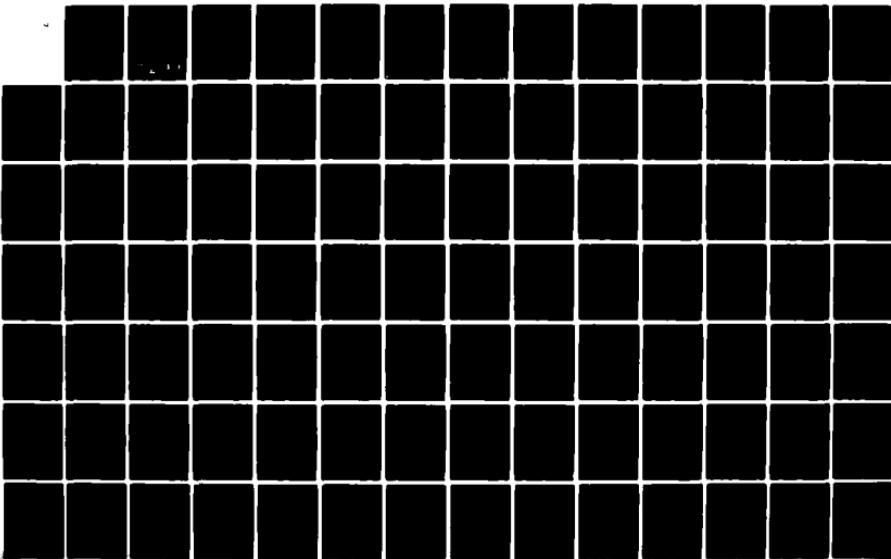


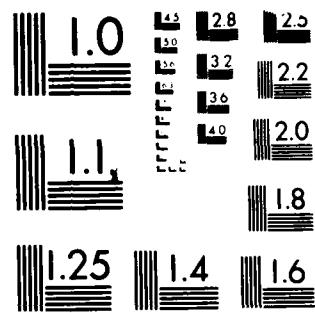
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Goddard Space Flight Center,
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ORBITAL RADIATION STUDY FOR INCLINED CIRCULAR TRAJECTORIES

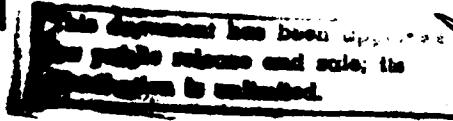
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Orbital Radiation Study for Inclined
Circular Trajectories

E. G. Stassinopoulos

NASA-Goddard Space Flight Center
Sciences Directorate
National Space Science Data Center



November 1981

Goddard Space Flight Center
Greenbelt, Maryland 20771

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1. Introduction

At the request of and with support from the Naval Research Laboratory*, a comprehensive study was conducted to determine the space radiation environment of a series of high inclination geocentric orbits for a mission duration of five years.

>Following the precedent established with previous studies, the external (surface incident) charged particle radiation, predicted for the satellite was determined by orbital flux integration for six independent trajectories, (see section 3). The latest standard models of the environment were used in the calculations, (see section 5).

< Magnetic field definitions for the six nominal circular trajectories were obtained from a current field model, (see section 3).

Spatial and temporal variations or conditions affecting the static environment models were considered and accounted for, wherever possible.

> Finally, limited shielding and dose evaluations were performed for simple infinite slab and spherical geometries.

Results, given in graphical and tabular form, are analyzed, explained, and discussed. Conclusions are presented and commented on.

2. SPECIFICATION OF ORBITS

The analysis was based on nominal circular orbits with inclination of 60 degrees and altitudes of 1667, 2593, 3889, 5186, 6389, and 10371 kilometers.

3. GENERATION OF TRAJECTORIES

Six separate flight path ephemerides were generated for the specified orbits with the GEODYN-BILCONV System¹ for trajectories of 24-hour duration defined at 1-minute intervals. The length of simulated orbit time and the integration stepsize were especially selected so as to provide sufficient point density to insure an adequate sampling of the ambient radiation environment when flying the trajectories through the models. The trajectories were subsequently converted from geodetic polar to magnetic B-L coordinates with McIlwain's INVAR program of 1965² and the field routine ALLMAG,³ which now utilizes the BARRACLOUGH 1975 field model.⁴ The field computations were extrapolated to the tentative mission epoch of 1989.5 with linear time terms representing secular variations of the field.

4. FLIGHT PATH EXPOSURE TO TRAPPING DOMAINS

The specified nominal flight-path configurations display a significant characteristic of high inclination orbits in magnetic L-space: they traverse almost the entire terrestrial radiation belt twice during each revolution, moving back and forth through regions of low L values (the inner zone: $1.0 < L \leq 2.8$), regions of high L values (the outer zone: $2.8 < L < 12$), and

*This work funded by the Naval Electronics Systems Command under the NRL Nuclear Survivability/Vulnerability Program.

regions outside the trapping domain (external). Occasionally, some revolutions will also enter regions of space where no particle trapping can occur because of atmospheric cut-off conditions; that is, trajectory segments may have a combination of magnetic B and L values that place them outside the atmospheric cut-off limits of the models.

These excursions and the "external" visitations afford the satellite an amount of flux-free time, which may be of substantial duration (see section 11, C).

5. TRAPPED PARTICLE ENVIRONMENT MODELS

The fluxes in this study were obtained from current NSSDC models: the solar maximum AE6 for the inner zone electrons⁵, the new interim model AEI7 for the outer zone electrons⁶, and the solar maximum version of the new AP8 model⁷ for energetic trapped protons. It should be noted that the interim AEI7 does not reflect solar cycle variations in its present state. However, this model was issued in two versions, the AEI7-HI and the AEI7-LO, in order to account for differences in the data sets used in their construction. The LO version was used in this effort. All models describe an average static environment at a given epoch.

6. ORBITAL FLUX INTEGRATIONS

Orbital flux integrations were performed with the UNIFLUX⁸ and the SOFIP⁹ systems. UNIFLUX provides L-band distributions and exposure times with B-L bin breakdown, while SOFIP provides the dose and shield data.

7. GEOMAGNETIC SHIELDING AND SOLAR FLARE PROTONS

Low altitude high inclination orbits experience a significant amount of geomagnetic shielding from cosmic rays of solar or galactic origin in the energy range $E > 10$ MeV. Therefore, it may be assumed that the spacecraft will only intermittently be exposed to the unattenuated interplanetary solar flare proton intensities of all energies above 10 MeV. To a first approximation, the fluxes may also be considered omnidirectional and isotropic, probably to within 10-15%.

Usually, geomagnetic shielding effects on geocentric missions are being evaluated with simple rigidity considerations because of substantial diurnal variations in the cutoff latitude associated with geomagnetic tail effects (2-4 degrees) and storm-induced changes (> 4 degrees). The simple analysis used here assumed that energetic solar protons of all energies above 10 MeV have free access to all magnetospheric regions external to a dipole shell of $L=5$ earth radii, which is equivalent to a cut-off latitude of about 63 degrees.

Predictions of solar flare proton fluxes at 1 AU are obtained as a function of mission duration τ and confidence level Q^* on the basis of a probabilistic analysis¹⁰ using a modified type of Poisson statistics by a computerized model SOLPRO¹¹ that includes the distinction between "ordinary" (OR) and

* Q denotes the degree of confidence one wishes to assign to the results, namely that for the specified mission duration the calculated fluences are the smallest values which will not be exceeded by actually encountered intensities.

"anomalously large" (AL) events and the probability of occurrence of the latter. Both AL- and OR- event fluences are non-linear functions of Q and τ . For these predictions, only high quality comprehensive satellite measurements (not ground observations) are being used, covering almost the entire 20th solar cycle. There have been indications that descriptions of the solar flare environment in interplanetary space (at 1 AU), derived from interpretations and extrapolations of ground based measurements, have not been very accurate.

It should be noted that the statistics cannot predict when an AL event will occur; only the probability that one will occur in a given length of time. And it must be remembered that a single AL event will impart its total fluence within two to four days.

This implies that for unmanned satellites with mission durations of $\tau \geq 1$ year, OR-event fluences are not significant because probabilistic theory predicts the possible occurrence of at least one AL event, even for the lowest allowable confidence level ($Q=80\%$).

8. FLUX DATA: TYPE, QUALITY, AND VARIATIONS

The trapped particle flux data available from the models represent omnidirectional, integral intensities that one would expect to obtain as average values over periods in excess of six months. But over most regions of magnetospheric space ($L \geq 2$ earth radii), short term excursions can vary from these values by factors of 10^2 to 10^3 , depending on the particle energies and on the type and intensity of the causative event. These variations do affect the investigated missions because their trajectories enter regions of space where L is greater than 2 earth radii. Also, trapped particle populations experience changes due to: (a) local time (LT) dependence, and (b) solar cycle dependence. Both are of some consequence to these missions. The former is significant for spacecraft that sample regions of $L > 5$ earth radii, which are visited by the specified missions. To compensate for these variations, the model provides LT-averaged values, which should yield an adequate approximation for missions of long duration ($\tau > 1$ year). The solar cycle variations have been taken into account by selecting the appropriate models for each period, where available.

Generally, solar cycle variations have opposite effects on each particle species:

	<u>Solar Min</u>	<u>Solar Max</u>
Electrons	lower	higher
Protons	higher	lower

The solar cycle changes, as derived from a comparison of the corresponding models, are functions of energy E and magnetic parameter L . For the inner zone electrons, they may range from a factor of 1 to a factor of 5.

Protons are only affected in the vicinity of the atmospheric cutoff regions. No changes of consequence have been observed in the heart of the proton trapping domain. Proton changes have about the same range as those of the electrons.

It is necessary to emphasize that the calculations, although based on the best data available for the past epochs, can only serve as approximations for the future.

It also should be noted that a basic uncertainty factor of 2 is defined for the flux values of the AP8 and the AE5 models, while the AE6 is characterized by an average uncertainty factor of 5. No uncertainty factor has yet been defined for the interim AEI7.

9. DOSE AND SHIELDING EVALUATION

Doses were calculated from the total orbit integrated, surface incident, omnidirectional, integral fluences by existing shielding codes¹², as functions of various aluminum shield thicknesses and geometries.

A simple procedure was followed, not involving solid angle sectoring or three-dimensional ray tracing considerations. Instead, a simple two-dimensional geometry with a cosine law for the incident spectra, and a three-dimensional spherical geometry were considered. (See comment in section 11D-III)

Bremsstrahlung calculations were performed with the same codes.

10. RESULTS: PRESENTATION DESCRIPTION

This section describes the form and format in which the results, derived from the Orbital Flux Integration (OFI) process, are presented for practical use. Except where otherwise specified, all particle data in this report relate to integral, omnidirectional fluxes or fluences.

A. Tabular Presentations

The outcome of all calculations is summarized in Tables 1 to 60. The tables are arranged in six sets, where every set pertains to one specific type of data. The first two sets have two similar members for every trajectory considered in the study: one for trapped protons and one for electrons, in that order. The next three sets contain only one member for each trajectory. The sixth set contains three similar members for each trajectory. A more detailed description of the tables is provided in the following paragraphs.

I. L-band Tabulations: Tables 1-12

Tabulation of total orbit-integrated fluence distributions by L-bands for selected energy thresholds, in units of particles per square centimeter, normalized to 5 MeV and .5 MeV for protons and electrons, respectively.

The tables contain 48 L-bands of equal size covering the range from L=1.0 to L > 10.4 earth radii in constant increments of .2 earth radii.

II. Spectral Profiles: Tables 13-24

Tabulation of average orbit-integrated spectral distributions. Composite spectra are given in units of: fluxes per square centimeter per second, fluxes per square centimeter per day, and total fluences per specified mission duration (5 years). For the electrons, the latter are also given in terms of

inner and outer zone contributions. Functionally derived differential fluxes are listed in the last columns for both species of particles.

Total orbit-integrated spectra in percent, for energy intervals ΔE corresponding to the energy levels of the L-band tables, are also given in terms of average instantaneous and daily intensities.

An exposure index (for the normalization energies used in the L-band tables) is listed for nine successive intensity ranges varying by one order of magnitude, in terms of processed exposure duration (in hours) and total number of particles accumulated while in that intensity range for the indicated number of hours.

III. Peaks and Totals Per Orbit: Tables 25-30

These tables contain the absolute instantaneous peak fluxes and the total fluences accumulated during each successive revolution, as obtained from the nominal trajectories for the investigated flight duration (24 hours of mission time).

Specifically, there are nine columns on these tables. Column 1 is an orbit counting device, based on:

- a) the orbit period when the trajectory is circular and lies in the equatorial plane;
- b) the physical perigee in all elliptical flight-path cases; and,
- c) the equatorial crossing for circular inclined trajectories.

Column 2 gives the peak flux. Columns 3, 4 and 5 indicate the spacecraft position in geocentric coordinates at which the predicted peak flux was encountered. Columns 6, 7 and 8 determine respectively the relative orbit time and the magnetic B-L coordinates for this event. For the purpose of orbital radiation studies, all simulated trajectories start at $t_0 = \text{hours}$. Finally, the last column indicates the total predicted flux to be encountered during that particular orbit. It is advisable to disregard the last line on this table because many times that orbit is incomplete and the fluxes or positions shown do not correspond to true peaks.

IV. Time-Accounting and Exposure-Analysis: Tables 31-36

The "EXPOSURE-ANALYSIS" summary indicates what percent of its total lifetime T the satellite spends in "flux-free" regions of space, what percent of its total lifetime it spends in high intensity proton and electron domains, and while so exposed, what percent of its total flux it accumulates.

In the context of this study, the term "flux-free" applies to all regions of space where trapped particle fluxes are less than one proton or electron per square centimeter per second, having energies $E > 5 \text{ MeV}$, and $E > .5 \text{ MeV}$, respectively. By definition, this includes all regions external to the Van Allen radiation belts.

The concept of "trapped particle fluxes" is meant to include stably trapped, pseudo trapped, and transient fluxes, as long as they are part of or contained in the environment models used and, in the case of transients or pseudos, their sources are considered powerful enough to supply them continuously in substantial numbers.

Similarly, as "high intensity" are defined those regions of space where the instantaneous, integral, omnidirectional, trapped-particle flux is greater than 10^3 protons with energies $E > 5$ MeV, and greater than 10^5 electrons with energies $E > 5$ MeV.

The values given in these tables are statistical averages, obtained over extended intervals of mission time. However, they may vary significantly from one orbit to the next, when individual revolutions are considered.

The "TIME-ACCOUNT" breakdown shows what percent of its total time the satellite spends in the "inner zone" ($1.0 \leq L < 2.8$) and in the "outer zone" ($2.8 \leq L \leq 11.0$) electron trapping domains, and also the percent of time spent in regions external to the latter ($L > 11.0$).

It should be noted that the confinement of the outer zone within the boundary of the $L=11.0$ earth radii volume is arbitrary and has no physical meaning. It is intended only as a simplification to facilitate the calculations. The region considered "external" in this study ($L > 11.0$) is still partially a domain of the outer zone, at least as far out as $L=12.0$ earth radii, according to the current environment models.

A last item on this table: the inner zone time is further subdivided into two parts: the percentage of time spent outside ($L < 1.1$) and inside ($1.1 \leq L < 2.8$) the trapping domain.

V. Solar Proton Fluences and Exposure Factor: Tables 37-42

For the specified mission duration τ (printed in the sub-title), and dipole cut-off shell ($L=5$ earth radii, shown in the header), this table lists the solar proton fluence-spectra (in units of particles per square centimeter) at five discrete confidence levels Q (given at the top of each column).

The exposure factors (in percent of total mission duration) obtained from the geomagnetic shielding analysis are also listed for four dipole cut-off shell values (in earth radii).

VI. Total Dose and Components: Tables 43-60

These tables list doses in units of rads_{AL} as a function of aluminum shield thickness, given in three ways: range s in grams per square centimeter, depth t in millimeters, and depth \underline{t} in mils.

Electron, bremsstrahlung, and proton contributions to the overall sumtotal dose are given separately. Electron and proton doses are further broken down into their respective constituents; namely, inner zone and outer zone for the former, trapped and solar flare for the latter.

The specific mission duration for which the doses have been calculated is indicated in the table headline.

Caution: the AL-event solar flare protons are not contributed gradually over the investigated mission duration ($\tau = 5$ years) but are imparted in toto in a relatively short burst, that is, within approximately 2-4 days per AL event.

B. Graphical Presentation

Some of the tabulated data are also plotted in Figures 1 to 36, and 49 to 102 with additional Figures 37 to 48 containing plots of flight path data. Positional flux and dose data are plotted in Figures 103-162. As with the tables, the computer plots are arranged in eight sets, where again each set pertains to one specific type of data. The first three sets have two similar members for each trajectory investigated: one for each particle species. The next two sets (fourth and fifth) contain one member for each trajectory considered. The sixth set contains nine similar members for each trajectory, providing three graphs (for respective depth ranges) for each of three geometries. The seventh set contains two similar members for each trajectory: one for each particle species. Finally, the last set has eight members for each trajectory.

I. Time and Flux Histograms: Figures 1-12

These plots show two curves superimposed on the same graph; namely, one each for the variables "time" and "flux". Both are given on a semi-log scale as functions of the parameter L (earth radii), within the range $1 < L \leq 10$, and for constant L-bands of .1 earth radius width. The plots are plotted:

- a) by a plain curve, the characteristic trajectory intensities as obtained from the orbital integration process in terms of averaged integral particle fluxes above a given energy.
- b) by a contour marked with symbols, the percent total lifetime (%T) spent in each L interval.

The logarithmic ordinate relates to the time-flux variables. The printed numbers are powers of 10 and pertain to the fluxes; the scale values for the time curves are given in the upper part of the ordinate label: from 10^{-3} to 10^2 percent of T, the type of particles, their integral energy, and the units, are all given in the lower part of the label. The label on the top of the graph identifies the trajectory.

II. Spectral Profiles: Figures 13-24

A graphical presentation of the final composite spectral distribution, obtained from the orbital integration process. The plots are semi-log graphs, where the abscissa is a linear energy scale for integral particle energies E, in MeV, and the ordinate is a logarithmic scale for the fluxes, given in daily averages for energies greater than E; the printed scale values are powers of 10.

III. Peaks Per Orbit: Figures 25-36

Here the absolute peak intensities, encountered per period (1 period = 1 revolution = 1 orbit), are plotted for the duration of the flight-time processed in the analysis. The logarithmic ordinate, with scale values in powers of 10, relates to instantaneous particle fluxes of the environment at the indicated energy thresholds, while the abscissa is a linear orbit enumeration.

IV. Trajectory World Map Projections: Figures 37-42

These graphs depict the surface trace of the geocentrically projected subsatellite positions. The trajectories are plotted for several revolutions on a global map produced by a Miller Cylindrical Projection method. The contours of the continents have been omitted for clarity. The positions of equatorial crossing, of physical perigee, or of period commencement are indicated by numbers identifying the orbits shown in the graphs. For all trajectories, the distance between successive sequential numbers is a measure of the orbit precession.

V. Flight Path Tracing in B-L Space: Figures 43-48

Plots showing trajectory traces in B-L space on a semi-log scale. Several orbits are depicted, each identified by its sequential number. The magnetic equator is entered on all plots. The logarithmic ordinate relates to the field strength B in gauss; the printed values are exponents of 10. L is given in earth radii on the linear abscissa.

VI. Dose-Depth Curves by Geometry: Figures 49-102

Plots of final depth-dose values for the indicated mission duration. Normally, these plots show composite curves for bremsstrahlung, combined electrons (inner and outer zone), combined protons (trapped and solar flare), and sumtotal of all contributions. In the present case, the respective contours consist of inner and outer zone electrons separately and of trapped and solar flare protons, separately, of composite bremsstrahlung, and the sumtotal.

For ease of use and in order to provide a greater resolution at the more sensitive range of depths (namely the thinner shields) three plots have been generated per processed trajectory, for shield-ranges and subdivisions increasing by one order of magnitude.

The logarithmic ordinate, with scale values in powers of 10, relates to aluminum dose in units of rads. The linear abscissa is the shield thickness, given in three different units: range s in grams per square centimeter, depth t in millimeters, depth t in mils.

VII. Positional Flux Plots: Figures 103-114

Plots of instantaneous omnidirectional trapped particle fluxes (electrons and protons) at (up to 10) specified threshold energy levels (>MeV), for a selected orbit (usually worst case revolution through heart of SAA).

The logarithmic ordinate, with scale values in powers of 10, relates to the number of particles per square centimeter per second. The linear abscissa is the relative time, in minutes or hours, from the beginning of the selected orbital pass.

VIII. Positional Dose Plots: Figures 115-162

Plots of instantaneous omnidirectional trapped particle dose values at (up to 10) specified shield thicknesses (omnidirectional isotropic incidence, cosine-theta distribution) for a selected orbit (usually worst case revolution through heart of SAA). Separate plots are generated (if present) for: electron dose (including bremsstrahlung), proton dose, and total dose (no solar proton contributions are included) for dose at transmission surface of aluminum slab shields, dose in semi-infinite aluminum medium, and dose at center of aluminum spheres.

The logarithmic ordinate, with scale values in powers of 10, relates to the respective dose in units of rads-aluminum. The linear abscissa is the relative time, in minutes or hours, from the beginning of the selected orbital pass.

11. RESULTS: ANALYSIS AND DISCUSSION

In this section, some of the presented tabular or graphical study-results are discussed, with occasional comments as to their use, limits, and applications.

A. Spectral Profiles

Characteristic features of the near earth radiation environment are strong altitude and inclination dependencies. However, at high inclination values ($30^\circ < i < 90^\circ$) small changes in inclination will not produce changes in flux levels and spectral distributions as significant as those produced by small changes in altitude. The greatest inclination dependent variations occur in the range $0^\circ \leq i \leq 30^\circ$.

I. Protons: The protons exhibit relatively hard, almost uniform spectra in the investigated inclination-altitude regime.

It should be noted that a characteristic softening of the high energy tail of the spectrum appears at the 6389 km altitude orbit, near $E > 400$ MeV, as a consequence of the limit of the volume of space occupied by these particles. The extent of the proton trapping domain along the magnetic equator is inversely related to their energy. This is strikingly demonstrated by the spectrum of the 10371 km altitude orbit, which falls off sharply at about $E > 100$ MeV and which indicates that according to the standard model there are no protons with energies $E > 150$ MeV contained in the region of space sampled by this trajectory.

II. Electrons: The electrons show complex variable spectra. Inner zone and outer zone average, orbit-integrated, composite intensities rise non-uniformly with altitude, particularly at energies above 3.75 MeV with differences reaching up to several orders of magnitude at $E > 6$ MeV. Spectra extend to higher energies as height increases.

The inner zone spectra fall rapidly off to zero flux in the energy range from 4 to 5 MeV and they are therefore more benign than their harder outer-zone counterparts, which extend to energies of about 7 MeV.

At low altitudes (1667 abd 2593 km), the inner zone contributions prevail up to about $E > 2.75$ MeV, but for all energies $E > 2$ MeV the inner zone spectra are always softer than the outer zone spectra (in agreement with the models).

However, at high altitudes (e.g. the 10371 km orbit), the inner zone contributions become insignificant even at low energies ($.1 < E(\text{MeV}) < .7$).

B. Peaks Per Orbit

The absolute peaks per revolution have been obtained for standard processing energies: $E > 5$ MeV for protons and $E > .5$ MeV for electrons. Other energy selections produce different peak curves in an inverse relationship: lower energies yield higher and more expanded contours, and vice versa.

Peak contours of inclined circular trajectories display amplitude variations and sometimes discontinuities (flux-free time) that follow periodic patterns based on the daily cycle of revolutions. For fixed energies, amplitudes and discontinuities are function of: (a) inclination i , and (b) altitude h .

Variations in either i or h may produce significant changes in the amplitude of the peak curves and in the duration of the discontinuities: up to several orders of magnitude for the former, and completely eliminating the latter.

For the investigated trajectories at the given, fixed, inclination ($i = 60^\circ$), the following observations can be made:

a) protons: at the processed energy of $E > 5$ MeV only small variations are obtained for the low altitude orbits at 1667 and 2593 km; the difference between maximum and minimum peak intensity predicted is about a factor of 6 at 13, respectively. These differences disappear at higher altitudes, while at the same time the peak flux levels rise by about two orders of magnitude, from $\sim 7 \times 10^4$ particles per square centimeter at 1667 km to $\sim 7 \times 10^6$ particles per square centimeter at 5186 km.

b) electrons: at the processed energy of $E > .5$ MeV the electron peaks appear very similar to those of the protons, as described in the previous paragraph. But the electron peak fluxes start at higher levels and reach an upper limit at the same altitude as the protons only with smaller differences: from $\sim 3 \times 10^6$ particles per square centimeter at 1667 km to $\sim 1 \times 10^7$ particles per square centimeter at 5186 km.

C. Flux-Free Time

Some comments on this topic have been provided in the previous section and in section 10/IV. Here a more detailed discussion will be given.

Flux-free time (FFT) intervals are an important feature of certain orbital configurations. They may occur over short orbit segments (partial FFT per period) or over the entire length of a revolution (total FFT per period). In terms of geomagnetic geometry, the FFTs establish the duration for which the trajectory lies outside the trapping domain of the corresponding particle species, evaluated at the given energies. Or conversely, they are a measure of the degree to which the trajectory is exposed to the charged particle trapping domains.

The number of consecutive flux-free orbits of circular trajectories is primarily a function of altitude and inclination and to a lesser degree a function of particle energy. Of the investigated flight paths, and for the selected energies (electrons: $E > .5$ MeV, protons: $E > 5.$ MeV), none shows any completely flux-free revolutions per day. The total FFT, which derives completely from partially exposed revolutions (see "Exposure Analysis," Tables #31 to 36), in percent of total mission duration, can be summarized as follows:

<u>Altitude</u> (km)	<u>Protons</u> ($E > 5.$ MeV)	<u>Electrons</u> ($E > .5$ MeV)
1667	22%	2%
2593	24%	3%
3889	30%	4%
5186	35%	6%
6389	39%	7%
10371	51%	11%

Higher energies will yield longer FFTs because the more energetic particles occupy a smaller volume of space.

D. Dose and Shielding

The calculated doses display features characteristic of the terrestrial radiation environment: at medium-to-high shield thicknesses, small contributions from relatively benign and low intensity electron spectra combined with major contributions from comparatively hard and intense proton spectra; at thin shield thicknesses the electrons predominate.

Depending on altitude, the proton doses prevail for shield thicknesses from greater than 16 to greater than 200 mils of aluminum. At high altitudes (e.g. 10371 km orbit) the opposite is true: protons are the major dose contributors only for shield thicknesses of less than 5 mils of aluminum.

Significant, however, is the fact that for aluminum the proton dose is only a weak function of shield thickness, as it shows very little attenuation over the evaluated depth range. Thus, in order to get an appreciable reduction in the dose, say by one order of magnitude, a 20-fold increase in shield thickness is necessary. The same is true for the bremsstrahlung dose. However, at low altitudes, in comparison to the proton contributions, the bremsstrahlung dose is so small (about 2 orders of magnitude lower) that it may be disregarded.

I. Decay and Degradation

The total doses obtained for each of the six investigated trajectories for the five year mission duration are substantial. In terms of electronics decay or materials degradation, the doses to be experienced on this mission inside the satellite, that is, behind a skin of about 80 mils of equivalent aluminum, are severe even for insensitive components or equipment:

<u>Altitudes (km)</u>	<u>Spherical Dose</u>
1667	~294K rads
2593	~1093K rads
3889	~1558K rads
5186	~1266K rads
6389	~1099K rads
10371	~1682K rads

II. Contamination and Interference

It should be remembered, that the direct or indirect effects of the radiation environment may also be a nuisance in terms of instrument interference or measurement contamination. If such is the case, some remedies may be available.

III. Possible Improvements

In the event that the magnitude of total dose or degree of radiation penetration behind the skin of the satellite is of importance to the mission, four possibilities exist to reduce the radiation effects on instrument and components:

- a) build or design an instrument less sensitive to radiation and construct the on-board and/or on-ground data processing software to remove or suppress radiation-induced noise
 - b) change the orbit by any combination of the elements eccentricity, altitude, and inclination so as to achieve a more benign environment
 - c) change the mission epoch: solar max for reduced proton intensities, solar min for reduced electron intensities
 - d) provide increased shielding either by geometry or by weight or by a combination of both;
- by geometry: perform a 3-D analysis (solid angle sectoring) and rearrange other equipment on board the satellite in order to provide maximum protection to sensitive part over greatest possible fraction of solid angle.*
- by weight: place additional shields around sensitive part as needed. Clearly options (a), (b), and (d) are most readily accessible.

*A powerful computer package for complex radiation shielding and transport calculations is now operational at GSFC. It is capable of addressing such topics as: (a) material mixtures, cross sections for protons, electrons, heavy charge particles, and neutrons, including source spectra and response functions; (b) source geometry, detector geometry, surfaces, rays, bodies, regions, body intersections, body unions, simple meshes, design bodies, spacecraft rays, with diverse features such as combinatorial options, translate-rotate-replicate capabilities, etc.; (c) heavy charged particle applications-1D transport by numerical integration, small volume pulse height (soft errors), 3D ray trace sectoring, 3D adjoint Monte Carlo; (d) electron bremsstrahlung-1D transport by numerical integration and by adjoint Monte

Carlo, small volume pulse height, 3D ray trace sectoring, 3D forward and adjoint Monte Carlo, energy deposition, charging distributions.

References

1. Stassinopoulos, E. G., K. A. Maale, and J. J. Hebert, "Trajectory Computations with the NSSDC Version of GEODYN and BLCONV Programs", NSSDC 73-15, National Space Science Data Center, Greenbelt, Maryland, December 1973.
2. Hassit, A., and C. C. McIlwain, "Computer Programs for the Computation of B and L (May 1966)", Data User's Note NSSDC 67-27, National Space Science Data Center, Greenbelt, Maryland, March 1967.
3. Stassinopoulos, E. G., and G. D. Mead, "ALLMAG, GDALMG, LINTRA: Computer Programs for Geomagnetic Field and Field-Line Calculations", NSSDC 72-12, National Space Science Data Center, Greenbelt, Maryland, February 1972.
4. Barraclough, D. R., T. M. Harwood, B. R. Leaton and S. R. C. Malin, "A Model of the Geomagnetic Field at Epoch 1975", Geophys. R. Roy. Ast. Soc. 43, 645-659, 1975.
5. Teague, M. J., K. W. Chan, and J. I. Vette, "AE6: A Model Environment for Trapped Electrons for Solar Maximum", NSSDC/WDC-A-R&S 76-04, National Space Science Data Center, Greenbelt, Maryland, March 1976.
6. Hills, H. K., Chan, K. W., Teague, M. J., and J. I. Vette, to be published, 1981.
7. Sawyer, D. M., and J. I. Vette, "AP8 Trapped Proton Environment for Solar Maximum and Solar Minimum", NSSDC 76-06, National Space Data Center, Greenbelt, Maryland, December 1976.
8. Stassinopoulos, E. G., and C. Z. Gregory, "UNIFLUX: A Unified Orbital Flux Integration and Analysis System", to be published in 1981.
9. Stassinopoulos, E. G., J. J. Hebert, and E. L. Butler, "SOFIP: A Short Orbital Flux Integration Program", NASA-GSFC Report X-601-77-114, May 1977.
10. King, J. H., "Solar Proton Fluences for 1977-1983 Space Missions", J. Spacecraft and Rockets, 11: 401-408, 1974.
11. Stassinopoulos, E. G., "SOLPRO: A Computer Code to Calculate Probabilistic Energetic Solar Proton Fluences", NSSDC 75-11, National Space Science Data Center, Greenbelt, Maryland, April 1975.
12. Seltzer, S., "SHIELDOSE: A Computer Code for Space Shielding Radiation Dose Calculations", U.S. Department of Commerce, National Bureau of Standards, NBS Technical Note 1116, May 1980.

TABLE 1

TABLE 2

 ***** ORBITAL FLUX STUDY WITH CLOUDSITE PARTICLE ENVIRONMENT: VENUS, AERB, AEL7 FLR, SOLAR MAXIMUM
 ***** UNCERTAINTY FACTORS (UF) APPLIED FOR THIS RUN ARE:
 ***** FOR PROTONS (APB1) - JF = 1.0
 ***** FOR INNER ZONE EFFECTS (AEB1) - UF = 1.0
 ***** FOR ALL MAG. MODEL - 4
 ***** BARKA-COUGHLIN ET AL. 1975 - PW 1989.5
 ***** TIME = 1989.5
 ***** 2 SWIMMERS IN A GOLF CART TRADE
 ***** FOR INFORMATION JR EXPLANATION CONTACT E.S. STASSI KOPOLIS AT NASA-GSFC, CODE 611, GSFC, GREENBELT, MARYLAND 20771-1000
 ***** PRETCNC
 ***** SPECIAL DISTRIBUTION : NORMALIZED FLUX OR ENERGY GREATER THAN F COOMEV

ENERGY >(MEV)	1.0E-6	1.0E-5	1.0E-4	1.0E-3	1.0E-2	1.0E-1	1.0E0	1.0E+1	1.0E+2	1.0E+3	1.0E+4	1.0E+5	1.0E+6	1.0E+7	1.0E+8	1.0E+9	1.0E+10	1.0E+11	1.0E+12	1.0E+13	1.0E+14	1.0E+15	1.0E+16	1.0E+17	1.0E+18	1.0E+19	1.0E+20	1.0E+21	1.0E+22	1.0E+23	1.0E+24	1.0E+25	1.0E+26	1.0E+27	1.0E+28	1.0E+29	1.0E+30	1.0E+31	1.0E+32	1.0E+33	1.0E+34	1.0E+35	1.0E+36	1.0E+37	1.0E+38	1.0E+39	1.0E+40	1.0E+41	1.0E+42	1.0E+43	1.0E+44	1.0E+45	1.0E+46	1.0E+47	1.0E+48	1.0E+49	1.0E+50	1.0E+51	1.0E+52	1.0E+53	1.0E+54	1.0E+55	1.0E+56	1.0E+57	1.0E+58	1.0E+59	1.0E+60	1.0E+61	1.0E+62	1.0E+63	1.0E+64	1.0E+65	1.0E+66	1.0E+67	1.0E+68	1.0E+69	1.0E+70	1.0E+71	1.0E+72	1.0E+73	1.0E+74	1.0E+75	1.0E+76	1.0E+77	1.0E+78	1.0E+79	1.0E+80	1.0E+81	1.0E+82	1.0E+83	1.0E+84	1.0E+85	1.0E+86	1.0E+87	1.0E+88	1.0E+89	1.0E+90	1.0E+91	1.0E+92	1.0E+93	1.0E+94	1.0E+95	1.0E+96	1.0E+97	1.0E+98	1.0E+99	1.0E+100	1.0E+101	1.0E+102	1.0E+103	1.0E+104	1.0E+105	1.0E+106	1.0E+107	1.0E+108	1.0E+109	1.0E+110	1.0E+111	1.0E+112	1.0E+113	1.0E+114	1.0E+115	1.0E+116	1.0E+117	1.0E+118	1.0E+119	1.0E+120	1.0E+121	1.0E+122	1.0E+123	1.0E+124	1.0E+125	1.0E+126	1.0E+127	1.0E+128	1.0E+129	1.0E+130	1.0E+131	1.0E+132	1.0E+133	1.0E+134	1.0E+135	1.0E+136	1.0E+137	1.0E+138	1.0E+139	1.0E+140	1.0E+141	1.0E+142	1.0E+143	1.0E+144	1.0E+145	1.0E+146	1.0E+147	1.0E+148	1.0E+149	1.0E+150	1.0E+151	1.0E+152	1.0E+153	1.0E+154	1.0E+155	1.0E+156	1.0E+157	1.0E+158	1.0E+159	1.0E+160	1.0E+161	1.0E+162	1.0E+163	1.0E+164	1.0E+165	1.0E+166	1.0E+167	1.0E+168	1.0E+169	1.0E+170	1.0E+171	1.0E+172	1.0E+173	1.0E+174	1.0E+175	1.0E+176	1.0E+177	1.0E+178	1.0E+179	1.0E+180	1.0E+181	1.0E+182	1.0E+183	1.0E+184	1.0E+185	1.0E+186	1.0E+187	1.0E+188	1.0E+189	1.0E+190	1.0E+191	1.0E+192	1.0E+193	1.0E+194	1.0E+195	1.0E+196	1.0E+197	1.0E+198	1.0E+199	1.0E+200	1.0E+201	1.0E+202	1.0E+203	1.0E+204	1.0E+205	1.0E+206	1.0E+207	1.0E+208	1.0E+209	1.0E+210	1.0E+211	1.0E+212	1.0E+213	1.0E+214	1.0E+215	1.0E+216	1.0E+217	1.0E+218	1.0E+219	1.0E+220	1.0E+221	1.0E+222	1.0E+223	1.0E+224	1.0E+225	1.0E+226	1.0E+227	1.0E+228	1.0E+229	1.0E+230	1.0E+231	1.0E+232	1.0E+233	1.0E+234	1.0E+235	1.0E+236	1.0E+237	1.0E+238	1.0E+239	1.0E+240	1.0E+241	1.0E+242	1.0E+243	1.0E+244	1.0E+245	1.0E+246	1.0E+247	1.0E+248	1.0E+249	1.0E+250	1.0E+251	1.0E+252	1.0E+253	1.0E+254	1.0E+255	1.0E+256	1.0E+257	1.0E+258	1.0E+259	1.0E+260	1.0E+261	1.0E+262	1.0E+263	1.0E+264	1.0E+265	1.0E+266	1.0E+267	1.0E+268	1.0E+269	1.0E+270	1.0E+271	1.0E+272	1.0E+273	1.0E+274	1.0E+275	1.0E+276	1.0E+277	1.0E+278	1.0E+279	1.0E+280	1.0E+281	1.0E+282	1.0E+283	1.0E+284	1.0E+285	1.0E+286	1.0E+287	1.0E+288	1.0E+289	1.0E+290	1.0E+291	1.0E+292	1.0E+293	1.0E+294	1.0E+295	1.0E+296	1.0E+297	1.0E+298	1.0E+299	1.0E+300	1.0E+301	1.0E+302	1.0E+303	1.0E+304	1.0E+305	1.0E+306	1.0E+307	1.0E+308	1.0E+309	1.0E+310	1.0E+311	1.0E+312	1.0E+313	1.0E+314	1.0E+315	1.0E+316	1.0E+317	1.0E+318	1.0E+319	1.0E+320	1.0E+321	1.0E+322	1.0E+323	1.0E+324	1.0E+325	1.0E+326	1.0E+327	1.0E+328	1.0E+329	1.0E+330	1.0E+331	1.0E+332	1.0E+333	1.0E+334	1.0E+335	1.0E+336	1.0E+337	1.0E+338	1.0E+339	1.0E+340	1.0E+341	1.0E+342	1.0E+343	1.0E+344	1.0E+345	1.0E+346	1.0E+347	1.0E+348	1.0E+349	1.0E+350	1.0E+351	1.0E+352	1.0E+353	1.0E+354	1.0E+355	1.0E+356	1.0E+357	1.0E+358	1.0E+359	1.0E+360	1.0E+361	1.0E+362	1.0E+363	1.0E+364	1.0E+365	1.0E+366	1.0E+367	1.0E+368	1.0E+369	1.0E+370	1.0E+371	1.0E+372	1.0E+373	1.0E+374	1.0E+375	1.0E+376	1.0E+377	1.0E+378	1.0E+379	1.0E+380	1.0E+381	1.0E+382	1.0E+383	1.0E+384	1.0E+385	1.0E+386	1.0E+387	1.0E+388	1.0E+389	1.0E+390	1.0E+391	1.0E+392	1.0E+393	1.0E+394	1.0E+395	1.0E+396	1.0E+397	1.0E+398	1.0E+399	1.0E+400	1.0E+401	1.0E+402	1.0E+403	1.0E+404	1.0E+405	1.0E+406	1.0E+407	1.0E+408	1.0E+409	1.0E+410	1.0E+411	1.0E+412	1.0E+413	1.0E+414	1.0E+415	1.0E+416	1.0E+417	1.0E+418	1.0E+419	1.0E+420	1.0E+421	1.0E+422	1.0E+423	1.0E+424	1.0E+425	1.0E+426	1.0E+427	1.0E+428	1.0E+429	1.0E+430	1.0E+431	1.0E+432	1.0E+433	1.0E+434	1.0E+435	1.0E+436	1.0E+437	1.0E+438	1.0E+439	1.0E+440	1.0E+441	1.0E+442	1.0E+443	1.0E+444	1.0E+445	1.0E+446	1.0E+447	1.0E+448	1.0E+449	1.0E+450	1.0E+451	1.0E+452	1.0E+453	1.0E+454	1.0E+455	1.0E+456	1.0E+457	1.0E+458	1.0E+459	1.0E+460	1.0E+461	1.0E+462	1.0E+463	1.0E+464	1.0E+465	1.0E+466	1.0E+467	1.0E+468	1.0E+469	1.0E+470	1.0E+471	1.0E+472	1.0E+473	1.0E+474	1.0E+475	1.0E+476	1.0E+477	1.0E+478	1.0E+479	1.0E+480	1.0E+481	1.0E+482	1.0E+483	1.0E+484	1.0E+485	1.0E+486	1.0E+487	1.0E+488	1.0E+489	1.0E+490	1.0E+491	1.0E+492	1.0E+493	1.0E+494	1.0E+495	1.0E+496	1.0E+497	1.0E+498	1.0E+499	1.0E+500	1.0E+501	1.0E+502	1.0E+503	1.0E+504	1.0E+505	1.0E+506	1.0E+507	1.0E+508	1.0E+509	1.0E+510	1.0E+511	1.0E+512	1.0E+513	1.0E+514	1.0E+515	1.0E+516	1.0E+517	1.0E+518	1.0E+519	1.0E+520	1.0E+521	1.0E+522	1.0E+523	1.0E+524	1.0E+525	1.0E+526	1.0E+527	1.0E+528	1.0E+529	1.0E+530	1.0E+531	1.0E+532	1.0E+533	1.0E+534	1.0E+535	1.0E+536	1.0E+537	1.0E+538	1.0E+539	1.0E+540	1.0E+541	1.0E+542	1.0E+543	1.0E+544	1.0E+545	1.0E+546	1.0E+547	1.0E+548	1.0E+549	1.0E+550	1.0E+551	1.0E+552	1.0E+553	1.0E+554	1.0E+555	1.0E+556	1.0E+557	1.0E+558	1.0E+559	1.0E+560	1.0E+561	1.0E+562	1.0E+563	1.0E+564	1.0E+565	1.0E+566	1.0E+567	1.0E+568	1.0E+569	1.0E+570	1.0E+571	1.0E+572	1.0E+573	1.0E+574	1.0E+575	1.0E+576	1.0E+577	1.0E+578	1.0E+579	1.0E+580	1.0E+581	1.0E+582	1.0E+583	1.0E+584	1.0E+585	1.0E+586	1.0E+587	1.0E+588	1.0E+589	1.0E+590	1.0E+591	1.0E+592	1.0E+593	1.0E+594	1.0E+595	1.0E+596	1.0E+597	1.0E+598	1.0E+599	1.0E+600	1.0E+601	1.0E+602	1.0E+603	1.0E+604	1.0E+605	1.0E+606	1.0E+607	1.0E+608	1.0E+609	1.0E+610	1.0E+611	1.0E+612	1.0E+613	1.0E+614	1.0E+615	1.0E+616	1.0E+617	1.0E+618	1.0E+619	1.0E+620	1.0E+621	1.0E+622	1.0E+623	1.0E+624	1.0E+625	1.0E+626	1.0E+627	1.0E+628	1.0E+629	1.0E+630	1.0E+631	1.0E+632	1.0E+633	1.0E+634	1.0E+635	1.0E+636	1.0E+637	1.0E+638	1.0E+639	1.0E+640	1.0E+641	1.0E+642	1.0E+643	1.0E+644	1.0E+645	1.0E+646	1.0E+647	1.0E+648	1.0E+649	1.0E+650	1.0E+651	1.0E+652	1.0E+653	1.0E+654	1.0E+655	1.0E+656	1.0E+657	1.0E+658	1.0E+659	1.0E+660	1.0E+661	1.0E+662	1.0E+663	1.0E+664	1.0E+665	1.0E+666	1.0E+667	1.0E+668	1.0E+669	1.0E+670	1.0E+671	1.0E+672	1.0E+673	1.0E+674	1.0E+675	1.0E+676	1.0E+677	1.0E+678	1.0E+679	1.0E+680	1.0E+681	1.0E+682	1.0E+683	1.0E+684	1.0E+685	1.0E+686	1.0E+687	1.0E+688	1.0E+689	1.0E+690	1.0E+691	1.0E+692	1.0E+693	1.0E+694	1.0E+695	1.0E+696	1.0E+697	1.0E+698	1.0E+699	1.0E+700	1.0E+701	1.0E+702	1.0E+703	1.0E+704	1.0E+705	1.0E+706	1.0E+707	1.0E+708	1.0E+709	1.0E+710	1.0E+711	1.0E+712	1.0E+713	1.0E+714	1.0E+715	1.0E+716	1.0E+717	1.0E+718	1.0E+719	1.0E+720	1.0E+721	1.0E+722	1.0E+723	1.0E+724	1.0E+725	1.0E+726	1.0E+727	1.0E+728	1.0E+729	1.0E+730	1.0E+731	1.0E+732	1.0E+733	1.0E+734	1.0E+735	1.0E+736	1.0E+737	1.0E+738	1.0E+739	1.0E+740	1.0E+741	1.0E+742	1.0E+743	1.0E+744	1.0E+745	1.0E+746	1.0E+747	1.0E+748	1.0E+749	1.0E+750	1.0E+751	1.0E+752	1.0E+753	1.0E+754	1.0E+755	1.0E+756	1.0E+757	1.0E+758	1.0E+759	1.0E+760	1.0E+761	1.0E+762	1.0E+763	1.0E+764	1.0E+765	1.0E+766	1.0E+767	1.0E+768	1.0E+769	1.0E+770	1.0E+771	1.0E+772	1.0E+773	1.0E+774	1.0E+775	1.0E+776	1.0E+777	1.0E+778	1.0E+779	1.0E+780	1.0E+781	1.0E+782	1.0E+783	1.0E+784	1.0E+785	1.0E+786	1.0E+787	1.0E+788	1.0E+789	1.0E+790	1.0E+791	1.0E+792	1.0E+793	1.0E+794	1.0E+795	1.0E+796	1.0E+797	1.0E+798	1.0E+799	1.0E+800	1.0E+801	1.0E+802	1.0E+803	1.0E+804	1.0E+805	1.0E+806	1.0E+807	1.0E+808	1.0E+809	1.0E+810	1.0E+811	1.0E+812	1.0E+813	1.0E+814	1.0E+815	1.0E+816	1.0E+817	1.0E+818	1.0E+819	1.0E+820	1.0E+821	1.0E+822	1.0E+823	1.0E+824	1.0E+825	1.0E+826	1.0E+827	1.0E+828	1.0E+829	1.0E+830	1.0E+831	1.0E+832	1.0E+833	1.0E+834	1.0E+835	1.0E+836	1.0E+837	1.0E+838	1.0E+839	1.0E+840	1.0E+841	1.0E+842	1.0E+843	1.0E+844	1.0E+845	1.0E+846	1.0E+84

TABLE 4

TABLE 5

TABLE 6

URETIA FLUX STUDY WITH COMPOSITE PARTICLE ENSEMBLES: VARIATIONS AND ANALYSIS OF THE UNLUX CF 1979
UNCERTAINTY FACTORS (UF) APPLIED TO THIS FLUX FUNCTIONAL FORMULA, AND THE UNLUX CF 1979 UF = 1.0
MAGNETIC COOKING FACTOR AND ACCURACY OF THE UNLUX UNLUX CF 1979 UF = 1.0495
FOR INFORMATION OF EXPLANATION OF THESE UNLUX UNLUX CF 1979 UF = 1.0438

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TABLE 7

ORBITAL FLUX STATION WITH COMPUTED EFFICIENT ORBITS AND UNCERTAINTY FACTORS FOR THE FUNAFUTI PLANETARY MAGNETIC CONCURRENCES AND ULTRACOOL FLUX LEVELS AND MAXIMUM INCULPATIVE POLLUTION INDEXES

FOR INFORMATION OF EXPLOITATION CONTACT: GOVERNMENT OF LUXEMBOURG

THE LANE COASTAL PLATEAU

TABLE 8

SOLAR THERMAL DISTILLATION ENERGY FLUXES AND CONVECTION COEFFICIENTS

TABLE 9

DEBLIN FLUX STUDY BILATERAL ENVIRONMENTAL ASSESSMENT FOR SULAN TAHMUN INC. - UFLUX OF 1979 - 44
INCERTAINTY FACTOR 5.0 FOR THIS STUDY. BILATERAL ENVIRONMENTAL ASSESSMENT FOR SULAN TAHMUN INC. - UFLUX OF 1979 - 44
MAGNETIC COORDINATES AND COMPUTED BY INVACSA IN 1972 WITH ALLUVIAL VOLCANIC LAYER. BILATERAL ENVIRONMENTAL ASSESSMENT FOR SULAN TAHMUN INC. - UFLUX OF 1979 - 44
FOR INFORMATION OR EXPLANATION CONTACT S. STJORNARUD, NASA-CODE 601, CHURCHILL, MANITOBA, CANADA N0A 1L0. BILATERAL ENVIRONMENTAL ASSESSMENT FOR SULAN TAHMUN INC. - UFLUX OF 1979 - 44
ELECTIONS FOR THE BILATERAL ENVIRONMENTAL ASSESSMENT FOR SULAN TAHMUN INC. - UFLUX OF 1979 - 44
SPECIAL DISTRIBUTION: NORMALIZED FLUX OF ENERGY (WATT) PER CC/M² V

TABLE 10

TABLE II A BRIEF STUDY WITH COMPUTED PARTICLE ENVIRONMENTS FOR THE APPLIED FIELD IN VARIOUS CIRCUMSTANCES AND COMPUTED BY IRVING J. FELTON AND R. L. WILSON, ALL AT NASA-GFSC, GREENBELT, MARYLAND, 1972. THE COMPUTATIONS ARE FOR A BLOCK IMPACTOR OF 10.37 gm² AND A BLOCK IMPACTOR OF 1.037 gm². THE CONTACT TIME IS 1.0 sec. AND THE IMPACT VELOCITY IS 10 km/sec. THE IMPACT DIRECTION IS NORMAL TO THE SURFACE. THE COMPUTED FLUXES ARE FOR THE EARTH'S MAGNETIC FIELD AND FOR THE EARTH'S FIELD WITH A 100 G GAUSS FIELD ADDED ALONG THE DIRECTION OF MOTION. THE COMPUTED FLUXES ARE FOR THE EARTH'S FIELD AND FOR THE EARTH'S FIELD WITH A 100 G GAUSS FIELD ADDED ALONG THE DIRECTION OF MOTION. THE COMPUTED FLUXES ARE FOR THE EARTH'S FIELD AND FOR THE EARTH'S FIELD WITH A 100 G GAUSS FIELD ADDED ALONG THE DIRECTION OF MOTION.

Table II

TAKE 1/2

TABLE I

***** ORBITAL FLUX STUDY WITH COMPOSITE PARTICLE ENVIRONMENTAL VARIETIES. APB: AEG-AE17 FOR SOLAR MAXIMUM UNIF. LUX (AE6) - UP = 1.0 JF = 1.0; FOR INFR. ZONE ELECTRONS (AE6) - UP = 1.0 JF = 1.0. FOR THIS RUN ARE: MAGNETIC COORDINATES B AND L COMPUTED BY INVARA OF 1972 WITH ALL MAG. MODEL 4; BARRAGAUGH ET AL. 16-E-TRN 1975 * TIME = 1989.5 * VEHICLE: INV-A-2000A AND AGOGE-E-1602KA AND INCLINATION 60DEG. * DELEGATE: D. G. CUBILLI, TAPER: JOSAAAD, DELCO: 1-005. * FOR INFORMATION OR EXPLANATION CONTACT E.G. STASSING/CPC/CG, AT NASA-GSFC, CODE 601, GREENBELT, MARYLAND 20771. TEL. (301) 344-8067. * ELECTRONS LTD.

***** SPECTRUM IN PERCENT DELTA ENERGY *****

ENERGY RANGES #CM ⁻² /SEC #/MEV	AVERAGED TOTAL FLUX #CM ⁻² /DAY	SPECTRUM LEVELS #MEV	ENERGY LEVELS #MEV	AVERAGED INFLUX #CM ⁻² /SEC	AVERAGED TOTAL FLUX #CM ⁻² /DAY	AVERAGED INFLUX #CM ⁻² /SEC	AVERAGED TOTAL FLUX #CM ⁻² /DAY	AVERAGED INFLUX #CM ⁻² /SEC	AVERAGED TOTAL FLUX #CM ⁻² /DAY	AVERAGED INFLUX #CM ⁻² /SEC	AVERAGED TOTAL FLUX #CM ⁻² /DAY	AVERAGED INFLUX #CM ⁻² /SEC
1.000-5.000	1.028E-02	8.89E-11	1.726	1.000E-011	6.11E-07	1.322E-12	2.311E-15	1.5	2.311E-15	1.5	6.93E-15	1.5
5.000-1.000	2.698E-05	2.331E-10	1.763	7.000E-011	1.265E-07	1.093E-12	1.54E-15	1.5	1.54E-15	1.5	5.52E-15	1.5
1.000-1.500	3.735E-04	3.227E-09	0.247	1.000E-011	1.062E-07	9.172E-12	1.61E-15	1.5	1.61E-15	1.5	4.42E-15	1.5
1.500-2.000	1.357E-03	1.176E-09	0.089	4.923E-006	4.251E-06	7.758E-11	7.758E-14	1.4	7.758E-14	1.4	2.72E-14	1.4
2.000-3.000	6.336E-03	7.020E-08	0.055	3.000	2.085E-006	1.802E-06	3.289E-14	1.4	3.289E-14	1.4	1.69E-14	1.4
3.000-4.000	1.901E-03	1.642E-08	0.03	4.000	6.124E-005	7.119E-05	1.281E-14	1.4	1.281E-14	1.4	6.43E-15	1.4
4.000-5.000	3.229E-02	2.760E-07	0.02	5.000	3.312E-005	2.862E-05	5.22E-15	1.2	5.22E-15	1.2	2.47E-15	1.2
5.000-6.000	1.618E-01	1.618E-06	0.01	6.000	2.127E-005	1.618E-05	3.35E-15	1.2	3.35E-15	1.2	1.029E-15	1.2
6.000- OVER	1.461E-02	1.263E-03	0.000	2.000	1.415E-005	1.223E-05	2.31E-15	1.2	2.31E-15	1.2	5.25E-15	1.2
TOTAL	1.062E-03	9.172E-11	7.0164	8.000	1.023E-015	8.839E-09	1.612E-13	1.2	1.612E-13	1.2	5.802E-12	1.2
***** EXPOSURE INDEX: ENERGY > 5000 MEV *****	1.000	6.181E-04	5.306E-04	9.000	6.181E-004	5.306E-004	7.477E-13	1.2	7.477E-13	1.2	4.28E-12	1.2
INTENSITY EXPOSURE TOTAL # OF RANGES DURATION ACCUMULATED #/CM ⁻² /SEC (HOURS)	1.500	2.435E-04	1.593E-04	1.750	2.078E-004	1.376E-004	3.793E-12	1.2	3.793E-12	1.2	3.25E-12	1.2
ZERO-PTOX 1.E0-1.E1 1.E1-1.E2 1.E2-1.E3 1.E3-1.E4 1.E4-1.E5	0.517 0.350 0.133 0.777 2.467 6.083	0.0 0.2 0.0 0.0 0.0 0.0	7.418E-02 2.284E-02 1.359E-02 1.54E-02 1.54E-02 0.8	3.000 3.253 3.500 3.750 4.000 4.500	3.000 1.313E-03 1.159E-02 5.247E-02 4.528E-02 2.951E-02	2.919E-08 1.937E-08 1.135E-08 7.057E-08 5.528E-08 3.030E-08	5.122E-11 5.039E-11 2.071E-11 1.288E-11 1.288E-11 1.288E-11	1.682E-11 1.682E-11 1.682E-11 1.682E-11 1.682E-11 1.682E-11	3.64E-11 3.64E-11 2.817E-11 2.817E-11 2.817E-11 2.817E-11	6.128E-01 6.128E-01 2.567E-01 2.567E-01 2.567E-01 2.567E-01		
TOTAL	24.0000	2.462E-10	7.0000	6.550	6.550	6.550	0.3	0.3	0.3	0.3	0.0	0.0

TABLE 14

***** SPECTRUM IN PERCENT DELTA ENERGY *****
 ENERGY RANGES AVERAGED FLUX SPECTRUM *****
 TOTAL FLUX TOTAL FLUX AVERAGED FLUX
 2(MEV) μ CM $^{-2}$ /SEC μ CM $^{-2}$ /DAY PERCENT
 2(MEV) μ CM $^{-2}$ /SEC μ CM $^{-2}$ /DAY
 ***** UNDILUTED FLUX STUDY WITH COMPOSITE PARTICLES ENVIRONMENTAL VARIANCE AMBI AEG AL17 FROM SOLAR MAXIMUM UNIF LUX 1979
 ***** UNCERTAINTY FACTORS (LAPB) - JF=1.0; FN=1.0; INFEZDNFLCPCNS (LAPB) - UF=1.3
 ***** MAGNETIC COORDINATES H AND L COMPUTED BY INVARA OF 1972 #11 ALL MAG. MODEL 4; LARMAUGH ET AL. 1975 TIME = 1989.5
 ***** MAGNETIC COORDINATES H AND L COMPUTED BY INVARA OF 1972 #11 ALL MAG. MODEL 4; LARMAUGH ET AL. 1975 TIME = 1989.5
 ***** FOR INFORMATION OR EXPLANATION CONTACT E.C. STASSIN, RPPCL, AT NAL-GUFC, CONE C01, GR. CRISTI, MAI YLAND 20771, TEL. (301) 344-8067
 ***** PRETICES

		***** CLOUDS ITC CLOUD SPECTRUM ***** TAU = 5.0000 YAH(15)									
		ENERGY LEVELS					AVERAGED INTEGRATED FLUX				
		μ CM $^{-2}$ /SEC					μ CM $^{-2}$ /DAY				
		1.000-2.000	5.219F 05	7.592E 10	6.141E 05	4.000E-011	5.041E 06	1.333E 11	1.1	2.372E 14	1.372E 14
2.000-3.000	2.366E 04	2.366E 04	1.324E 04	1.144E 05	0.880	1.000E 004	8.861E 05	9.544E 10	1.559E 14	6.222E 03	8.246E 03
3.000-4.000	6.431E 03	6.431E 03	5.575E 03	5.575E 03	0.428	5.003	1.971E 05	1.773E 10	3.107E 13	6.923E 02	7.303E 02
4.000-5.000	1.396E 03	1.396E 03	1.276E 03	1.276E 03	0.920	1.003	9.869E 05	8.327E 09	1.557E 13	1.303E 01	2.941E 01
5.000-50.000	3.184E 03	3.184E 03	2.751E 08	2.751E 08	0.212	2.000	6.500E 04	5.616E 05	1.025E 13	2.941E 01	2.941E 01
50.00-100.0	2.099E 03	2.099E 03	1.814E 08	1.814E 08	0.140	3.000	5.444E 04	4.744E 05	8.582E 12	9.623E 02	9.623E 02
100.0-500.0	2.495E 03	2.495E 03	2.447E 08	2.447E 08	0.165	4.000	4.703E 04	4.2664E 05	7.416E 12	6.023E 02	6.023E 02
500.0-1000	3.981E 01	3.981E 01	2.440E 08	2.440E 08	0.303	5.000	4.140E 04	3.583E 05	6.534E 12	5.164E 02	5.164E 02
TOTAL	5.894E 05	8.544E 10	65.739	8.000	2.022E 04	2.436E 04	2.436E 05	2.436E 12	2.544E 05	0.0	0.0
***** EXPOSURE INDEX: ENERGY > 5.000 MEV *****			1.000	1.000	2.177E 34	1.431E 34	1.431E 35	3.432E 12	2.177E 34	1.012E 29	1.012E 29
***** INTENSITY EXPONENTIAL TOTAL OF RANGES DURATION ACCUMULATED PARTICLES μ CM $^{-2}$ /SEC SHOURS *****			1.577E 35	1.577E 35	1.430E 35	1.430E 35	1.430E 35	2.217E 12	1.430E 35	1.012E 29	1.012E 29
ZERO FLUX 5.050	0.0	5.050	5.050	5.050	5.047E 32	5.047E 32	5.047E 32	1.431E 12	5.047E 32	0.0	0.0
1.0E-1 1.0E2	5.219	5.219	6.563E 33	6.563E 33	6.030	4.624E 32	3.958E 32	7.292E 11	7.038E-13	5.502E-02	5.502E-02
1.0E-2 1.0E3	1.350	1.350	2.086E 05	2.086E 05	1.000	3.212E 33	2.775E 33	5.064E 11	3.840E-02	3.840E-02	3.840E-02
1.0E-3 1.0E4	2.463	2.463	2.684E 06	2.684E 06	1.000	2.525E 33	2.182E 33	5.592E 11	2.982E-02	2.982E-02	2.982E-02
1.0E-4 1.0E5	4.130	4.130	4.441E 07	4.441E 07	1.500	1.423E 33	1.237E 33	2.255E 11	1.603E-02	1.603E-02	1.603E-02
1.0E-5 1.0E6	5.283	5.283	2.045E 08	2.045E 08	2.000	3.067E 02	6.973E 02	1.277E 11	8.785E-03	8.785E-03	8.785E-03
1.0E-6 1.0E7	1.200	1.200	2.045E 08	2.045E 08	2.000	4.841E 02	4.216E 02	2.676E 10	5.002E-03	5.002E-03	5.002E-03
1.0E-7 OVER	0.0	0.0	0.0	0.0	3.000	2.654E 02	2.532E 02	4.640E 10	2.962E-03	2.962E-03	2.962E-03
TOTAL	24.000	3.580E 39	500.0	500.0	1.781E 32	1.581E 32	2.094E 06	2.094E 10	1.781E 32	1.064E-02	1.064E-02
					3.981E 31	3.981E 31	3.981E 31	6.277E 04	3.981E 31	1.571E-04	1.571E-04

TABLE 15

ORBITAL FLUX STUDY WITH CLOUDS IN THE ENVIRONMENT; VELT S. AND AL. 17 JULY 1979
 UNCERTAINTY FACTORS OF 1 APPLIED FOR THIS RUN ARE:
 MAGNETIC COORDINATES & ANGULAR CHANGES IN VARIOUS HEAVY
 NUCLEI.
 FOR INFORMATION OR EXPLANATION CONTACT DR. STASINSKI AT NASA-JPL, CURE 601, JET PROPULSION LABORATORY, ELECTRONS LC

SPECTRUM IN PERCENT DELTA ENERGY *****

ENERGY RANGES >>(MeV)	AVERAGED TOTAL FLUX #/CM**2/SEC	SPECTRUM TOTAL FLUX #/CM**2/SEC	ENERGY LEVELS >(MeV)	AVERAGED INTEGRAL FLUX #/CM**2/SEC	AVERAGED INTEGRAL FLUX #/CM**2/SEC	AVERAGED INTEGRAL FLUX #/CM**2/SEC	AVERAGED INTEGRAL FLUX #/CM**2/SEC
1.000-1.500	2.56E-32	2.62E-32	1.79E-10	2.16E-10	2.30E-10	2.25E-10	2.16E-10
1.500-2.000	6.45E-32	6.52E-32	3.71E-05	3.70E-05	3.70E-05	3.70E-05	3.70E-05
2.000-3.000	2.82E-32	2.82E-32	7.12E-05	7.07E-05	7.07E-05	7.07E-05	7.07E-05
3.000-4.000	4.31E-32	4.31E-32	1.72E-05	1.69E-05	1.69E-05	1.69E-05	1.69E-05
4.000-5.000	6.02E-32	6.02E-32	5.19E-05	5.09E-05	5.09E-05	5.09E-05	5.09E-05
5.000-6.000	3.44E-32	3.44E-32	2.15E-05	2.02E-05	2.02E-05	2.02E-05	2.02E-05
6.000-6.45E-02	1.25E-31	1.25E-31	0.086E-03	0.086E-03	0.086E-03	0.086E-03	0.086E-03
TOTAL	3.676E-37	3.176E-12	6.978E-06	6.933E-06	6.933E-06	6.933E-06	6.933E-06
EXPOSURE INDEX: ENERGY>5000 MEV *****	1.253	1.252	0.5	1.07E-05	1.07E-05	1.07E-05	1.07E-05
INTENSITY RANGES DURATION ACCUMULATED #/CM**2/SEC (HOURS)	1.75	7.42E-02	0.24	6.46E-04	6.46E-04	6.46E-04	6.46E-04
ECO-FLUX	0.663	0.663	0.5	1.02E-10	1.02E-10	1.02E-10	1.02E-10
1.E0-1.E1	3.067	6.75E-02	0.2	2.68E-02	2.68E-02	2.68E-02	2.68E-02
1.E1-1.E2	0.167	2.52E-02	0.4	1.54E-02	1.54E-02	1.54E-02	1.54E-02
1.E2-1.E3	0.267	3.66E-02	0.5	9.80E-03	9.80E-03	9.80E-03	9.80E-03
1.E3-1.E4	0.820	1.75E-02	0.7	4.23E-02	4.23E-02	4.23E-02	4.23E-02
1.E4-1.E5	4.283	6.65E-02	0.8	1.53E-02	1.53E-02	1.53E-02	1.53E-02
1.E5-1.E6	5.817	1.50E-02	1.0	5.23E-02	5.23E-02	5.23E-02	5.23E-02
1.E6-1.E7	7.917	8.17E-02	1.3	3.01E-02	3.01E-02	3.01E-02	3.01E-02
1.E7-1.E8	0.0	6.00E-02	1.0	1.01E-01	1.01E-01	1.01E-01	1.01E-01
TOTAL	24.039	5.285E-13	7.300	0.0	0.0	0.0	0.0

TABLE /6

ORBITAL PLUX STUDY WITH COMPOSITE PARTICLE ENVIRONMENTS: VETTES APD-AEG-AE17 P/JR SCALAR MAXIMUM UNIFLUX CP 1974
PRACTICAL FOR THIS RAYBARE: 1. J. PORBINNEE ELECTRONS 1 (AEG) - U/E = 1.0
UNCERTAINITY FACTORS (UP) APPLIED TO COMPUTED BY INVESTIGATION OF 1972. D. KIRKACLOUGH, ET AL. MODEL = 1.75 FINKE = 1.689.5
HORIZONTAL COORDINATES B AND PERIGEE = 3489 KM PERIGEE = 3649 KM PERIOD = 1054.6 SEC.
VEHICLE: NAVX-5 MAX INCLINATION = 60 DEG. PERIGEE = 3489 KM. EQUATORIAL TAPF = 1054.6 SEC.
FOR INFORMATION CONTACT E.O. STASSINOPOLOV AT NASA-GSP/COD2 611 GREENBELT MARYLAND 20771 TEL: (301) - 344-8677
EXPLANATION OF ENVIRONMENTS

SPECTRUM IN PERCENT DELTA ENERGY ***

ENERGY RANGES >(HEV)	AVERAGED SPECTRUM		PERCENT
	TOTAL FLUX #/CH*2/SEC	AVERAGED FLUX #/CH*2/SEC	
100.0-2.000	2.57E 06	2.201E 11	0.2-270
100.0-5.000	1.48E 06	2.812E 10	3.624
100.0-8.000	7.72E 05	6.67E 09	1.889
100.0-10.000	3.07E 04	2.657E 09	0.752
100.0-15.000	4.75E 04	4.099E 08	0.198
100.0-25.000	4.49E 03	3.917E 08	0.098
100.0-50.000	4.59E 03	3.841E 08	0.028
100.0-100.0	1.51E 02	0.841E 07	0.000
100.0-200.0	1.01E 01	0.804E 05	0.000
TOTAL	2.85E 06	2.470E 11	69.368

***** EXPOSURE INDEX: ENERGY>5.000 MEV *****			
INTENSITY RANGES #/CH*2/SEC	EXPOSURE TOTAL & OF DURATION	ACCUMULATED	PARTICLES
2.0E-1-2.1	7.233	0.7	943E 33
1.2E-1-2.2	0.283	1.1	725E 03
1.2E-1-2.3	1.117	1.467	1025E 03
1.2E-1-2.4	1.124	1.833	735E 03
1.2E-1-2.5	1.125	3.917	1345E 03
1.2E-1-2.6	1.125	8.833	2045E 03
1.2E-1-2.7	1.125	1.993	2.407E 03
1.2E-1-OVER	0.0	0.0	0.0
TOTAL	24.400	1.405E 10	

TABLE 17

ORBITAL PLUN STUDY WITH COMBINE 2 ARTICLE ENVIRONMENTS. VETTES APH AEG A317 PGE SCALAR MAXIMUM UNPLUX OF 1975. ORBITAL PLUN STUDY WITH COMBINE 2 ARTICLE ENVIRONMENTS. VETTES APH AEG A317 PGE SCALAR MAXIMUM UNPLUX OF 1975. UNCERTAINTY FACTORS (UP) APPLIED FOR THIS RUN ARE: UP = 1.0. FOR INNER ZONE ELECTIONS (APL) - UP = 1.0. FOR EXPACIONS (APL) - UP = 1.0. BANRAC/LUGH ITAL. 1689.5 LINE = 1989.5. HAGNETIC COORDINATES (QONEL 1775) = 388.9 KM. B/L ORBIT TAPF: LD546 * PEG10D: 2.878. MARYLAND 20771 ITEL (301) - 344-8067. FOR INFORMATION OR EXPLANATION CONTACT E.G. STASSINO/EQUULOS AT NASA-GSFC/CODE 601 GREENBELT, MARYLAND.

SPECTRUM IN PRESENT DIGITAL ENERGY • 4

ENERGY RANGES > (REV)	AVERAGED TOTAL FLUX #/CH**2/SEC	SPECTRUM TOTAL FLUX #/CH**2/SEC	PERCENT
1000-15000	6.301E-06	6.619E-06	1.000
1-10000	1.860E-06	1.975E-06	1.000
1-5000	1.258E-05	1.087E-05	1.000
1-2000	4.721E-05	4.075E-05	1.000
1-1000	2.000E-05	1.603E-05	1.000
1-500	6.000E-06	5.532E-06	1.000
1-200	1.500E-06	1.508E-06	1.000
1-100	5.000E-07	5.934E-07	1.000
1-50	1.500E-07	1.934E-07	1.000
1-25	5.000E-08	6.479E-08	1.000
1-12.5	1.500E-08	2.023E-08	1.000
1-6.25	5.000E-09	6.747E-09	1.000
1-3.125	1.500E-09	2.062E-09	1.000
1-1.562	5.000E-10	6.207E-10	1.000
1-0.781	1.500E-10	1.802E-10	1.000
TOTAL	6.508E-07	5.623E-12	6.9100
***** EXPOSURE INDEX: ENERGY > 5000 MEV *****			
INTENSITY RANGES #/CH**2/SEC	EXPOSURE DURATION (HOURS)	TOTAL # OF PARTICLES	ACCUMULATED PARTICLES
1-200	1.000	0.005	0.005
1-50	0.033	0.056	0.056
1-25	0.010	0.028	0.028
1-12.5	0.003	0.008	0.008
1-6.25	0.001	0.003	0.003
1-3.125	0.0003	0.001	0.001
1-1.562	0.0001	0.0003	0.0003
TOTAL	24.000	1.785E-11	0.000

TABLE I

DIRECT FLUX STUDY WITH COMPUTER PARTICLE SIMULATOR. THIS STUDY IS FOR THE 1972 ALTITUDE INCLINOMETER AND ACCUMULATORS. THE INCLINOMETER IS A 100000 COUNTS/SEC. COUNTER. THE ACCUMULATOR IS A 100000 COUNTS/SEC. COUNTER. THE INCLINOMETER AND ACCUMULATOR ARE CONNECTED IN PARALLEL. THE INCLINOMETER IS CONNECTED TO THE COMPUTER THROUGH A 100000 COUNTS/SEC. COUNTER. THE ACCUMULATOR IS CONNECTED TO THE COMPUTER THROUGH A 100000 COUNTS/SEC. COUNTER.

SPECTRUM IN PERCENT, FLUX ENERGY		EXPOSURE RATE, SEC/SEC		INTENSITY EXPOSURE RATE, SEC/SEC		ACCUMULATOR RATE, SEC/SEC	
ENERGY RANGES	AVERAGE TOTAL FLUX	SPATIAL FLUX	TOTAL FLUX	LEVELS	LEVELS	LEVELS	LEVELS
(keV)	a/CHARGE/SEC	a/CHARGE/SEC	a/CHARGE/SEC	(keV)	(keV)	(keV)	(keV)
1000-2000	0.0000	0.0000	0.0000	4.0000	0.0000	0.0000	0.0000
2000-5000	5.0000	5.0000	5.0000	4.0000	0.0000	0.0000	0.0000
5000-10000	3.0000	3.0000	3.0000	1.0000	0.0000	0.0000	0.0000
10000-20000	1.0000	1.0000	1.0000	0.0000	0.0000	0.0000	0.0000
20000-50000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
50000-100000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
100000-200000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
200000-500000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
500000-OVER	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
TOTAL	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

SPECTRUM IN PERCENT, FLUX ENERGY		EXPOSURE RATE, SEC/SEC		INTENSITY EXPOSURE RATE, SEC/SEC		ACCUMULATOR RATE, SEC/SEC	
ENERGY RANGES	AVERAGE TOTAL FLUX	SPATIAL FLUX	TOTAL FLUX	LEVELS	LEVELS	LEVELS	LEVELS
(keV)	a/CHARGE/SEC	a/CHARGE/SEC	a/CHARGE/SEC	(keV)	(keV)	(keV)	(keV)
1000-2000	1.0000	1.0000	1.0000	0.7500	0.7500	0.7500	0.7500
2000-5000	4.0000	4.0000	4.0000	1.0000	1.0000	1.0000	1.0000
5000-10000	3.0000	3.0000	3.0000	0.5000	0.5000	0.5000	0.5000
10000-20000	1.0000	1.0000	1.0000	0.0000	0.0000	0.0000	0.0000
20000-50000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
50000-100000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
100000-200000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
200000-500000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
500000-OVER	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
TOTAL	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

TABLE 19

THE PRACTICAL INVESTIGATOR

TABLE 20

ORBITAL FLUX STUDY WITH CLASSICAL PLANETARY EQUATIONS: VETTES AFB, ALB, AT 17 FEB 1979
INCREASINGLY ACCURATE FOR THIS PLANETARY EQUATION - JF = 1.0; FFL = 1.0; TIME = 1949.5
MAGNETIC COORDINATES AND COMPUTED INTEGRALS FOR ALL WGS-72 WITH MC2L
EFFECTIVE IN VARIOUS AREAS OF THE EARTH'S SURFACE.
FOR INFORMATION OR EXPLANATION CONTACT: STASSINUS CECIL, JR., 601 CECIL, MARYLAND 20731, USA.

SPECTRA IN DIFFERENT GELS AND BY

EXPOSURE INDEX: FUNDAMENTALS AND VARIATIONS

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TABLE 21

*** SPOTTRUM IN DIFFERENT SPECTRAL LINES, V 4000

***** TAU = 0.3000 YR(S) *****

TABLE 22

THE JOURNAL OF CLIMATE

TABLE 23

CHIETAL FLUX SPECTRUM FOR THE 1979 OUTBURST OF THE X-RAY SOURCE V404 ORIONIS. THIS PAPER CONTAINS THE DATA FROM THE 1979 OUTBURST, WHICH OCCURRED IN JUNE AND JULY. THE TOTAL FLUX DURING THE OUTBURST WAS 1.0 E-10 WATTS PER CM². THE TOTAL ENERGY RANGE IS 0.500-6.000 keV.

TABLE 1. FLUX SPECTRUM FOR THE 1979 OUTBURST

ENERGY RANGE (keV)	AVGARED FLUX		TOTAL FLUX	AVERAGED FLUX	TOTAL FLUX
	INTENSITy # / CM ⁻² SEC ⁻¹	FLUX W / CM ⁻² SEC ⁻¹			
0.500-1.000	1.0E+00	3.4E-02	3.4E-02	1.0E-01	3.4E-02
1.000-1.500	1.0E+00	1.0E-01	1.0E-01	1.0E-01	1.0E-01
1.500-2.000	1.0E+00	3.0E-02	3.0E-02	1.0E-01	3.0E-02
2.000-2.500	1.0E+00	1.0E-01	1.0E-01	1.0E-01	1.0E-01
2.500-3.000	1.0E+00	3.0E-02	3.0E-02	1.0E-01	3.0E-02
3.000-3.500	1.0E+00	1.0E-01	1.0E-01	1.0E-01	1.0E-01
3.500-4.000	1.0E+00	3.0E-02	3.0E-02	1.0E-01	3.0E-02
4.000-4.500	1.0E+00	1.0E-01	1.0E-01	1.0E-01	1.0E-01
4.500-5.000	1.0E+00	3.0E-02	3.0E-02	1.0E-01	3.0E-02
5.000-6.000	1.0E+00	1.0E-01	1.0E-01	1.0E-01	1.0E-01
TOTAL	1.0E+00	1.0E+00	1.0E+00	1.0E+00	1.0E+00
EXPOSURE TIME FOR 1000000000 W					
INTENSITy # / CM ⁻² SEC ⁻¹	EXPOSURE TIME SEC	INTEGRAL FLUX W / CM ⁻²	INTENSITy # / CM ⁻² SEC ⁻¹	EXPOSURE TIME SEC	INTEGRAL FLUX W / CM ⁻²
1.0E+00	1.0E+00	1.0E+00	1.0E+00	1.0E+00	1.0E+00
2.0E+00	2.0E+00	2.0E+00	2.0E+00	2.0E+00	2.0E+00
3.0E+00	3.0E+00	3.0E+00	3.0E+00	3.0E+00	3.0E+00
4.0E+00	4.0E+00	4.0E+00	4.0E+00	4.0E+00	4.0E+00
5.0E+00	5.0E+00	5.0E+00	5.0E+00	5.0E+00	5.0E+00
6.0E+00	6.0E+00	6.0E+00	6.0E+00	6.0E+00	6.0E+00
TOTAL	1.0E+00	1.0E+00	1.0E+00	1.0E+00	1.0E+00

TABLE 2. FLUX SPECTRUM FOR THE 1979 OUTBURST

ENERGY RANGE (keV)	AVGARED FLUX		TOTAL FLUX	AVERAGED FLUX	TOTAL FLUX
	INTENSITy # / CM ⁻² SEC ⁻¹	FLUX W / CM ⁻² SEC ⁻¹			
0.500-1.000	1.0E+00	3.4E-02	3.4E-02	1.0E-01	3.4E-02
1.000-1.500	1.0E+00	1.0E-01	1.0E-01	1.0E-01	1.0E-01
1.500-2.000	1.0E+00	3.0E-02	3.0E-02	1.0E-01	3.0E-02
2.000-2.500	1.0E+00	1.0E-01	1.0E-01	1.0E-01	1.0E-01
2.500-3.000	1.0E+00	3.0E-02	3.0E-02	1.0E-01	3.0E-02
3.000-3.500	1.0E+00	1.0E-01	1.0E-01	1.0E-01	1.0E-01
3.500-4.000	1.0E+00	3.0E-02	3.0E-02	1.0E-01	3.0E-02
4.000-4.500	1.0E+00	1.0E-01	1.0E-01	1.0E-01	1.0E-01
4.500-5.000	1.0E+00	3.0E-02	3.0E-02	1.0E-01	3.0E-02
5.000-6.000	1.0E+00	1.0E-01	1.0E-01	1.0E-01	1.0E-01
TOTAL	1.0E+00	1.0E+00	1.0E+00	1.0E+00	1.0E+00

TABLE 24

ORBITAL FLUX STUDY WITH COMPOSITE PARTICLE ENVIRONMENT VEHICLE APPROX ALONG EQUATOR
 UNCERTAINTY FACTORS (UF) APPLIED FOR THIS RUN ARE:
 MAGNETIC COORDINATES & L COMPUTED BY INVARA OF 1972 WITH ALL MAG. ALIGN.
 VEHICLE AND X-LISMAX ANALYSIS ALONG EQUATOR
 FOR INFORMATION OR EXPLANATION CONTACT F. G. STASSINGFLUX AT JPL-A-347
 PROCTER
 TABLE OF ER (A) TOTAL FLUXES
 FOR DENSITY 25.0 DUST V
 SEE PAGE 2

ORBIT NUMBER	MAX FLUX ENCOUNTERED PCM*2/S	DURATION AT WHICH ENCOUNTERED (CEC)	LATITUDE (DEG)	ALTITUDE (KM)	SHUT-TIME (HRS)	MAX FLUX PCM*2/S	DURATION AT WHICH ENCOUNTERED (CEC)	LATITUDE (DEG)	ALTITUDE (KM)	SHUT-TIME (HRS)	MAX FLUX PCM*2/S
1	2.2426 04	-1.00.048	-16.1%	1660.73	1.12200	2.14011	1.01	4.2477	07	4.2477	07
2	2.9051 04	-11.4.07	-16.42	1565.46	3.46666	2.14011	1.01	4.6475	37	4.6475	37
3	5.058E 34	-62.0515	-24.43	1665.44	7.91667	2.13519	1.00	6.8475	37	6.8475	37
4	6.828E 04	-49.059	-16.70	1668.46	7.91667	2.13482	1.01	7.5555	37	7.5555	37
5	6.5001 04	-72.2.28	-16.94	1662.32	6.22222	2.13254	1.01	8.2232	37	8.2232	37
6	2.1561 04	-1.00.763	-13.85	1667.54	11.16667	2.14424	1.01	2.1561	37	2.1561	37
7	1.158E 04	-97.4.22	6.31	1567.14	11.16667	2.14424	1.01	1.158E	37	1.158E	37
8	1.7722 04	35.526	73.97	1559.23	1.69667	2.15493	1.02	2.6214	37	2.6214	37
9	2.803E 04	15.545	-17.58	1663.64	1.70565	2.15937	1.05	4.865E	37	4.865E	37
10	4.655E 04	-23.076	-10.94	1559.3	12.14424	2.13241	1.01	6.656E	37	6.656E	37
11	6.722E 04	-46.922	-17.33	1663.93	21.34331	2.12475	1.01	7.3214	37	7.3214	37
12	4.744F 04	-73.054	-20.97	1561.84	23.04949	2.12475	1.01	8.4227	37	8.4227	37

ORBITAL FLUX STUDY WITH COMPOSITE PARTICLE ENVIRONMENT VEHICLE APPROX ALONG EQUATOR
 UNCERTAINTY FACTORS (UF) APPLIED FOR THIS RUN ARE:
 MAGNETIC COORDINATES & L COMPUTED BY INVARA OF 1972 WITH ALL MAG. ALIGN.
 VEHICLE AND X-LISMAX ANALYSIS ALONG EQUATOR
 FOR INFORMATION OR EXPLANATION CONTACT F. G. STASSINGFLUX AT JPL-A-347
 PROCTER
 TABLE OF ER (A) TOTAL FLUXES
 FOR DENSITY 25.0 DUST V
 SEE PAGE 2

ORBIT NUMBER	MAX FLUX ENCOUNTERED PCM*2/S	DURATION AT WHICH ENCOUNTERED (CEC)	LATITUDE (DEG)	ALTITUDE (KM)	SHUT-TIME (HRS)	MAX FLUX PCM*2/S	DURATION AT WHICH ENCOUNTERED (CEC)	LATITUDE (DEG)	ALTITUDE (KM)	SHUT-TIME (HRS)	MAX FLUX PCM*2/S
1	1.921F 06	-1.00.023	-26.32	1663.30	1.15067	2.11511	1.04	2.1434	33	2.1434	33
2	2.091E 06	16.775	-8.01	1667.20	2.09333	2.11502	1.04	1.6104	33	1.6104	33
3	2.657E 06	-16.044	-14.71	1567.87	5.93433	2.13413	1.04	1.6515	33	1.6515	33
4	2.951E 06	-53.436	-26.24	1669.94	7.94002	2.12774	1.04	1.2561	34	1.2561	34
5	2.272E 06	-26.4.24	-22.62	1673.26	1.62333	2.11613	1.01	2.11613	34	2.11613	34
6	1.647F 06	-17.0.234	3.18	1666.99	9.00333	2.11377	1.04	1.6741	34	1.6741	34
7	1.020F 06	-57.1.22	4.33	1507.14	1.16667	2.11633	1.07	1.2041	34	1.2041	34
8	1.021* 06	-9.078	-8.01	1659.49	15.52222	2.11974	1.09	1.6697	34	1.6697	34
9	1.137E 06	16.946	-8.83	1559.51	16.44444	2.12711	1.04	1.5405	34	1.5405	34
10	2.761F 06	-16.741	-15.57	1669.13	19.01667	2.11377	1.04	2.7144	34	2.7144	34
11	1.007E 06	-44.513	-22.43	1662.15	21.30667	2.12743	1.04	3.2777	34	3.2777	34
12	2.033E 06	-73.0.94	-73.53	1564.30	23.04949	2.12743	1.04	3.3951	34	3.3951	34

TABLE 25

ORBITAL FLUX STUDY WITH COMPOSITE PARTICLE ENVIRONMENTS: VEHICLE: A7A AGO AT 17 APR 1979
 UNCERTAINTY FACTORS (APR) = 1.0; FPC PROJECTIONS (APR) = 1.0; UNFLUX OF 1979
 MAGNETIC COORDINATES AND LATITUDES IN VARIOUS WITH ALLMASS, MEDIUM: 4;
 VEHICLE: MAX-XIS MAX, AND ALLMASS, MEDIUM: 4;
 FOR INFORMATION OR EXPLANATION CONTACT L.S. STASSINICUUS AT NASA-USC CODE C31, GOMATI MARYLAND 20771, TEL (301)-734-6007
 PRECISE

TABLE OF PEAK AND TOTAL FLUXES WITH PERIOD: 1 MONTH 25 OCT 79

REF ID NUMBER	POSITION AT WHICH SOURCE IS LOCATED			TOTAL FLUX		
	ENCOUNTERD BY CM*2/S/C	LATITUDE (DEG)	ALTITUDE (KM)	PERIOD (CMOS)	(AUSS)	(FNU)
1	1.524E 05	-110.840	-112.36	2580.65	1.656E 7	3.134E 7
2	2.084E 05	6.494	-3.59	2594.97	4.656E 7	1.43
3	3.353E 05	-72.675	-7.59	1563.17	2.05E 7	3.35E 7
4	3.182E 05	-68.453	-15.49	2694.16	6.533E 7	7.72E 7
5	1.280E 05	-1.01.403	-11.16	2583.45	7.266E 7	5.05E 7
6	1.244E 05	-1.33.597	-4.13	2593.15	1.421E 7	4.51E 7
7	5.551E 05	24.297	-2.82	2585.85	1.233E 7	2.61E 7
8	-2.420E 05	-4.283	-4.28	2585.85	17.533E 7	1.43
9	3.490E 05	-36.018	-9.08	2580.33	20.016E 7	1.50
10	3.230E 05	-66.824	-114.20	2587.95	22.413E 7	1.51

ORBITAL FLUX STUDY WITH COMPOSITE PARTICLE ENVIRONMENTS: VEHICLE: A7A AGO AT 17 APR 1979
 UNFLUX OF 1979
 UNCERTAINTY FACTORS (APR) = 1.0; FPC PROJECTIONS (APR) = 1.0; UNFLUX OF 1979
 MAGNETIC COORDINATES AND LATITUDES IN VARIOUS WITH ALLMASS, MEDIUM: 4;
 VEHICLE: MAX-XIS MAX, AND ALLMASS, MEDIUM: 4;
 FOR INFORMATION OR EXPLANATION CONTACT L.S. STASSINICUUS AT NASA-USC CODE C31, GOMATI MARYLAND 20771, TEL (301)-734-6007
 PRECISE

TABLE OF PEAK AND TOTAL FLUXES WITH PERIOD: 1 MONTH 25 OCT 79

REF ID NUMBER	POSITION AT WHICH SOURCE IS LOCATED			TOTAL FLUX		
	ENCOUNTERD BY CM*2/S/C	LATITUDE (DEG)	ALTITUDE (KM)	PERIOD (CMOS)	(AUSS)	(FNU)
1	3.97E 06	-1.06.609	-10.74	587.07	1.30E 00	1.03E 04
2	6.455E 06	0.454	-3.59	2582.97	4.656E 7	1.65
3	6.348E 06	-27.531	-9.79	2593.36	7.266E 7	1.52
4	5.212E 06	-63.451	-15.49	2594.16	6.533E 7	1.52
5	1.136E 06	-13.564	-13.564	2586.21	1.233E 7	1.45
6	3.475E 06	-1.06.675	-1.06.675	2593.43	1.421E 7	1.52
7	4.036E 06	31.356	-1.11	2585.77	1.656E 7	1.42
8	6.721E 06	-2.895	-2.895	2585.77	1.741E 7	1.32
9	4.423E 06	-31.018	-9.08	2586.03	2.031E 7	1.49
10	5.267E 06	-66.924	-114.20	2587.07	2.241E 7	1.50

ORBITAL FLUX STUDY WITH COMPOSITE PARTICLE ENVIRONMENT: VECTORS APM-AEC, APRIL 1975
 UNCERTAINLY FACTOR (UF) APPLIED FOR THIS RUN: API = 1.0
 MAGNETIC COORDINATES (UF) AND LONGITUDES (UF) APPLIED FOR THIS RUN: AL = 1.0
 VEHICLE: INVX3-S-AXIS SPHERICAL (APOGEE = 3889 KM PERIGEE = 3841 KM)
 FOR INFORMATION OR EXPLANATION CONTACT EUGENE MELISSA MARYLAND 10546 * TIME = 10546 * PERIOD = 2077.46 * DATE = MAY 15, 1975 * 344-8067

TABLE OF PEAK AND TOTAL FLUXES PER PERIOD: ENERGY > 5000 EV

PERIOD NUMBER	PEAK FLUX ENCOUNTERED /CM ⁻² /SEC	POSITION AT WHICH ENCOUNTERED TO LONGITUDE (DEG)	POSITION AT WHICH ENCOUNTERED LATITUDE (DEG)	CABIN TIME (HOURS)	FIELD (E) (GAUSS)	LINE (L) (E.R.)	TOTAL FLUX PER GIRD /CM ⁻² /CABIN
1	7.315E 05	-116.921	-73.64	3683.25	1.21607	0.07270	1.43
2	1.031E 06	-54.559	-71.39	3885.06	5.23337	0.06554	1.782E 09
3	1.031E 05	-54.555	-11.39	3885.21	1.23169	0.06315	2.091E 09
4	9.878E 05	-97.944	-14.17	3885.75	0.09515	1.479	1.653E 09
5	9.358E 05	-136.630	-21.15	3885.07	1.43200	0.07492	1.259E 09
6	6.772E 05	-20.726	4.36	3882.80	15.7667	0.06432	1.259E 09
7	1.081E 06	-18.784	-13.39	3882.77	18.7166	0.06429	1.581E 09
8	1.120E 05	-57.750	-13.91	3883.96	21.54330	0.06330	1.731E 09

ORBITAL FLUX STUDY WITH COMPOSITE PARTICLE ENVIRONMENT: VECTORS APM-AEC, APRIL 1975
 UNCERTAINLY FACTOR (UF) APPLIED FOR THIS RUN: API = 1.0; PERIOD = 1.0; PCK INTEGRATION FUNCTIONS (APM) - UF = 1.0
 MAGNETIC COORDINATES (UF) AND LONGITUDES (UF) APPLIED FOR THIS RUN: AL = 1.0; PERIOD = 1.0; TIME = 1369.5
 VEHICLE: INVX3-S-AXIS SPHERICAL (APOGEE = 3889 KM PERIGEE = 3841 KM)
 FOR INFORMATION OR EXPLANATION CONTACT EUGENE MELISSA MARYLAND 10546 * TIME = 10546 * PERIOD = 2077.46 * DATE = MAY 15, 1975 * 344-8067

TABLE OF PEAK AND TOTAL FLUXES PER PERIOD: ENERGY > 5000 EV

PERIOD NUMBER	PEAK FLUX ENCOUNTERED /CM ⁻² /SEC	POSITION AT WHICH ENCOUNTERED TO LONGITUDE (DEG)	POSITION AT WHICH ENCOUNTERED LATITUDE (DEG)	CABIN TIME (HOURS)	FIELD (E) (GAUSS)	LINE (L) (E.R.)	TOTAL FLUX PER GIRD /CM ⁻² /CABIN
1	7.329E 06	-116.921	-8.64	3683.25	1.21667	0.07270	1.43
2	4.725E 06	-54.566	0.22	3888.73	5.70000	0.06542	2.483E 10
3	4.214E 06	-54.537	-13.17	3889.63	8.50000	0.06290	2.643E 10
4	9.318E 06	-97.970	-19.37	3889.56	1.14400	0.06954	2.093E 10
5	7.695E 06	-136.930	-21.15	3889.37	1.43400	0.07492	1.743E 10
6	9.260E 06	-20.726	4.36	3882.80	15.7667	0.06432	1.259E 09
7	9.344E 06	-18.784	-13.91	3882.77	18.7166	0.06429	1.581E 09
8	9.175E 06	-57.750	-13.91	3883.96	21.54330	0.06330	1.731E 09

TABLE 27

* SPATIAL FLUX STATION WITH COMPARISON OF EARTH'S MAGNETIC FIELD AND THE SUN'S MAGNETIC FIELD
 * UNCERTAINTY FACTORS USED ARE:
 * MAGNETIC COHERENCE AND LINEARITY 1.05
 * INCLINATION EFFECT 0.95
 * INFLUENCE OF NEARBY SOURCES 0.95
 * INFLUENCE OF EXTRAPOLATION 0.95
 * INFLUENCE OF FLUX DENSITY 0.95
 * TOTAL FLUX 0.95

	PERIOD NUMBER	PEAK FLUX AMOUNT (EFC)	POSITION & WHITE POINT CENTER LATITUDE ALTITUDE (EFC)	WEIGHT (EFC)	WEIGHT (EFC)	WEIGHT (EFC)
1	103751	56	-162°45'	5.0	1.0	1.0
2	103751	56	-162°45'	5.0	1.0	1.0
3	103751	56	-162°45'	5.0	1.0	1.0
4	103751	56	-162°45'	5.0	1.0	1.0
5	103751	56	-162°45'	5.0	1.0	1.0
6	103751	56	-162°45'	5.0	1.0	1.0
7	103751	56	-162°45'	5.0	1.0	1.0

* SPATIAL FLUX STATION WITH COMPARISON OF EARTH'S MAGNETIC FIELD AND THE SUN'S MAGNETIC FIELD
 * UNCERTAINTY FACTORS USED ARE:
 * MAGNETIC COHERENCE AND LINEARITY 1.05
 * INCLINATION EFFECT 0.95
 * INFLUENCE OF NEARBY SOURCES 0.95
 * INFLUENCE OF EXTRAPOLATION 0.95
 * INFLUENCE OF FLUX DENSITY 0.95
 * TOTAL FLUX 0.95

	PERIOD NUMBER	PEAK FLUX AMOUNT (EFC)	POSITION & WHITE POINT CENTER LATITUDE ALTITUDE (EFC)	WEIGHT (EFC)	WEIGHT (EFC)	WEIGHT (EFC)
1	103451	57	-162°41'	5.0	1.0	1.0
2	103451	57	-162°41'	5.0	1.0	1.0
3	103451	57	-162°41'	5.0	1.0	1.0
4	103451	57	-162°41'	5.0	1.0	1.0
5	103451	57	-162°41'	5.0	1.0	1.0
6	103451	57	-162°41'	5.0	1.0	1.0

TABLE 20

EXPT NO.	NUMBER	SIGHTING		WHICH ENCOUNTERED		CLOUD TIME	FIELD (L)	LINE (L)	TOTAL FLUX PER ORBIT #/C 4442/C 311
		LATITUDE (DEG.)	LONGITUDE (DEG.)	LATITUDE (DEG.)	ALTITUDE (KM.)				
1	4-462	34	81-550	80-66	10371.4	0-41667	2-61771	2-61	1-514E-25
2	4-21105	65	122-678	13-54	10372.3	0-78333	0-01110	2-58	1-346E-25
3	4-6646	34	74-227	10-35	10371.35	14-68333	2-01655	2-58	7-05E-25
4	4-6521	34	172-241	5-77	10371.14	14-20331	2-01771	2-58	1-012E-25

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DEPIA FLUX STUDY WITH MOBILE PARTICLE ENVIRONMENT: VETTES AFU ACO, ALIT HOF, LAF, NAVY
 INJECTIVITY FACTORS OF APOLLO FUELS, BUN AR; FOR FECTS CAL-1-10; FILE NO.
 MAGNETIC CORDINATE AND LOCALIZATION IN INAN ME 1972, 1972, 1972, 1972, 1972,
 EFFECTIVE EFFECTIVE EFFECTIVE EFFECTIVE EFFECTIVE EFFECTIVE EFFECTIVE EFFECTIVE
 FOR INFORMATION ON EXPANSION CONTACTS, STAINLESS STEEL, STAINLESS STEEL, STAINLESS STEEL,
 TOTAL FLUXES FILE NUMBER: DEPIA
 AFU, EAK AND DEPIA

DETECTION NUMBER	DETECTION UNCERTAINTY (μ A cm^{-2})	POSITION AT WHICH ACCURATE LATITUDE AND ALTITUDE (km)		(KFT TIME (hr:min))	FIFI (cm) (CMB)	FIFI (cm) (Eof +)	INITIAL FLUX AT ORBIT #C4442/C4311
		LATITUDE (deg)	ALTITUDE (km)				
1	3.6710	66	-26.46	1037.46	0.4205	0.655	4.624E-16
2	3.6710	66	-11.757	43.74	0.4113	0.545	5.576E-16
3	3.6710	66	46.57	1037.46	0.4205	0.545	5.576E-16
4	3.6710	36	-19.19	1037.46	0.4205	0.24	2.052E-16
			-30.077	1037.46	0.4205	0.011	2.027E-16

TABLE 30

TABLE 31

TABLE -
NVL : S-MAX
CALCULATED

INCLINATION: 60 DEG		INCLINATION: 60 DEG			
PERIGEE: 1667 KM		PERIGEE: 1667 KM			
APOGEE: 1667 KM		APOGEE: 1667 KM			
***** EXPENSE ANALYSIS *****					
* PERCENT OF TOTAL LIFE TIME SPENT INSIDE AND *					
* OUTSIDE THE TRAPPED-PARTICLE RADIATION BELT *					
PERIODS	EXCEPTIONS L.	INTEGRAL ZONE	-W- : 67.99 %		
(E>500 MEV)	(E>500 MEV)	(1.0 < L < 2.0)			
PERCENT OF TOTAL LIFE- TIME SPENT IN FLUX-FREE REGIONS OF SPACE	2.16 %	CUTOFF ZONE -10-	30.35 %		
PERCENT OF TOTAL LIFE- TIME SPENT IN HIGH- INTENSITY REGIONS OF VAN ALLEN BELTS	49.47 %	EXTERNAL -TE- : 1.67 %			
PERCENT OF TOTAL DAILY FLUX ACCUMULATED IN HIGH-INTENSITY REGIONS:	54.31 %	(L > 11.0)			
***** TIME IN INNER ZONE WAY OFF SUBDIVIDED AS FOLLOWS:*****					
OUTSIDE TRAPPING REGION :		JUPITER TRAPPING REGION :	60.9 %		
(1.0 < L < 1.1)		(1.1 < L < 2.0)			
INSIDE TRAPPING REGION :		INSIDE TRAPPING REGION :	67.99 %		

* < 1 PARTICLE /CM**2/S C					
* > 1.65 FL/CM**2/SFC (F. 1.65 PP/C M**2/SFC)					

TABLE 32

PERCENT OF TOTAL DAILY FLUX ACCUMULATED IN ALBEDOLESS SURFACE REGIONS:		PERCENT OF TOTAL DAILY FLUX ACCUMULATED IN ALBEDOLESS SURFACE REGIONS:	
OUTSIDE TRAPPED-PARTICLE FACILITATION BELT:	100.0%	OUTSIDE TRAPPED-PARTICLE FACILITATION BELT:	100.0%
($1.0 < L < 2.0$)	100.0%	($1.0 < L < 2.0$)	100.0%
INSIDE TRAPPED-PARTICLE FACILITATION BELT:	100.0%	INSIDE TRAPPED-PARTICLE FACILITATION BELT:	100.0%
($1.0 < L < 2.0$)	100.0%	($1.0 < L < 2.0$)	100.0%
PERCENT OF TOTAL LIFT-TIME SPENT INSIDE AND OUTSIDE THE TRAPPED-PARTICLE FACILITATION BELT:		PERCENT OF TOTAL LIFT-TIME SPENT INSIDE AND OUTSIDE THE TRAPPED-PARTICLE FACILITATION BELT:	
FLUX DENSITY, cm^{-2}	FLUX DENSITY, cm^{-2}	FLUX DENSITY, cm^{-2}	FLUX DENSITY, cm^{-2}
INCLINATION: 0 DEG	INCLINATION: 0 DEG	INCLINATION: 0 DEG	INCLINATION: 0 DEG
OUTSIDE : 25.93 KM	OUTSIDE : 25.93 KM	OUTSIDE : 25.93 KM	OUTSIDE : 25.93 KM
INSIDE : 25.93 KM	INSIDE : 25.93 KM	INSIDE : 25.93 KM	INSIDE : 25.93 KM
***** EXPERT ANALYSIS *****			
PERCENT OF TOTAL LIFT-TIME SPENT IN HIGH-INTENSITY REGIONS OF SPACE:	62.31 %	PERCENT OF TOTAL LIFT-TIME SPENT IN HIGH-INTENSITY REGIONS OF SPACE:	77.01 %
PERCENT OF TOTAL LIFT-TIME SPENT IN FLUX-FILTER REGIONS OF SPACE:	26.30 %	PERCENT OF TOTAL LIFT-TIME SPENT IN FLUX-FILTER REGIONS OF SPACE:	22.02 %
PERCENT OF TOTAL LIFT-TIME SPENT IN HIGH-INTENSITY REGIONS OF SPACE:	11.39 %	PERCENT OF TOTAL LIFT-TIME SPENT IN HIGH-INTENSITY REGIONS OF SPACE:	10.98 %
PERCENT OF TOTAL DAILY FLUX ACCUMULATED IN ALBEDOLESS SURFACE REGIONS:	100.00 %	PERCENT OF TOTAL DAILY FLUX ACCUMULATED IN ALBEDOLESS SURFACE REGIONS:	100.00 %
OUTSIDE TRAPPED-PARTICLE FACILITATION BELT:	100.00 %	OUTSIDE TRAPPED-PARTICLE FACILITATION BELT:	100.00 %
($1.0 < L < 2.0$)	100.00 %	($1.0 < L < 2.0$)	100.00 %
INSIDE TRAPPED-PARTICLE FACILITATION BELT:	100.00 %	INSIDE TRAPPED-PARTICLE FACILITATION BELT:	100.00 %
($1.0 < L < 2.0$)	100.00 %	($1.0 < L < 2.0$)	100.00 %

* <1 PARTICLE /CM*2/SEC		* <1 PARTICLE /CM*2/SEC	
* >1.E5 FLUXES/SEC FOR 1.E3 PF/CM*2/SEC		* >1.E5 FLUXES/SEC FOR 1.E3 PF/CM*2/SEC	

TABLE -

MVIX3:S-MAX
CIRCULAR
INCLINATION: 60 DEG
PERIGEE: 3889 KM
APOGEE: 3889 KM

**** EXPOSURE ANALYSIS ****

PROTONS	ELECTRONS LO (E>5.000MEV)
PERCENT OF TOTAL LIFE- TIME SPENT IN FLUX-PRE- REGIONS* OF SPACE :	30.14 %
PERCENT OF TOTAL LIFE- TIME SPENT IN HIGH- INTENSITY REGIONS+ OF VAN ALLEN BELTS :	57.92 %
PERCENT OF TOTAL DAILY FLUX ACCUMULATED IN HIGH-INTENSITY REGIONS:	99.98 %

* PERCENT OF TOTAL LIFETIME SPENT INSIDE AND
* OUTSIDE THE TRAPPED-PARTICLE RADIATION BELT *

INNER ZONE -TI- : (1.0 < L < 2.6)	54.51 %
CUTTER ZONE -TO- : (2.8 < L < 11.0)	42.08 %
EXTERNAL -TE- : (L > 11.0)	3.40 %
TOTAL : *****	100.00 %

* TIME IN INNER ZONE MAY BE SUBDIVIDED AS FOLLOWS:

OUTSIDE TRAPPING REGION : (1.0 < L < 1.1)	0.0 %
INSIDE TRAPPING REGION : (1.1 < L < 2.6)	54.51 %

- * <1 PARTICLE/CM**2/SEC
- + >1.E5 EL/CM**2/SEC OR 1.E3 RAD/CM**2/SEC

TABLE 33

TABLE 34

INCLINATION: EC CEG		PERIGEE: 6166 KM		APOGEE: 6166 KM		PERCENT OF TOTAL LIFETIME SPENT IN SIGHT AT DISTANCE THE TRAJECTORY-NIGHT FADEOUT SELV *	
FFC1CNS	ELFFCCNS LLC	(E>5000MEV)	(E>5000MEV)	INTER ZONE - 11-9	42.9%	INTER ZONE - 11-9	42.9%
PERCENT OF TOTAL LIFE-				11.0 < L < 20.0		11.0 < L < 20.0	
TIME SPENT IN FLUX-FREE				OLTR ZONE - 10-	46.6%	OLTR ZONE - 10-	46.6%
REGIONS OF SPACE				10.0 < L < 11.0		10.0 < L < 11.0	
PERCENT OF TOTAL LIFE-				EXTERNAL - 10-	2.00%	EXTERNAL - 10-	2.00%
TIME SPENT IN HIGH-				(L > 11.0)		(L > 11.0)	
INTENSITY REGIONS OF				TOTAL	: 100.00 %	TOTAL	: 100.00 %
VAN ALLEN BELTS :				87.67 %		87.67 %	
PERCENT OF TOTAL DAILY							
FLUX ACCUMULATED IN							
HIGH-INTENSITY-REGIONS							

* TIME IN INTER ZONE MAY BE SUBDIVIDED AS FOLLOWS:							
JUXTA TRAJECTORY REGION : COG *							
(1.0 < L < 1.1)							
INTER TRAJECTORY REGION : 48.33 %							
(1.1 < L < 2.0)							

* <1 PARTICLE/CM**2/SEC							
+ >1.E: ELS/CM**2/SEC OF 1.03 PR/CM**2/SEC							

TABLE 35

***** SURVEY ANALYSIS *****

Seconds of Space	Van Allen Belts (%)	Percent of Total Carry Flux (%)	Time Spent in Each Region (%)	Intensity Regions (%)
0	0	0	0	0
50	10	10	10	10
100	20	20	20	20
150	30	30	30	30
200	40	40	40	40
250	50	50	50	50

***** SURVEY ANALYSIS *****

TABLE I
TABLE II

TABLE -		
WAVELENGTH-MAX		
CIRCULAR		
INTERACTION : 40 DEG		
INTERFERER : 0.365 KM		
ARM-LEN : 6.789 KM		
* PERCENT OF TOTAL RECEIVING SPOTLIGHT INSIDE AND *		
* OUTSIDE THE OPTICAL-ABSTRACT RADIATION FIELD *		
WAVELENGTH-INTER- : 42.36 X		
(1.0 < L < 2.0)		
OUTSIDE RADIATION - 1E- : 51.64 X		
(2.0 < L < 11.0)		
EXTERRAL - 1E- : 6.09 X		
(L > 11.0)		
TOTAL : 100.00 X		
* TRUE IN THIS CASE MAYBE DIVIDED AS FOLLOWS:		
OUTSIDE RADIATING REGION : C.G X		
(1.0 < L < 1.0)		
INSIDE RADIATING REGION : C.G X		
(1.0 < L < 2.0)		

TABLE 36

TABLE -

TIME SPENT IN SPACE		TIME SPENT IN AIR		TIME SPENT IN WATER		
INERTIAL	1e-03	1.000	0.000	0.000	0.000	
ROTATIONAL	1e-03	0.000	1.000	0.000	0.000	
TRANSLATIONAL	1e-03	0.000	0.000	1.000	0.000	
TRANSLATIONAL ROTATIONAL	1e-03	0.000	0.000	0.000	1.000	
TRANSLATIONAL INERTIAL	1e-03	0.000	0.000	0.000	1.000	
TRANSLATIONAL ROTATIONAL INERTIAL	1e-03	0.000	0.000	0.000	1.000	
<hr/>						
PERCENT OF TOTAL TIME						
TIME SPENT IN FLIGHT	1.000	2	1.000	2	1.000	2
PERCENTAGE OF SPACE	1.000	2	1.000	2	1.000	2
PERCENT OF TOTAL TIME	1.000	2	1.000	2	1.000	2
TIME SPENT IN FLIGHT	1.000	2	1.000	2	1.000	2
INTENSITY RECEIVED	1.000	2	1.000	2	1.000	2
VAN ALLEN BELTS	1.000	2	1.000	2	1.000	2
PERCENT OF TOTAL DAILY						
FLUX ACCUMULATED IN						
ACCELERATION REGION						
INTERPLANETARY REGION						
INTERSTELLAR REGION						
<hr/>						
ACTUAL TRANSPORT POSITION :	C.C.	x				
(1.0 < r < 1.1)						
IDEAL TRANSPORT POSITION :	1e+00	x				
(1.1 < r < 1.2)						
<hr/>						
* 1.000 = 1.000 E/SOL						
+ 1.000 = 1.000 E/SEC						

ORBITAL FLUX STUDY WITH COMPOSITE PARTICLE ENVIRONMENT. VELLES, ABIA ALB, AEL7 FOR SOLAR MAXIMUM UNFLUX CF 1979
 UNCERTAINTY FACTORS (UF) APPLIED FOR THIS RUN ARE: FOR PARTICLES (APB) ALB, UF = 1.0; FOR INNER ZONE ELECTRONS, UF = 1.0
 MAGNETIC COORDINATES (B AND L COMPUTED BY INVARA OF 1972 WITH ALLHAG MODEL 4); HARRACOUGH ET AL. IC-TRM 1975 TIME = 199.5
 MAXIMALE: MAXIMUM DENSITY AT EQUATORIAL DISTANCE 1.65ZKM. ADOPTED DENSITY PROFILE: JOURNAL OF GEOPHYSICAL RESEARCH 1995
 FOR INFORMATION OR COMMUNICATION CONTACT E.G. STASSI KOPOULOS, AI NASA-GSFC, CODE 601, GREENBELT, MARYLAND 20771, TEL. (301) - 944-8067
 ENERGY FLUXES FOR ENERGETIC SOLAR PROTON PLUME
 FOR CUT OFF DIPOLE SHELL L = 5, ER =
 PARTICLES (APB) 2

ENERGY LEVELS (MEV)	MISSION DURATION T=60 MONTHS			GEOMAGNETIC SHIELDING		
	80	85	90	95	99	100
10.0	5.636E 05	5.636E 05	7.515E 05	9.394E 05	1.315E 05	1.618
20.0	3.065E 09	3.065E 09	5.153E 09	6.402E 09	9.017E 09	11.18
30.0	2.005E 09	2.005E 09	3.933E 09	6.616E 09	9.163E 09	12.0
40.0	1.027E 09	1.027E 09	2.423E 09	3.008E 09	4.239E 09	7.71
50.0	1.124E 05	1.246E 05	1.661E 05	2.046E 05	2.507E 05	5.76
60.0	8.532E 06	8.542E 06	1.136E 06	1.424E 06	1.593E 06	0.9
70.0	7.000E 06	5.857E 06	7.809E 06	9.762E 06	1.267E 06	0.9
80.0	4.016E 06	4.016E 06	5.355E 06	6.604E 06	8.321E 06	0.9
90.0	2.154E 06	2.754E 06	3.671E 06	4.595E 06	6.425E 06	0.9
100.0	1.158E 06	1.889E 06	2.517E 06	3.197E 06	4.405E 06	0.9
110.0	1.219E 06	1.219E 06	2.572E 06	3.122E 06	3.021E 06	0.9
120.0	8.027E 07	8.877E 07	1.164E 08	1.494E 08	2.071E 08	0.9
130.0	6.016E 07	6.089E 07	8.115E 07	1.034E 08	1.420E 08	0.9
140.0	4.173E 07	4.173E 07	5.567E 07	6.955E 07	9.738E 07	0.9
150.0	2.882E 07	2.882E 07	3.815E 07	4.709E 07	6.677E 07	0.9
160.0	1.902E 07	1.902E 07	2.616E 07	3.224E 07	4.528E 07	0.9
170.0	1.345E 07	1.345E 07	1.794E 07	2.242E 07	3.139E 07	0.9
180.0	9.224E 06	9.224E 06	1.230E 07	1.537E 07	2.152E 07	0.9
190.0	6.322E 06	6.322E 06	8.653E 06	1.054E 07	1.477E 07	0.9
200.0	4.337E 06	4.337E 06	5.782E 06	7.228E 06	1.012E 07	0.9

TABLE 37

DRAFT. UNFINISHED. WITH COMPOSITE PARTICLE ENVIRONMENT. APB: AEB, AEL FOR SOLAR MAXIMUM UNIFORMITY FACTORS (UF) APPLIED FOR THIS RUN ARE: FOR PROTONS (APB) - UF = 1.0; FOR INNEF7ZONE ELECTRONS (AEL) - UF = 1.0; FOR ALL MAG. MODEL A: BARRACLOUD ET AL. 1975. TIME = 1989.5 SEC. MAGNETIC COORDINATES B AND L COMPUTED BY L. INVARA OF 1972 WITH ALL MAG. MODEL A. GEODESIC LONGITUDE = 250.0 KM. INCIDENCE ANGLE = 25.0 DEG. AT 250.0 KM. DUBL. IADE. IDEAS 6.2A. DEOLCO 1.4A. FOR INFORMATION OR EXPLANATION CONTACT E.G. STASSHOULCS AT NASA-GSFC, CODE 601, GREENBELT, MARYLAND 20771. TEL (301)-346-8067.

***** ENERGY SOLAR PROTON FLUX *****

***** FOR CUT OFF DIPOLE SHELL, L = 5 ER *****

***** PARTICLES (2) *****

***** EMISSION DURATION T=60. MCNT95 *****

ENERGY L/THERS EV	CONFIDENCE LEVEL G(x)		95	99	GEOMAGNETIC SHIELDING	
	80	85			DIPOLE CLIFF SHELL	PERCENT EXPOSURE TIME
10.0	6.651E 09	6.651E 09	8.868E 19	1.039E 10	1.552E 10	L.24
20.0	4.561E 09	4.561E 09	6.081E 19	7.001E 19	1.064E 10	L.25
30.0	3.012E 09	3.012E 09	4.169E 19	5.212E 19	7.294E 19	L.26
40.0	2.144E 09	2.144E 09	2.859E 19	3.374E 19	5.003E 09	L.27
50.0	1.470E 09	1.470E 09	1.960E 19	2.450E 19	3.430E 09	-
60.0	1.008E 09	1.008E 09	1.344E 19	1.680E 19	2.352E 09	-
70.0	6.912E 08	6.912E 08	9.216E 18	1.152E 19	1.612E 09	-
80.0	4.236E 08	4.236E 08	6.140E 18	7.890E 18	1.106E 09	-
90.0	3.250E 08	3.250E 08	4.333E 18	5.166E 18	7.582E 08	-
100.0	2.228E 08	2.228E 08	2.971E 18	3.714E 18	5.199E 08	-
110.0	1.523E 08	1.523E 08	2.037E 18	2.536E 18	3.503E 08	-
120.0	1.042E 08	1.042E 08	1.397E 18	1.744E 18	2.444E 08	-
130.0	7.183E 07	7.183E 07	9.577E 17	1.197E 18	1.676E 08	-
140.0	4.932E 07	4.932E 07	6.267E 17	8.08E 17	1.149E 08	-
150.0	3.372E 07	3.372E 07	4.503E 17	5.628E 17	7.879E 07	-
160.0	2.315E 07	2.315E 07	3.082E 17	3.859E 17	5.403E 07	-
170.0	1.588E 07	1.588E 07	2.117E 17	2.646E 17	3.704E 07	-
180.0	1.089E 07	1.089E 07	1.451E 17	1.814E 17	2.540E 07	-
190.0	7.498E 06	7.498E 06	9.952E 16	1.244E 17	1.742E 07	-
200.0	5.118E 06	5.118E 06	6.824E 16	8.530E 16	1.194E 07	-

TABLE 30

ORBITAL FLUX STUDY WITH COMPOSITE PARTICLE ENVIRONMENTS: VENUS APhi AZ= ARI7 FOR SOLAR MAXIMUM UNILUA UP 1973
 FOR PROTONS (UP) - UPE= 1.0; FOR INNER ZECKE ELECTRONS (Aphi) - UP= 1.0
 UNCERTAINTY FACTORS (UP) APPLIED TO THIS RUN ARE:
 MAGNETIC COORDINATES (B) AND L COMPUTED BY INVARA OF 1972 WITH ALLMAG MODEL 4;
 VEHICLE: MILX3; S-MAX INCLINATION= 30DEG; STASSINOPOULOS CONTACT E.G.;
 FOR INFORMATION OR EXPLANATION OF THE ABOVE,
 ENERGY SOLAR PROTON FLUXE
 FOR CUTCFP DIPOLES SHELL L=5.2A
 FOR CUTCFP DIPOLES/C SHELL L=5.2A

ENERGY LEVELS >(REV)	MISSION DURATION T=60, MONTHS		99
	80	65	
10.0	8.7367E 0.9	9.3672E 0.9	1.116E 0.9
20.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
30.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
40.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
50.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
60.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
70.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
80.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
90.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
100.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
110.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
120.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
130.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
140.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
150.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
160.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
170.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
180.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
190.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9
200.0	8.7345E 0.9	9.3672E 0.9	1.116E 0.9

GROMAGNETIC SHIELDING
 DIPOLE
 COEFF.
 SHELL

	1.339E 10	1.339E 10	1.339E 10
1.0	1.339E 10	1.339E 10	1.339E 10
1.5	1.339E 10	1.339E 10	1.339E 10
2.0	1.339E 10	1.339E 10	1.339E 10
2.5	1.339E 10	1.339E 10	1.339E 10
3.0	1.339E 10	1.339E 10	1.339E 10
3.5	1.339E 10	1.339E 10	1.339E 10
4.0	1.339E 10	1.339E 10	1.339E 10
4.5	1.339E 10	1.339E 10	1.339E 10
5.0	1.339E 10	1.339E 10	1.339E 10
5.5	1.339E 10	1.339E 10	1.339E 10
6.0	1.339E 10	1.339E 10	1.339E 10
6.5	1.339E 10	1.339E 10	1.339E 10
7.0	1.339E 10	1.339E 10	1.339E 10
7.5	1.339E 10	1.339E 10	1.339E 10
8.0	1.339E 10	1.339E 10	1.339E 10
8.5	1.339E 10	1.339E 10	1.339E 10
9.0	1.339E 10	1.339E 10	1.339E 10
9.5	1.339E 10	1.339E 10	1.339E 10
10.0	1.339E 10	1.339E 10	1.339E 10
10.5	1.339E 10	1.339E 10	1.339E 10
11.0	1.339E 10	1.339E 10	1.339E 10
11.5	1.339E 10	1.339E 10	1.339E 10
12.0	1.339E 10	1.339E 10	1.339E 10
12.5	1.339E 10	1.339E 10	1.339E 10
13.0	1.339E 10	1.339E 10	1.339E 10
13.5	1.339E 10	1.339E 10	1.339E 10
14.0	1.339E 10	1.339E 10	1.339E 10
14.5	1.339E 10	1.339E 10	1.339E 10
15.0	1.339E 10	1.339E 10	1.339E 10
15.5	1.339E 10	1.339E 10	1.339E 10
16.0	1.339E 10	1.339E 10	1.339E 10
16.5	1.339E 10	1.339E 10	1.339E 10
17.0	1.339E 10	1.339E 10	1.339E 10
17.5	1.339E 10	1.339E 10	1.339E 10
18.0	1.339E 10	1.339E 10	1.339E 10
18.5	1.339E 10	1.339E 10	1.339E 10
19.0	1.339E 10	1.339E 10	1.339E 10
19.5	1.339E 10	1.339E 10	1.339E 10
20.0	1.339E 10	1.339E 10	1.339E 10

TABLE 39

ENERGY LEVELS 21 MEV	E-3	EE	EFFICIENCY (%)	NUMBER OF MONTHS
100 C	1.001E+10	1.001E+10	1.000E+00	1.000E+00
200 C	1.000E+09	1.000E+09	1.000E+00	1.000E+00
200 C	4.000E+07	4.000E+07	1.000E+00	1.000E+00
400 C	1.000E+06	1.000E+06	1.000E+00	1.000E+00
800 C	1.000E+05	1.000E+05	1.000E+00	1.000E+00
1600 C	1.000E+04	1.000E+04	1.000E+00	1.000E+00
3200 C	1.000E+03	1.000E+03	1.000E+00	1.000E+00
6400 C	1.000E+02	1.000E+02	1.000E+00	1.000E+00
12800 C	1.000E+01	1.000E+01	1.000E+00	1.000E+00
25600 C	1.000E+00	1.000E+00	1.000E+00	1.000E+00
51200 C	1.000E-01	1.000E-01	1.000E+00	1.000E+00
102400 C	1.000E-02	1.000E-02	1.000E+00	1.000E+00
204800 C	1.000E-03	1.000E-03	1.000E+00	1.000E+00
409600 C	1.000E-04	1.000E-04	1.000E+00	1.000E+00
819200 C	1.000E-05	1.000E-05	1.000E+00	1.000E+00
1638400 C	1.000E-06	1.000E-06	1.000E+00	1.000E+00
3276800 C	1.000E-07	1.000E-07	1.000E+00	1.000E+00
6553600 C	1.000E-08	1.000E-08	1.000E+00	1.000E+00
13107200 C	1.000E-09	1.000E-09	1.000E+00	1.000E+00
26214400 C	1.000E-10	1.000E-10	1.000E+00	1.000E+00
52428800 C	1.000E-11	1.000E-11	1.000E+00	1.000E+00
104857600 C	1.000E-12	1.000E-12	1.000E+00	1.000E+00
209715200 C	1.000E-13	1.000E-13	1.000E+00	1.000E+00
419430400 C	1.000E-14	1.000E-14	1.000E+00	1.000E+00
838860800 C	1.000E-15	1.000E-15	1.000E+00	1.000E+00
1677721600 C	1.000E-16	1.000E-16	1.000E+00	1.000E+00
3355443200 C	1.000E-17	1.000E-17	1.000E+00	1.000E+00
6710886400 C	1.000E-18	1.000E-18	1.000E+00	1.000E+00
13421772800 C	1.000E-19	1.000E-19	1.000E+00	1.000E+00
26843545600 C	1.000E-20	1.000E-20	1.000E+00	1.000E+00
53687091200 C	1.000E-21	1.000E-21	1.000E+00	1.000E+00
107374182400 C	1.000E-22	1.000E-22	1.000E+00	1.000E+00
214748364800 C	1.000E-23	1.000E-23	1.000E+00	1.000E+00
429496729600 C	1.000E-24	1.000E-24	1.000E+00	1.000E+00
858993459200 C	1.000E-25	1.000E-25	1.000E+00	1.000E+00
1717986918400 C	1.000E-26	1.000E-26	1.000E+00	1.000E+00
3435973836800 C	1.000E-27	1.000E-27	1.000E+00	1.000E+00
6871947673600 C	1.000E-28	1.000E-28	1.000E+00	1.000E+00
13743895347200 C	1.000E-29	1.000E-29	1.000E+00	1.000E+00
27487788694400 C	1.000E-30	1.000E-30	1.000E+00	1.000E+00
54975577388800 C	1.000E-31	1.000E-31	1.000E+00	1.000E+00
109951154777600 C	1.000E-32	1.000E-32	1.000E+00	1.000E+00
219902309555200 C	1.000E-33	1.000E-33	1.000E+00	1.000E+00
439804619110400 C	1.000E-34	1.000E-34	1.000E+00	1.000E+00
879609238220800 C	1.000E-35	1.000E-35	1.000E+00	1.000E+00
1759218476441600 C	1.000E-36	1.000E-36	1.000E+00	1.000E+00
3518436952883200 C	1.000E-37	1.000E-37	1.000E+00	1.000E+00
7036873855766400 C	1.000E-38	1.000E-38	1.000E+00	1.000E+00
14073747711532800 C	1.000E-39	1.000E-39	1.000E+00	1.000E+00
28147495423065600 C	1.000E-40	1.000E-40	1.000E+00	1.000E+00
56294988846131200 C	1.000E-41	1.000E-41	1.000E+00	1.000E+00
112589977692262400 C	1.000E-42	1.000E-42	1.000E+00	1.000E+00
225179955384524800 C	1.000E-43	1.000E-43	1.000E+00	1.000E+00
450359910769049600 C	1.000E-44	1.000E-44	1.000E+00	1.000E+00
900719821538099200 C	1.000E-45	1.000E-45	1.000E+00	1.000E+00
1801439643076198400 C	1.000E-46	1.000E-46	1.000E+00	1.000E+00
3602879286152396800 C	1.000E-47	1.000E-47	1.000E+00	1.000E+00
7205758572304793600 C	1.000E-48	1.000E-48	1.000E+00	1.000E+00
1441151714460987200 C	1.000E-49	1.000E-49	1.000E+00	1.000E+00
2882303428921974400 C	1.000E-50	1.000E-50	1.000E+00	1.000E+00
5764606857843948800 C	1.000E-51	1.000E-51	1.000E+00	1.000E+00
1152921375688789600 C	1.000E-52	1.000E-52	1.000E+00	1.000E+00
2305842751377579200 C	1.000E-53	1.000E-53	1.000E+00	1.000E+00
4611685502755158400 C	1.000E-54	1.000E-54	1.000E+00	1.000E+00
9223371005510316800 C	1.000E-55	1.000E-55	1.000E+00	1.000E+00
1844674201052063200 C	1.000E-56	1.000E-56	1.000E+00	1.000E+00
3689348402104126400 C	1.000E-57	1.000E-57	1.000E+00	1.000E+00
7378696804208252800 C	1.000E-58	1.000E-58	1.000E+00	1.000E+00
1475739360841655600 C	1.000E-59	1.000E-59	1.000E+00	1.000E+00
2951478721683311200 C	1.000E-60	1.000E-60	1.000E+00	1.000E+00
5902957443366622400 C	1.000E-61	1.000E-61	1.000E+00	1.000E+00
1180591488673344800 C	1.000E-62	1.000E-62	1.000E+00	1.000E+00
2361182977346689600 C	1.000E-63	1.000E-63	1.000E+00	1.000E+00
4722365954693379200 C	1.000E-64	1.000E-64	1.000E+00	1.000E+00
9444731909386758400 C	1.000E-65	1.000E-65	1.000E+00	1.000E+00
18889463818773516800 C	1.000E-66	1.000E-66	1.000E+00	1.000E+00
37778927637547033600 C	1.000E-67	1.000E-67	1.000E+00	1.000E+00
75557855275094067200 C	1.000E-68	1.000E-68	1.000E+00	1.000E+00
15111571050188134400 C	1.000E-69	1.000E-69	1.000E+00	1.000E+00
30223142100376268800 C	1.000E-70	1.000E-70	1.000E+00	1.000E+00
60446284200752537600 C	1.000E-71	1.000E-71	1.000E+00	1.000E+00
120892568401505075200 C	1.000E-72	1.000E-72	1.000E+00	1.000E+00
241785136803010150400 C	1.000E-73	1.000E-73	1.000E+00	1.000E+00
483570273606020300800 C	1.000E-74	1.000E-74	1.000E+00	1.000E+00
967140547212040601600 C	1.000E-75	1.000E-75	1.000E+00	1.000E+00
193428109424081203200 C	1.000E-76	1.000E-76	1.000E+00	1.000E+00
386856218848162406400 C	1.000E-77	1.000E-77	1.000E+00	1.000E+00
773712437696324812800 C	1.000E-78	1.000E-78	1.000E+00	1.000E+00
1547424675392649625600 C	1.000E-79	1.000E-79	1.000E+00	1.000E+00
3094849350785299251200 C	1.000E-80	1.000E-80	1.000E+00	1.000E+00
6189698701570598502400 C	1.000E-81	1.000E-81	1.000E+00	1.000E+00
1237939740341197704800 C	1.000E-82	1.000E-82	1.000E+00	1.000E+00
2475879480682395409600 C	1.000E-83	1.000E-83	1.000E+00	1.000E+00
4951758961364790819200 C	1.000E-84	1.000E-84	1.000E+00	1.000E+00
9903517922729581638400 C	1.000E-85	1.000E-85	1.000E+00	1.000E+00
19807035845451763276800 C	1.000E-86	1.000E-86	1.000E+00	1.000E+00
39614071690903526553600 C	1.000E-87	1.000E-87	1.000E+00	1.000E+00
79228143381807053107200 C	1.000E-88	1.000E-88	1.000E+00	1.000E+00
15845626676361410614400 C	1.000E-89	1.000E-89	1.000E+00	1.000E+00
31691253352722821228800 C	1.000E-90	1.000E-90	1.000E+00	1.000E+00
63382506705445642457600 C	1.000E-91	1.000E-91	1.000E+00	1.000E+00
12676501341088888915200 C	1.000E-92	1.000E-92	1.000E+00	1.000E+00
25353002682177777830400 C	1.000E-93	1.000E-93	1.000E+00	1.000E+00
50706005364355555660800 C	1.000E-94	1.000E-94	1.000E+00	1.000E+00
101412010728711111321600 C	1.000E-95	1.000E-95	1.000E+00	1.000E+00
202824021457422222643200 C	1.000E-96	1.000E-96	1.000E+00	1.000E+00
405648042914844445286400 C	1.000E-97	1.000E-97	1.000E+00	1.000E+00
811296085829688890572800 C	1.000E-98	1.000E-98	1.000E+00	1.000E+00
1622592171659377781155600 C	1.000E-99	1.000E-99	1.000E+00	1.000E+00
3245184343318755562311200 C	1.000E-100	1.000E-100	1.000E+00	1.000E+00
6490368686637511124622400 C	1.000E-101	1.000E-101	1.000E+00	1.000E+00
1298073737327502249244800 C	1.000E-102	1.000E-102	1.000E+00	1.000E+00
2596147474655004498489600 C	1.000E-103	1.000E-103	1.000E+00	1.000E+00
5192294949310008977779200 C	1.000E-104	1.000E-104	1.000E+00	1.000E+00
10384589896200175555558400 C	1.000E-105	1.000E-105	1.000E+00	1.000E+00
20769179792400351111116800 C	1.000E-106	1.000E-106	1.000E+00	1.000E+00
41538359584800702222233600 C	1.000E-107	1.000E-107	1.000E+00	1.000E+00
83076719169601404444467200 C	1.000E-108	1.000E-108	1.000E+00	1.000E+00
16615343833920280888934400 C	1.000E-109	1.000E-109	1.000E+00	1.000E+00
33230687667840561777868800 C	1.000E-110	1.000E-110	1.000E+00	1.000E+00
66461375335681123555737600 C	1.000E-111	1.000E-111	1.000E+00	1.000E+00
13292274667162246711475200 C	1.000E-112	1.000E-112	1.000E+00	1.000E+00
26584549334324493422950400 C	1.000E-113	1.000E-113	1.000E+00	1.000E+00
51169098668648986845900800 C	1.000E-114	1.000E-114	1.000E+00	1.000E+00
102338193373297777890001600 C	1.000E-115	1.000E-115	1.000E+00	1.000E+00
204676386746559555780003200 C	1.000E-116	1.000E-116	1.000E+00	1.000E+00
409352773493119111560006400 C	1.000E-117	1.000E-117	1.000E+00	1.000E+00
818705546986238223120012800 C	1.000E-118	1.000E-118	1.000E+00	1.000E+00
163741109397247446240025600 C	1.000E-119	1.000E-119	1.000E+00	1.000E+00
327482218794494892480051200 C	1.000E-120	1.000E-120	1.000E+00	1.000E+00
6549644375889897849600102400 C	1.000E-121	1.000E-121	1.000E+00	1.000E+00
1309928875177979569200204800 C	1.000E-122	1.000E-122	1.000E+00	1.000E+00
2619857550355959138400409600 C	1.000E-123	1.000E-123	1.000E+00	1.000E+00
5239715100711918276800819200 C	1.000E-124	1.000E-124	1.000E+00	1.000E+00
10479430000000000000000000000000 C	1.000E-125	1.000E-125	1.000E+00	1.000E+00

GENAUS TIC	SPILLING	RECENT	EXCUSE	TINY
L24	32.65	21.74	16.62	11.74
L25	21.74	16.62	11.74	11.74
L26	16.62	11.74	11.74	11.74
L27	11.74	11.74	11.74	11.74

TABLE 40

MISSION DURATION T=60. MENTS *****
CONFIDENCE LEVEL 95% *****

ENERGY LEVELS (MEV)	EXPOSURE LEVEL (%)		SHIELDING TIME	PERCENT EXPOSURE TIME
	80	60		
CONSIDERATION DURATION T=60 MONTHS *****				
10.0	1.258E 1.0	1.288E 1.0	1.718E 1.0	2.147E 1.0
20.0	8.434E C5	8.434E C5	1.178E 1.0	1.472E 1.0
30.0	6.057E C5	6.057E C5	1.09E 0.9	1.43E 1.0
40.0	4.153E C5	4.153E C5	5.537E 0.9	6.921E 0.9
50.0	2.847E C5	2.847E C5	3.797E 0.9	4.765E 0.9
60.0	1.952E C5	1.952E C5	2.603E 0.9	3.254E 0.9
70.0	1.335E C5	1.335E C5	1.785E 0.9	2.231E 0.9
80.0	9.294E C5	9.294E C5	1.22E 0.9	1.520E 0.9
90.0	6.294E C5	6.294E C5	8.392E 0.9	1.049E 0.9
100.0	4.316E C5	4.316E C5	6.754E 0.8	1.007E 0.8
110.0	2.979E C5	2.979E C5	3.945E 0.8	4.932E 0.8
120.0	2.029E C5	2.029E C5	2.715E 0.8	3.824E 0.8
130.0	1.351E C5	1.351E C5	1.855E 0.8	4.734E 0.8
140.0	9.535E C7	9.535E C7	1.272E 0.8	2.319E 0.8
150.0	6.541E C7	6.541E C7	1.590E 0.8	2.226E 0.8
160.0	4.305E C7	4.305E C7	9.721E 0.7	1.090E 0.7
170.0	3.075E C7	3.075E C7	6.490E 0.7	7.474E 0.7
180.0	2.043E C7	2.043E C7	4.100E 0.7	7.125E 0.7
190.0	1.343E C7	1.343E C7	2.911E 0.7	3.514E 0.7
200.0	9.913E C7	9.913E C7	1.928E 0.7	2.409E 0.7
			1.322E 0.7	1.652E 0.7

TABLE 41

MAGNETIC SHIELDING SHELL	PERCENT EXPOSURE	TIME
DIPOLE CUT-OFF	100	10 sec.
CUT-OFF	100	10 sec.
SHIELD	100	10 sec.

2222
2222

1

TABLE 42

ORBITAL FLUX SIGHT WITH CHARGED PARTICLE ENVIRONMENTS. VERTICES AFG-AE17 FOR SOLAR MAXIMUM (APR 1979) AND AFG-AE17 FOR PROTONS (APR 1) - JF = 1.0; FOR INNER ZONE FLUXES (AEG6) - JF = 1.0. UNCERTAINTY FACTORS (UF) APPLIED FOR THIS RUN ARE: FOR PROTONS (APR 1) - UF = 1.5 MEV. MAGNETIC COORDINATES 9 AND 10 COMPUTED BY INVARA OF 1972 WITH ALLMAZ MODEL. 4: ARRAC, B: GIG ET AL. TIME: 1989.5. A: VEHICLE AND X-SAT. B: INCLINATION ANGLE. C: DEGREES. D: EARTH-MARS DISTANCE. E: G: GREENBELT, MARYLAND. 10: SAAAG. 11: PERIOD. 12: 1985. 13: 1986. 14: 1987.

FOR INFORMATION OR EXPLANATION CONTACT E.S. STASSINOPOLIS AT NASA-GFCC/CDIF 601, GREENBELT, MARYLAND 20771. TEL: (301) 734-8067.

MISSION DURATION: 5-1000 YEARS.

DCSE AT TRANSMISSION SURFACE OF FINITE ALUMINUM SHELL SHIELDS.

MISSION DURATION: 5-1000 YEARS.

SHIELD THICKNESS (ALUMINUM) S (CENTIMETERS) L (CENTIMETERS)	ELECTRONS*			URANIUM- ALUMINUM LOADS-ALL			PROTONS** URANIUM- ALUMINUM LOADS-ALL			TOTAL DOSE ALL SOURCES LOADS-ALL		
	INNER ZN, LOADS-ALL	OUTER ZN, LOADS-ALL	TOTAL LOADS-ALL	TRAPPED*** LOADS-ALL	SOLAR+ LOADS-ALL	TOTAL LOADS-ALL	TRAPPED*** LOADS-ALL	SOLAR+ LOADS-ALL	TOTAL LOADS-ALL	TRAPPED*** LOADS-ALL	SOLAR+ LOADS-ALL	TOTAL LOADS-ALL
0.001	0.00	1.0	2.257E-07	6.399E-05	2.361E-07	9.859E-03	6.960E-05	9.949E-02	6.527E-05	3.392E-07	3.333E-07	2.392E-07
0.002	0.07	3.0	1.257E-07	5.977E-05	1.257E-07	5.803E-03	3.554E-05	1.000E-02	3.542E-05	1.000E-07	1.000E-07	1.000E-07
0.003	0.14	4.0	7.784E-06	2.882E-05	8.022E-06	6.271E-03	2.655E-05	1.023E-02	2.649E-05	8.445E-06	8.445E-06	8.445E-06
0.004	0.15	6.0	5.064E-06	2.247E-05	5.099E-06	5.167E-03	2.163E-05	1.023E-02	2.174E-05	5.531E-06	5.531E-06	5.531E-06
0.005	0.19	7.0	3.136E-06	1.834E-05	3.160E-06	3.437E-03	1.864E-05	1.038E-02	1.875E-05	3.812E-06	3.812E-06	3.812E-06
0.006	0.22	9.0	2.385E-06	1.544E-05	2.559E-06	3.698E-03	1.655E-05	1.041E-02	1.666E-05	2.710E-06	2.710E-06	2.710E-06
0.007	0.24	10.0	1.603E-06	1.330E-05	1.826E-06	4.201E-03	1.490E-05	1.042E-02	1.493E-05	1.983E-06	1.983E-06	1.983E-06
0.008	0.30	12.0	1.228E-06	1.166E-05	1.359E-06	2.810E-03	1.359E-05	1.010E-02	1.370E-05	1.485E-06	1.485E-06	1.485E-06
0.009	0.33	13.0	9.076E-07	9.076E-06	9.331E-07	2.808E-03	2.499E-03	1.100E-02	1.261E-05	1.142E-06	1.142E-06	1.142E-06
0.010	0.37	15.0	6.073E-07	6.073E-06	6.229E-07	2.295E-03	1.180E-03	1.100E-02	1.170E-05	9.301E-06	9.301E-06	9.301E-06
0.020	0.74	25.0	1.063E-06	4.532E-05	1.517E-05	1.158E-03	6.901E-04	8.765E-02	6.958E-04	2.227E-05	2.227E-05	2.227E-05
0.030	1.14	44.0	6.881E-06	3.981E-04	6.688E-06	6.020E-03	7.001E-04	5.357E-02	7.001E-04	1.188E-05	1.188E-05	1.188E-05
0.40	1.48	58.0	2.045E-04	1.675E-04	3.791E-04	6.197E-04	4.062E-02	5.860E-02	4.120E-04	7.902E-04	7.902E-04	7.902E-04
0.50	1.85	73.0	1.228E-04	1.379E-04	1.379E-04	1.228E-03	1.228E-04	1.228E-02	3.452E-04	5.840E-04	5.840E-04	5.840E-04
0.60	2.20	87.0	7.512E-05	7.192E-03	1.420E-04	4.130E-03	3.016E-04	4.384E-02	3.155E-04	4.619E-04	4.619E-04	4.619E-04
0.80	2.56	117.0	3.124E-03	3.533E-03	3.291E-03	3.362E-02	2.545E-04	3.469E-02	2.560E-04	3.279E-04	3.279E-04	3.279E-04
1.00	3.70	146.0	1.241E-03	1.907E-03	3.148E-03	2.762E-02	2.235E-04	2.831E-02	2.264E-04	2.636E-04	2.636E-04	2.636E-04
1.20	5.03	182.0	5.022E-02	6.947E-02	4.598E-02	2.269E-02	1.980E-04	2.259E-02	2.033E-04	2.145E-04	2.145E-04	2.145E-04
1.50	5.56	219.0	5.036E-01	3.851E-01	4.598E-01	1.934E-02	1.795E-04	1.895E-02	1.813E-04	1.876E-04	1.876E-04	1.876E-04
1.75	6.48	265.0	6.355E-03	1.473E-02	1.537E-02	1.091E-02	1.654E-04	1.554E-02	1.670E-04	1.562E-04	1.562E-04	1.562E-04
2.00	7.41	292.0	6.679E-01	9.04E-01	4.971E-01	1.507E-02	1.535E-04	1.736E-02	1.548E-04	1.558E-04	1.558E-04	1.558E-04
2.50	9.26	365.0	1.673E-33	3.086E-00	3.087E-00	1.245E-02	1.350E-02	1.350E-04	1.360E-04	1.372E-04	1.372E-04	1.372E-04
2.00	11.11	432.0	0.0	5.018E-02	5.018E-02	1.062E-02	1.209E-02	1.209E-04	1.216E-04	1.227E-04	1.227E-04	1.227E-04
3.00	12.96	510.0	0.0	1.291E-05	1.291E-05	9.552E-01	1.098E-01	1.098E-04	5.797E-01	1.114E-04	1.114E-04	1.114E-04
4.00	14.81	583.0	0.0	0.0	0.0	6.338E-01	4.008E-01	4.008E-04	4.055E-01	1.013E-04	1.021E-04	1.021E-04
5.00	16.67	656.0	0.0	0.0	0.0	7.579E-01	9.399E-01	9.399E-04	3.775E-01	9.347E-03	9.722E-03	9.722E-03
6.00	18.52	729.0	0.0	0.0	0.0	6.634E-01	7.636E-01	7.636E-04	3.066E-01	6.677E-03	6.735E-03	6.735E-03
8.00	22.23	875.0	0.0	0.0	0.0	7.573E-01	7.521E-01	7.521E-04	2.503E-01	7.545E-03	7.603E-03	7.603E-03
10.00	25.63	1167.0	0.0	0.0	0.0	4.269E-01	5.917E-01	5.917E-04	1.118E-01	5.022E-03	5.965E-03	5.965E-03
	37.04	1458.0	0.0	0.0	0.0	3.287E-01	4.804E-01	4.804E-04	2.06E-01	4.810E-03	4.843E-03	4.843E-03

* ELECTRON MODEL:

AE6: INNER ZONE-SCAL MAX
NO UNCERTAINTY FACTOR WAS APPLIED TO THE MODEL DATA.

+ SOLAR PROTON MODEL:

SOLRD: SOLAR FLARE PROTONS AT 1 AU
FOR CUTOFF DIPOLE SHELL OF 5 E.R.

AE17: OUTER ZONE-INTERPLANETIC MODEL WITH SCALAR CYCLE DEPENDENCE.
FOR ENERGIES ABOVE 1.5 MEV, THIS MODEL CONTAINS UPPER L
LOWER LIMIT VALUES TO ACCOUNT FOR DISCRETE FAULTS BETWEEN
EXISTING DATA SETS. THE AE17-H1 FAULTS VARY FROM VARIOUS
MOMENTUM DATA WHILE AE17-L1 IS MORE REPRESENTATIVE OF
ALL THE DATA SETS PRESENTLY AVAILABLE TO ASSOC.

>>> THE RETROD POSITION WAS USED FOR THESE CALCULATIONS <<

NOTE: U DENOTES THE DEGREE OF CONFIDENCE ONE WISHES
TO ASSIGN TO RESULTS, NAMELY THAT FOR THE
SPECIFIC MISSION DURATION THE CALCULATED
FLUXES ARE THE SMALLEST VALUE WHICH WILL
NOT BE EXCEEDED. HY ACTUALLY ENCOUNTERED
INTERSTITIALS.

IT IS NOT ADVISED TO EXTRAPOLATE THE SOLAR
PROTON SPECTRA FURTHER TOWARDS LOWER NOR
TOWARDS HIGHER ENERGIES BECAUSE THE DATA SETS
USED IN THE CONSTRUCTION OF THE MODEL AS
LITTLE AS A SUNFLARE MADE DURING THE 20TH SOLAR
CYCLE (1964-1974) AND THE 21ST CYCLE (1974-1984).

TABLE 43

ORBITAL FLUX STUDY WITH COMPOSITE PARTICLE ENVIRONMENTAL VETTES APIA AEC - AE17 FOR SOLAR MAXIMUM 1979
 UNCERTAINTY FACTORS (UF) APPLIED FOR THIS RUN ARE:
 JF= 1.0; UF = 1.0
 MAGNETIC COORDINATES AND COMPUTED BY INVARA OF 1972 WITH ALL MAG. MODEL 4;
 VEHICLE POSITION AND INCLINATION CODED AS DEPICTED IN THE
 EXPLANATION JR.
 FOR INFORMATION JR.
 STASSINOPULOS AT NASA-GF, CUDF, COI, GREENBELT, MARYLAND 20771 TEL (301)-344-8067

DCIS AT TRANSMISSION SURFACE 0.1 FINITE ALUMINUM SLAB SHIELDS
 MISSION DURATION: 5,000 YR(H)

SHIELD THICKNESS (ALUMINUM) S ALUMINUM C CARBON A ANALOGUE	ELECTRONS*			PROTONS			TOTAL		
	INNER ZN. T		OUTER ZN. (HEADS-ALL)	TRAPPED** (HEADS-ALL)		SOLAR+ (HEADS-ALL)	TOTAL (HEADS-ALL)	TOTAL DOSE ALL SOURCES (HEADS-ALL)	
	INNER T	OUTER T	INNER T	OUTER T	TRAPPED T	TRAPPED T	SOLAR+ T	TOTAL T	DOSE T
0.01	0.04	1.	7.905E-27	1.199E-06	8.325E-07	2.414E-04	4.844E-06	1.175E-03	8.513E-07
0.02	0.07	3.	6.373E-27	4.764E-05	4.756E-07	2.078E-04	2.150E-06	1.197E-03	4.741E-07
0.03	0.11	4.	2.717E-27	5.364E-05	2.707E-07	2.162E-04	1.210E-06	2.152E-03	2.988E-07
0.04	0.15	7.	1.783E-27	9.71E-05	1.822E-07	1.785E-04	1.765E-06	1.219E-03	2.301E-07
0.05	0.19	7.	1.210E-27	3.303E-05	1.244E-07	1.494E-04	1.522E-06	1.225E-03	1.306E-07
0.06	0.22	5.	8.450E-27	9.759E-05	8.736E-06	1.274E-04	1.022E-06	1.223E-03	1.200E-07
0.07	0.26	10.	6.045E-27	2.460E-05	6.291E-06	1.103E-04	1.162E-06	1.230E-03	1.324E-07
0.08	0.30	12.	4.419E-27	1.156E-05	4.435E-05	9.775E-03	1.041E-06	1.228E-03	1.469E-07
0.09	0.33	13.	3.266E-27	1.916E-05	3.490E-05	9.074E-03	1.041E-05	1.228E-03	1.686E-07
0.10	0.37	15.	2.514E-27	1.724E-05	2.689E-05	7.703E-03	8.585E-05	1.227E-03	4.355E-07
0.20	0.74	29.	6.313E-05	6.308E-04	4.967E-05	3.962E-03	4.047E-05	1.227E-03	3.911E-07
0.30	1.11	44.	1.601E-05	4.965E-04	2.098E-03	2.732E-03	2.517E-05	1.226E-03	9.366E-07
0.40	1.48	58.	8.446E-05	4.693E-04	1.154E-03	2.105E-03	1.764E-05	1.226E-03	4.640E-07
0.50	1.85	73.	5.069E-04	1.993E-04	7.016E-04	1.724E-03	1.154E-05	1.226E-03	2.946E-07
0.60	2.22	87.	3.208E-04	1.328E-04	4.536E-04	1.466E-03	1.111E-05	1.226E-03	2.085E-07
0.80	2.96	117.	1.303E-04	6.519E-03	1.995E-03	1.366E-03	8.242E-03	1.226E-03	1.580E-07
1.00	3.70	146.	5.255E-03	3.516E-03	8.707E-03	9.313E-02	6.442E-04	1.226E-03	1.039E-07
1.20	5.55	172.	1.227E-02	1.056E-02	2.866E-02	7.035E-02	5.043E-04	1.226E-03	6.392E-07
1.50	8.44	219.	1.894E-02	7.066E-02	8.950E-02	4.497E-02	4.921E-04	1.219E-02	4.943E-07
1.75	0.48	255.	2.229E-01	2.687E-02	2.910E-02	5.673E-02	4.408E-04	1.226E-02	4.427E-07
2.00	7.41	292.	2.285E-01	6.844E-01	9.072E-01	5.050E-02	3.138E-04	1.542E-02	4.732E-07
2.50	9.26	365.	6.396E-03	5.362E-03	4.366E-03	4.165E-02	3.797E-04	1.142E-02	3.344E-07
3.00	11.11	437.	0.0	1.022E-01	1.022E-01	4.562E-02	2.993E-04	8.827E-03	1.020E-07
3.50	12.96	510.	0.0	6.676E-05	6.676E-05	3.115E-02	2.655E-04	6.891E-03	2.693E-07
4.00	14.81	582.	0.0	0.0	0.0	2.449E-02	2.215E-04	4.056E-03	2.449E-07
5.00	16.67	656.	0.0	0.0	0.0	2.098E-02	2.039E-04	2.021E-03	2.242E-07
5.00	18.52	729.	0.0	0.0	0.0	1.905E-02	1.753E-04	2.654E-03	2.036E-07
6.00	23.22	875.	0.0	0.0	0.0	1.408E-02	1.347E-04	1.755E-03	1.775E-07
8.00	29.33	1127.	0.0	0.0	0.0	1.008E-02	1.072E-04	1.347E-03	1.361E-07
10.00	37.04	1458.	0.0	0.0	0.0	1.008E-02	7.395E-04	1.074E-03	1.084E-07

ELECTRON MODELS:

AE1: INNER ZONE-SOLAR MAX
NO UNCERTAINTY FACTOR WAS APPLIED TO THE MODEL DATA.

SOLAR PROTON MODEL:

SOLAR: SOLAR FLARE FREQUENCIES AT 1 AU
LUNAR: LUNAR FLARE FREQUENCIES AT 1 AU
CUTOFF: CUTOFF DIPOLAR SHIELDING APPLIED

AE17: OUTER ZONE-INTERIM MODEL WITH SCALAR DIPOLAR.
 FOR ENERGIES ABOVE 1.5 MEV THIS MODEL CONTAINS JUPITER'S LOWER ENERGY VALUES TO ACCOUNT FOR DISCREPANCY BETWEEN EXISTING DATA SETS. THE AE17-H1 FAVORS VAMPULA'S FIT TO DATA-19 DATA WHILE AE17-L1 IS MORE REASONABLE. ALL THE DATA SETS PRESENTLY AVAILABLE TO NSSDC.
 NO UNCERTAINTY FACTOR WAS APPLIED TO THE MODEL DATA.

AE6: PROTON MODEL:
 AE6-MAC: TRAPPED PROTONS-SOLAR MAX
 NO UNCERTAINTY FACTOR WAS APPLIED TO THE MODEL DATA.

NOTE: * DENOTES THE DEGREE OF CONFIDENCE ONE WISHES TO ASSIGN TO THE SETS, NAMELY THAT FOR THE SOLAR FLARES THE DATA SETS ARE MORE RELIABLE. FLUXES ARE THE SMALLEST VALUES WHICH WILL NOT BE EXCEEDED BY ACTUALLY ENCOUNTERED FLUXES.

IT IS NOT ADVISED TO EXTRAPOLATE THE SOLAR PROTON SPECTRA NEITHER TOWARDS LOWER NOR TOWARDS HIGHER ENERGIES BECAUSE THE DATA SETS USED IN THE CONSTRUCTION OF THE MODEL ARE LIMITED TO THE 20TH SOLAR CYCLE: 1964-1975. DO NOT CONTAIN INFORMATION FROM 1976 AND FUTURE.

TABLE 44

ELECTRON MODELS:

FIG. 6: INNER ZONE-SOLAR MAX NO UNCERTAINTY FACTOR WAS APPLIED TO THE MODEL DATA.

AZ17: OUTER ZONE-INTERIOR MODEL WITHOUT SOLAR CYCLE DEPENDENCE.
FOR ENERGIES ABOVE 1.5 MeV, THIS MODEL CONTAINS UPPER & LOWER LIMIT VALUES TO ACCOUNT FOR DISCREPANCY BETWEEN EXISTING DATA SETS. THE AZ17-11 FAVORABLE VARIATION FROM OV1-9 DATA WHILE AZ17-LO IS MORE REPRESENTATIVE OF ALL THE DATA SETS PRESENTLY AVAILABLE TO NSSDC.

PROTON MODEL: AP6-HAC: TRAPPED PROTONS-SOLAR MAX NO DONG PRACTICALLY FACTION HAS ADDED TO THE MACHINE DATA

• SOLAR PHOTON MODEL:

SULPRO: SCALAR FLAME PROTONS AT 1 AU
(ATTENUATED, INTERPLANETARY)

NOTE: INDUCES THE DEGREE OF CONFIDENCE ONE WISHES TO ACQUIRE IN THE ASSESSMENT OF THE SPECIFIC POSITION OR STATE OF A FIELD, EXCEPTED BY ACTUALLY ENCOUNTERED FIELD.

IT IS NOT ADVISABLE TO EXTRAPOLATE THE SOLAR PROTONS SPECTRA NEITHER TOWARDS LOWER NOR TOWARDS HIGHER ENERGIES BECAUSE THE DATA SETS USED IN THE CONSTRUCTION OF THE MODEL (SATellite MEASURED SURFACE) MADE DURING THE 20TH SOLAR CYCLE (1964-1975) DO NOT CONTAIN INFORMATION

TABLE 465

DORBITA-EURO STUDY DUE COMPLETION DATE: VENTURE VETB3 API: A06, A117 FCH SULAT MAXTHW
 FOR PHOTONS (APB) - UFR = 1.0. FOR TRANS. ZNU. FLUXFCRS (APB) - UFR = 1.0.
 UNCERTAINITY FACTORS (UF) APPLIED FOR THE FOLLOWING: 1. UF = 1.0 FOR ALL MAN. MUDL 4;
 WITH ALL MAN. MUDL 4; 2. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C; 3. UF = 1.0 FOR ALL
 MAGNETIC COORDINATES B AND L COMPUT. B AND L COMPUT. C; 4. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C;
 5. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C; 6. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C;
 7. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C; 8. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C;
 9. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C; 10. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C;
 11. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C; 12. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C;
 13. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C; 14. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C;
 15. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C; 16. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C;
 17. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C; 18. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C;
 19. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C; 20. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C;
 21. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C; 22. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C;
 23. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C; 24. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C;
 25. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C; 26. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C;
 27. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C; 28. UF = 1.0 FOR ALL COMPUT. B AND L COMPUT. C;

FOR INFORMATION OR EXPLANATION CONTACT: DR. STASSI ACCUCUS AT NASA-GSFC (COLD CYCLE)
 OR DR. NATHAN MAHAYAN AT NASA-GSFC (COLD CYCLE). GENEVA, SWITZERLAND
 20771, L-3011-340-H067.

ELECTRONS

SHIELD THICKNESS (ALUMINUM)	TOTAL			PROTONS		
	ALUM TOTAL LEADS+AL	LEADS TOTAL LEADS+AL	LEADS TOTAL LEADS+AL	TRAP SCALAR (RAJ-S-AL)	SCALAR (RAJ-S-AL)	TOTAL -- ALL ECU'S (RAJ-S-AL)
0.01	0.04	1.0	1.41E-06	3.55E-06	1.47E-05	2.31E-08
0.02	0.07	-	7.21E-07	9.82E-07	5.09E-07	1.70E-08
0.03	0.11	4.87E-07	1.035E-06	5.009E-07	3.92E-07	1.54E-08
0.04	0.15	2.18E-07	1.254E-06	3.952E-07	2.21E-07	2.28E-08
0.05	0.19	7.0	2.17E-07	1.025E-06	2.765E-07	5.64E-08
0.06	0.22	9.0	1.624E-07	3.6E-06	2.765E-07	4.24E-08
0.07	0.25	1.0	8.87E-07	1.63E-06	1.63E-07	3.50E-08
0.08	0.27	1.0	6.655E-07	1.68E-06	2.022E-07	2.60E-08
0.09	0.29	1.2	6.55E-07	1.68E-06	2.022E-07	2.60E-08
0.10	0.32	1.2	7.54E-07	8.05E-06	8.05E-07	2.60E-08
0.11	0.34	1.5	4.96E-07	5.496E-06	5.496E-07	2.60E-08
0.12	0.37	1.5	4.96E-07	5.496E-06	5.496E-07	2.60E-08
0.13	0.40	2.9	2.43E-05	2.43E-05	6.93E-05	1.12E-06
0.14	0.42	4.4	5.641E-04	1.641E-03	2.08E-03	4.23E-05
0.15	0.44	5.8	8.67E-04	5.23E-03	4.712E-03	3.93E-05
0.16	0.46	7.2	6.65E-03	6.65E-03	1.61E-02	2.05E-05
0.17	0.48	7.2	6.65E-03	6.65E-03	1.61E-02	2.05E-05
0.18	0.50	11.7	1.92E-03	1.92E-03	4.49E-03	4.14E-05
0.19	0.52	14.6	1.92E-03	1.92E-03	4.49E-03	4.14E-05
0.20	0.54	17.2	4.72E-03	4.72E-03	1.225E-02	1.225E-04
0.21	0.56	21.9	1.45E-02	1.45E-02	3.69E-02	3.69E-04
0.22	0.58	25.5	2.43E-02	2.43E-02	6.09E-02	6.09E-04
0.23	0.60	29.0	7.789E-02	7.789E-02	1.939E-01	1.939E-04
0.24	0.61	32.5	3.655E-01	2.554E-01	8.020E-02	8.020E-04
0.25	0.62	36.0	1.757E-03	1.757E-03	6.891E-01	6.891E-04
0.26	0.63	43.2	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.27	0.64	51.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.28	0.65	59.6	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.29	0.66	68.1	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.30	0.67	76.5	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.31	0.68	85.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.32	0.69	93.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.33	0.70	101.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.34	0.71	110.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.35	0.72	118.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.36	0.73	126.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.37	0.74	135.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.38	0.75	143.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.39	0.76	151.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.40	0.77	160.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.41	0.78	168.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.42	0.79	176.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.43	0.80	185.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.44	0.81	193.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.45	0.82	201.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.46	0.83	210.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.47	0.84	218.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.48	0.85	226.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.49	0.86	235.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.50	0.87	243.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.51	0.88	251.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.52	0.89	260.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.53	0.90	268.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.54	0.91	276.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.55	0.92	285.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.56	0.93	293.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.57	0.94	301.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.58	0.95	310.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.59	0.96	318.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.60	0.97	326.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.61	0.98	335.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.62	0.99	343.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.63	0.00	351.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.64	0.00	360.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.65	0.00	368.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.66	0.00	376.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.67	0.00	385.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.68	0.00	393.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.69	0.00	401.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.70	0.00	410.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.71	0.00	418.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.72	0.00	426.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.73	0.00	435.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.74	0.00	443.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.75	0.00	451.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.76	0.00	460.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.77	0.00	468.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.78	0.00	476.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.79	0.00	485.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.80	0.00	493.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.81	0.00	501.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.82	0.00	510.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.83	0.00	518.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.84	0.00	526.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.85	0.00	535.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.86	0.00	543.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.87	0.00	551.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.88	0.00	560.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.89	0.00	568.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.90	0.00	576.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.91	0.00	585.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.92	0.00	593.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.93	0.00	601.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.94	0.00	610.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.95	0.00	618.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.96	0.00	626.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.97	0.00	635.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.98	0.00	643.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.99	0.00	651.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.00	0.00	660.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.01	0.00	668.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.02	0.00	676.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.03	0.00	685.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.04	0.00	693.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.05	0.00	701.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.06	0.00	710.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.07	0.00	718.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.08	0.00	726.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.09	0.00	735.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.10	0.00	743.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.11	0.00	751.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.12	0.00	760.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.13	0.00	768.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.14	0.00	776.7	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.15	0.00	785.0	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.16	0.00	793.4	1.92E-04	1.92E-04	4.49E-02	4.49E-04
0.						

FIELD THICKNESS (IN INCHES)		ELECTRICAL CONDUCTIVITY		ELECTRICAL THICKNESS (INCHES-AL)		FREQUENCY- ABSORBING TOTAL (EACS-AL)		THICKNESS OF FINITE ALUMINUM SLAB (EADS-AL)		TOTAL THICKNESS (RAD-SAL)		TOTAL DOSE ALL SOURCES (RAD-SAL)		INITIAL DOSE ALL SOURCES (RAD-SAL)	
0.01	0.04	1.	0.107	0.1	0.209	0.04	0.381	0.1	0.209	0.04	0.381	0.04	0.000	0.000	0.000
0.03	0.11	1.	0.107	0.05	0.227	0.05	0.480	0.07	0.394	0.04	0.594	0.04	0.000	0.000	0.000
0.04	0.16	1.	0.107	0.05	0.227	0.05	0.511	0.07	0.426	0.04	0.646	0.04	0.000	0.000	0.000
0.05	0.19	1.	0.107	0.05	0.227	0.05	0.513	0.07	0.428	0.04	0.648	0.04	0.000	0.000	0.000
0.06	0.22	1.	0.107	0.05	0.227	0.05	0.515	0.07	0.430	0.04	0.650	0.04	0.000	0.000	0.000
0.08	0.26	1.	0.107	0.05	0.227	0.05	0.517	0.07	0.432	0.04	0.652	0.04	0.000	0.000	0.000
0.09	0.29	1.	0.107	0.05	0.227	0.05	0.519	0.07	0.434	0.04	0.654	0.04	0.000	0.000	0.000
0.10	0.31	1.	0.107	0.05	0.227	0.05	0.521	0.07	0.436	0.04	0.656	0.04	0.000	0.000	0.000
0.12	0.37	1.	0.107	0.05	0.227	0.05	0.523	0.07	0.438	0.04	0.658	0.04	0.000	0.000	0.000
0.15	0.49	1.	0.107	0.05	0.227	0.05	0.525	0.07	0.440	0.04	0.660	0.04	0.000	0.000	0.000
0.18	0.59	1.	0.107	0.05	0.227	0.05	0.527	0.07	0.442	0.04	0.662	0.04	0.000	0.000	0.000
0.20	0.74	1.	0.107	0.05	0.227	0.05	0.529	0.07	0.444	0.04	0.664	0.04	0.000	0.000	0.000
0.25	1.11	1.	0.107	0.05	0.227	0.05	0.532	0.07	0.447	0.04	0.667	0.04	0.000	0.000	0.000
0.30	1.46	1.	0.107	0.05	0.227	0.05	0.535	0.07	0.450	0.04	0.670	0.04	0.000	0.000	0.000
0.40	1.98	1.	0.107	0.05	0.227	0.05	0.538	0.07	0.453	0.04	0.673	0.04	0.000	0.000	0.000
0.50	2.53	1.	0.107	0.05	0.227	0.05	0.541	0.07	0.456	0.04	0.676	0.04	0.000	0.000	0.000
0.60	3.06	1.	0.107	0.05	0.227	0.05	0.544	0.07	0.459	0.04	0.679	0.04	0.000	0.000	0.000
0.70	3.70	1.	0.107	0.05	0.227	0.05	0.547	0.07	0.462	0.04	0.682	0.04	0.000	0.000	0.000
0.80	4.36	1.	0.107	0.05	0.227	0.05	0.550	0.07	0.465	0.04	0.685	0.04	0.000	0.000	0.000
0.90	5.02	1.	0.107	0.05	0.227	0.05	0.553	0.07	0.468	0.04	0.688	0.04	0.000	0.000	0.000
1.00	5.70	1.	0.107	0.05	0.227	0.05	0.556	0.07	0.471	0.04	0.691	0.04	0.000	0.000	0.000
1.25	8.52	1.	0.107	0.05	0.227	0.05	0.567	0.07	0.477	0.04	0.697	0.04	0.000	0.000	0.000
1.50	10.56	1.	0.107	0.05	0.227	0.05	0.574	0.07	0.484	0.04	0.704	0.04	0.000	0.000	0.000
1.75	13.62	1.	0.107	0.05	0.227	0.05	0.581	0.07	0.491	0.04	0.711	0.04	0.000	0.000	0.000
2.00	16.70	1.	0.107	0.05	0.227	0.05	0.588	0.07	0.498	0.04	0.718	0.04	0.000	0.000	0.000
2.50	25.08	1.	0.107	0.05	0.227	0.05	0.595	0.07	0.505	0.04	0.725	0.04	0.000	0.000	0.000
3.00	37.56	1.	0.107	0.05	0.227	0.05	0.602	0.07	0.512	0.04	0.732	0.04	0.000	0.000	0.000
4.00	56.32	1.	0.107	0.05	0.227	0.05	0.610	0.07	0.520	0.04	0.740	0.04	0.000	0.000	0.000
5.00	79.48	1.	0.107	0.05	0.227	0.05	0.618	0.07	0.528	0.04	0.748	0.04	0.000	0.000	0.000
6.00	106.04	1.	0.107	0.05	0.227	0.05	0.625	0.07	0.535	0.04	0.755	0.04	0.000	0.000	0.000
7.00	136.96	1.	0.107	0.05	0.227	0.05	0.632	0.07	0.542	0.04	0.762	0.04	0.000	0.000	0.000
8.00	171.12	1.	0.107	0.05	0.227	0.05	0.639	0.07	0.550	0.04	0.769	0.04	0.000	0.000	0.000
9.00	210.52	1.	0.107	0.05	0.227	0.05	0.646	0.07	0.557	0.04	0.776	0.04	0.000	0.000	0.000
10.00	254.12	1.	0.107	0.05	0.227	0.05	0.653	0.07	0.564	0.04	0.783	0.04	0.000	0.000	0.000
12.50	391.72	1.	0.107	0.05	0.227	0.05	0.660	0.07	0.571	0.04	0.790	0.04	0.000	0.000	0.000
15.00	516.56	1.	0.107	0.05	0.227	0.05	0.667	0.07	0.578	0.04	0.797	0.04	0.000	0.000	0.000
17.50	641.48	1.	0.107	0.05	0.227	0.05	0.674	0.07	0.585	0.04	0.804	0.04	0.000	0.000	0.000
20.00	766.40	1.	0.107	0.05	0.227	0.05	0.681	0.07	0.592	0.04	0.811	0.04	0.000	0.000	0.000
25.00	1148.00	1.	0.107	0.05	0.227	0.05	0.688	0.07	0.599	0.04	0.818	0.04	0.000	0.000	0.000
30.00	1468.00	1.	0.107	0.05	0.227	0.05	0.695	0.07	0.606	0.04	0.825	0.04	0.000	0.000	0.000
40.00	2152.00	1.	0.107	0.05	0.227	0.05	0.702	0.07	0.613	0.04	0.832	0.04	0.000	0.000	0.000
50.00	2666.00	1.	0.107	0.05	0.227	0.05	0.709	0.07	0.620	0.04	0.839	0.04	0.000	0.000	0.000
60.00	3282.00	1.	0.107	0.05	0.227	0.05	0.716	0.07	0.627	0.04	0.846	0.04	0.000	0.000	0.000
70.00	3776.00	1.	0.107	0.05	0.227	0.05	0.723	0.07	0.634	0.04	0.853	0.04	0.000	0.000	0.000
80.00	4266.00	1.	0.107	0.05	0.227	0.05	0.730	0.07	0.641	0.04	0.860	0.04	0.000	0.000	0.000
90.00	4756.00	1.	0.107	0.05	0.227	0.05	0.737	0.07	0.648	0.04	0.867	0.04	0.000	0.000	0.000
10.00	5246.00	1.	0.107	0.05	0.227	0.05	0.744	0.07	0.655	0.04	0.874	0.04	0.000	0.000	0.000
12.50	7872.00	1.	0.107	0.05	0.227	0.05	0.751	0.07	0.662	0.04	0.881	0.04	0.000	0.000	0.000
15.00	10168.00	1.	0.107	0.05	0.227	0.05	0.758	0.07	0.669	0.04	0.888	0.04	0.000	0.000	0.000
20.00	14252.00	1.	0.107	0.05	0.227	0.05	0.765	0.07	0.676	0.04	0.895	0.04	0.000	0.000	0.000
25.00	18336.00	1.	0.107	0.05	0.227	0.05	0.772	0.07	0.683	0.04	0.902	0.04	0.000	0.000	0.000
30.00	22420.00	1.	0.107	0.05	0.227	0.05	0.779	0.07	0.690	0.04	0.909	0.04	0.000	0.000	0.000
40.00	33632.00	1.	0.107	0.05	0.227	0.05	0.786	0.07	0.697	0.04	0.916	0.04	0.000	0.000	0.000
50.00	40848.00	1.	0.107	0.05	0.227	0.05	0.793	0.07	0.704	0.04	0.923	0.04	0.000	0.000	0.000
60.00	47064.00	1.	0.107	0.05	0.227	0.05	0.800	0.07	0.711	0.04	0.930	0.04	0.000	0.000	0.000
70.00	53280.00	1.	0.107	0.05	0.227	0.05	0.807	0.07	0.718	0.04	0.937	0.04	0.000	0.000	0.000
80.00	59504.00	1.	0.107	0.05	0.227	0.05	0.814	0.07	0.725	0.04	0.944	0.04	0.000	0.000	0.000
90.00	65720.00	1.	0.107	0.05	0.227	0.05	0.821	0.07	0.732	0.04	0.951	0.04	0.000	0.000	0.000
10.00	71936.00	1.	0.107	0.05	0.227	0.05	0.828	0.07	0.739	0.04	0.958	0.04	0.000	0.000	0.000
12.50	92904.00	1.	0.107	0.05	0.227	0.05	0.835	0.07	0.746	0.04	0.965	0.04	0.000	0.000	0.000
15.00	113972.00	1.	0.107	0.05	0.227	0.05	0.842	0.07	0.753	0.04	0.972	0.04	0.000	0.000	0.000
20.00	165960.00	1.	0.107	0.05	0.227	0.05	0.849	0.07	0.760	0.04	0.979	0.04	0.000	0.000	0.000
25.00	207948.00	1.	0.107	0.05	0.227	0.05	0.856	0.07	0.767	0.04	0.986	0.04	0.000	0.000	0.000
30.00	249936.00	1.	0.107	0.05	0.227	0.05	0.863	0.07	0.774	0.04	0.993	0.04	0.000	0.000	0.000
40.00	371924.00	1.	0.107	0.05	0.227	0.05	0.870	0.07	0.781	0.04	0.999	0.04	0.000	0.000	0.000
50.00	433012.00	1.	0.107	0.05	0.227	0.05	0.877	0.07	0.788	0.04	0.106	0.04	0.000	0.000	0.000
60.00	494100.00	1.	0.107	0.05	0.227	0.05	0.884	0.07	0.795	0.04	0.113	0.04	0.000	0.000	0.000
70.00	555188.00	1.	0.107	0.05	0.227	0.05	0.891	0.07	0.802	0.04	0.120	0.04	0.000	0.000	0.000
80.00	616276.00	1.	0.107	0.05	0.227	0.05	0.898	0.07	0.809	0.04	0.127	0.04	0.000	0.000	0.000
90.00	677364.00	1.	0.107	0.05	0.227	0.05	0.905	0.07	0.816	0.04	0.134	0.04	0.000	0.000	0.000
10.00	738452.00	1.	0.107	0.05	0.227	0.05	0.912	0.07	0.823	0.04	0.141	0.04	0.000	0.000	0.000
12.50	949540.00	1.	0.107	0.05	0.227	0.05	0.919	0.07	0.830	0.04	0.148	0.04	0.000	0.000	0.000
15.00	116062.00	1.	0.107	0.05	0.227	0.05	0.926	0.07	0.837	0.04	0.155	0.04	0.000	0.000	0.000
20.00	167150.00	1.	0.107	0.05	0.227	0.05	0.933	0.07	0.844	0.04	0.162	0.04	0.000	0.000	0.000
25.00	228238.00	1.	0.107	0.05	0.227	0.05	0.940	0.07	0.851	0.04	0.169</				

ELASTOSTATIC ANALYSIS

Barry: This is a primary area where interculturality has been made a priority in the model CATA.

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THE DATA CENTER WILL BE LOCATED NEAR THE
HEADQUARTERS OF THE COMPANY.

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TABLE 47

• SCALAR PROPERTY OF \mathcal{O}_F :

RECEIVED
FEDERAL BUREAU OF INVESTIGATION,
U. S. DEPARTMENT OF JUSTICE,
WASHINGTTON, D. C.
JULY 10 1941
SEARCHED INDEXED SERIALIZED FILED
FBI - WASH. D. C.

IT IS NOT ADVISABLE TO EXTRAPOLATE THE SOLAR
FIRING EFFECTS NEITHER TOWARD LOWER NOR
TOWARD HIGHER ENERGIES BECAUSE THE DATA SETS
ARE NOT CONSTRUCTED FOR THIS PURPOSE.
THE MODEL IS BASED ON THE 20TH SOLAR
CYCLE (1948-1975) AND DOES NOT CONTAIN INFORMATION

TABLE I ELLIPTICITY AND PARTITION FUNCTIONS FOR THE GUNARD AND INCHENTINY ACTIVATION MODEL WITH A MAGNETIC CLOUD PLASMA AND A TWO-LEVEL SYSTEM AND FOR THE CLASSICAL SAWFISH MODEL AT KASAROF CLOUDS AT CLASSICAL CONDITIONS

AT INSPECTION SURFACE OF FINITE DILUTION WOULD BE 51.2% AND THE CONCENTRATION AT THE SURFACE OF THE CLOTHESLINE WOULD BE 0.0001 MOLES/LITER.

ELECTRIC ACCELS: AEG: INVER 2 MFT-A MA
ACCELERATION FACIL. 10-140 ACCEL DATA.

FIGURE 1: RUTER 20-F INTEGRATED CYCLE DEFERENCE
FIG. 2. EFFECTS OF VARIOUS CYCLES ON THE CYCLE DEFERENCE.
FIG. 3. CYCLES OF VARIOUS CYCLES ON THE CYCLE DEFERENCE.

L. THE CHIEF PRACTITIONER OF THE NATION IN THE FIELD OF MEDICAL EDUCATION.

FUNCTION ACCURATE

Tenn. E 49

56 L. B. R. :

FIG. 7A-10. MC-0503: # OF AL EVENTS =
62.14% CE MAGNETIC SHIELDING APPLIED

N.C.T.: PROJECT THE DEGREE OF CONFIDENCE ONE WISHES TO ATTAIN IN THE RESULTS, NAMELY THAT FOR THE SPECIFIC MISSION DURATION THE CALCULATED FLUXES ARE THE SMALLEST VALUES WHICH WILL NOT EXCEED, SAY ACTUALLY ENCOUNTERED IN OPERATIONS.

IT IS NOT ADVISABLE TO EXTRAPOLATE THE SCALAR DATA ON HIGHER ENGINES BECAUSE THE DATA SETS USED IN THE CONSTRUCTION OF THE MODEL IS BASED ON ENGINES MADE DURING THE 20TH CYCLE (1964-1975) TO NOT CONTAIN INFORMATION

ORBITAL FLUX STUDY WITH COMPOSITE PARTICLE ENVIRONMENT: VENUS APB1 AEB1 AE17 FLM1 UNIFLUX OF 1979
UNCERTAINTY FACTORS (UF) APPLIED FOR THIS RUN ARE:
MAGNETIC COORDINATES 3 AND L COMPUTED BY INVARA OF 1972 WITH ALL MAG. MODELS.
VEHICLE: VANGUARD-A. INCALCULATON TIME: 1975. TIME: 1989.5
FOR INFORMATION OR EXPLANATION CONTACT E.G.C. STASSINOPoulos AT NASA-GFC, CUDL Q11, GREENBELT, MARYLAND 20771. TEL (301) 340-8067

DOSAGE IN SEMI-INFINITE ALUMINUM MEDIUM
MISSION DURATION: 5,000 YEARS

SHIELD THICKNESS (ALUMINUM)
1CM₂ (MM) (MM)

SHIELD THICKNESS (ALUMINUM) 1CM₂ (MM) (MM)	ELECTRONS			BREMSSTRAHLUNG			PROTONS			TOTAL		
	OUTER ZN LOADS-ALL			TOTAL (RAD-S-ALL)			TRAPPED CHARGE-ALL			TOTAL (RAD-S-ALL)		
	TOTAL	GRADS-ALL	GRADS-ALL	TOTAL	GRADS-ALL	GRADS-ALL	TRAPPED	SOLAR CHARGE-ALL	GRADS-ALL	TRAPPED	SOLAR CHARGE-ALL	GRADS-ALL
0.01	0.04	1.	3.468E-07	9.742E-05	3.56E-37	1.04E-04	6.76E-05	9.98E-02	6.97E-05	3.637E-07	9.98E-02	3.54E-05
0.02	0.07	3.	1.924E-07	6.002E-05	1.98E-37	1.15E-04	5.98E-05	1.51E-02	5.91E-05	2.921E-07	1.52E-02	2.66E-05
0.03	0.11	4.	1.168E-07	4.320E-05	1.232E-37	8.703E-03	2.655E-05	1.025E-03	2.66E-05	1.259E-07	1.03E-02	1.259E-05
0.04	0.15	6.	7.145E-08	2.722E-05	8.08E-38	6.804E-03	2.163E-05	1.032E-03	2.174E-05	8.305E-06	8.305E-03	8.305E-05
0.05	0.19	7.	5.225E-08	2.722E-05	5.497E-36	5.568E-03	1.864E-05	1.038E-03	1.875E-05	5.690E-06	5.690E-03	5.690E-05
0.06	0.22	9.	3.619E-08	2.482E-05	3.847E-36	4.619E-03	1.655E-05	1.041E-03	1.666E-05	4.018E-06	4.018E-03	4.018E-05
0.07	0.26	10.	2.564E-08	2.482E-05	3.432E-36	4.027E-03	1.405E-05	1.042E-03	1.414E-05	3.14E-06	3.14E-03	3.14E-05
0.08	0.33	12.	1.856E-08	1.712E-05	2.322E-36	3.407E-03	1.355E-05	1.041E-03	1.370E-05	2.168E-06	2.168E-03	2.168E-05
0.09	0.33	13.	1.710E-08	1.513E-05	2.152E-36	3.024E-03	1.252E-05	1.261E-05	1.652E-05	1.652E-06	1.652E-03	1.652E-05
0.10	0.37	15.	1.034E-08	1.383E-05	1.170E-36	2.624E-03	1.180E-05	1.034E-05	1.170E-05	1.290E-05	1.290E-03	1.290E-05
0.20	5.74	29.	6.564E-06	6.564E-04	2.166E-35	6.039E-03	6.901E-04	8.766E-02	6.969E-04	2.928E-05	2.928E-03	2.928E-05
0.30	1.11	44.	5.766E-06	3.845E-04	9.612E-35	9.111E-03	5.057E-04	7.004E-02	5.167E-02	1.483E-05	1.483E-03	1.483E-05
0.40	1.48	58.	3.845E-06	2.384E-04	5.321E-34	5.981E-02	4.062E-04	5.867E-02	5.120E-02	9.512E-04	9.512E-03	9.512E-04
0.50	1.85	73.	1.729E-06	1.529E-04	3.249E-34	5.942E-02	3.455E-04	5.925E-02	5.056E-02	6.815E-04	6.815E-03	6.815E-04
0.60	2.22	87.	1.022E-06	1.015E-04	2.082E-34	5.901E-02	2.704E-04	5.838E-02	5.115E-02	5.242E-04	5.242E-03	5.242E-04
0.80	2.96	117.	4.456E-06	4.456E-03	9.404E-33	4.724E-02	2.545E-04	3.835E-02	2.570E-04	3.563E-04	3.563E-04	3.563E-04
1.00	3.70	146.	1.775E-06	1.670E-03	4.441E-03	3.256E-02	2.235E-04	3.465E-02	2.274E-04	2.743E-04	2.743E-04	2.743E-04
1.20	4.65	162.	6.75E-06	1.253E-03	1.668E-03	2.705E-02	1.975E-04	2.427E-02	1.935E-04	2.198E-04	2.198E-04	2.198E-04
1.50	5.56	219.	7.259E-06	5.409E-03	6.135E-02	2.329E-02	1.795E-04	2.185E-02	1.813E-04	1.898E-04	1.898E-04	1.898E-04
1.75	6.48	255.	9.107E-06	2.166E-02	2.166E-02	1.055E-02	1.654E-04	1.556E-02	1.712E-04	1.712E-04	1.712E-04	1.712E-04
2.00	7.41	292.	9.686E-06	6.944E-02	7.040E-02	1.046E-02	1.535E-04	1.370E-02	1.558E-04	1.574E-04	1.574E-04	1.574E-04
2.50	9.26	365.	2.621E-03	4.484E-03	4.492E-03	1.546E-02	1.455E-04	9.627E-02	1.375E-04	1.375E-04	1.375E-04	1.375E-04
3.00	11.00	432.	0.0	1.985E-05	1.985E-05	1.182E-02	1.098E-04	5.757E-01	1.116E-04	1.116E-04	1.116E-04	1.116E-04
3.50	12.96	510.	0.0	0.0	0.0	0.0	0.0	4.665E-01	1.034E-04	1.034E-04	1.034E-04	1.034E-04
4.00	14.81	583.	0.0	0.0	0.0	0.0	0.0	9.309E-01	3.787E-01	9.309E-01	9.309E-01	9.309E-01
4.90	18.67	656.	0.0	0.0	0.0	0.0	0.0	8.637E-01	3.056E-01	8.637E-01	8.637E-01	8.637E-01
5.00	18.52	725.	0.0	0.0	0.0	0.0	0.0	7.522E-01	2.153E-01	7.522E-01	7.522E-01	7.522E-01
6.00	22.22	875.	0.0	0.0	0.0	0.0	0.0	5.511E-01	1.117E-01	5.511E-01	5.511E-01	5.511E-01
8.00	26.63	1167.	0.0	0.0	0.0	0.0	0.0	4.289E-01	4.816E-01	4.289E-01	4.289E-01	4.289E-01
10.00	37.04	1458.	0.0	0.0	0.0	0.0	0.0	4.084E-01	4.816E-01	4.084E-01	4.084E-01	4.084E-01

ELECTRON MODEL S:

AEB1: INNER ZONE-SOLAR MAX
NO UNCERTAINTY FACTOR WAS APPLIED TO THE MODEL DATA.

PROTON MODEL:

SOLPAC: SOLAR FLARE PROTONS AT IAU
LUNAR SHELLS AND JUPITERIAN JUPITERIAN

F14-F16 GEOMAGNETIC SHIELDING APPLIED
FOR CUT-OFF DIPOLE SHELL OF S E O.

AE17: OUTER ZONE-INTERIM MODEL WITHOUT SOLAR CYCLE DEPENDENCE.
FOR ENERGIES ABOVE 1.5 MEV, THIS MODEL CONTAINS UPPER & LOWER LIMIT VALUES TO ACCOUNT FOR OBSERVATIONS FROM THE AE17-19 DATA SETS. THE AE17-19 FAVORS VAMPULA'S 111 AND 191-19 DATA WHILE AE17-19 HAS MORE BROADSPECTRAL CYCLES. ALL THE DATA SETS PRESENTLY AVAILABLE TO NSSDC.

» THE AE17-19 MODEL WAS USED FOR THESE CALCULATIONS. <<

» PROTON MODEL:
AP-14: TRAPPED PROTONS-SOLAR MAX
NO UNCERTAINTY FACTOR WAS APPLIED TO THE MODEL DATA.

F14-F16 GEOMAGNETIC SHIELDING APPLIED
FOR CUT-OFF DIPOLE SHELL OF S E O.

IT IS NOT ADVISED TO EXTRAPOLATE THE SOLAR SPECTRA FURTHER THAN 10 RADARS LONG BECAUSE THE DATA SETS USED IN THE CONSTRUCTION OF THE MODEL IS ALREADY OLD. THE CYCLES 1964-1970 DC-NOT CONTAIN INFORMATION

FROM CYCLES 1971-1975.

TABLE 49

ORIGIN FLUX STUDY WITH COMPOSITE ENVIRONMENT; VELITES AEG: AE17 FUH SOLAR MAXIMUM UNFLUX OF 1979
APRIL 1979 - JUNE 1979. APPLIED FOR THIS PUNAIRE FLUX PREDICTION. EFFECTS OF 1.0
UNCERTAINTY FACTORS (AE) APPLIED TO THIS PUNAIRE FLUX PREDICTION. TIME = 1979.5
MAGNETIC COORDINATES AND COMPUTED BY INVAR OF 1972 WITH ALL MAG. MODUL. 4.
ALL ZONE-1 AND ZONE-2 CALCULATIONS BASED ON THE AEG-1979.5
FOR INFORMATION OR EXPLANATION CONTACT E.G. STASSI/NPOLUS AT NASA-GSFC, CODE 601, GREENBELT, MARYLAND 20771. TE L(1301)-344-8067

DOSE IN SEMI-INFINITE ALUMINUM MEDIUM
MISSION DURATION: 5,000 YR(A.S.)

SHIELD THICKNESS (ALUMINUM) S (cm) S (cm) S (cm)	ELECTRONS*			BREMSSTRAHLING			PROTONS			TOTAL DOSE ALL SOURCES (cm ⁻²)		
	INNER ZN, CUTER ZN, (DOSES) (GRADS) (GRADS)	TOTAL LEAD-AL	LEAD-AL	TOTAL LEAD-AL	TRAPPED LEAD-AL	SOLAR LEAD-AL	TOTAL LEAD-AL	SOLAR LEAD-AL	TOTAL LEAD-AL	C3	4.045E 06	1.028E 08
0.01	0.04	1.	1.215E 07	0.8	1.026E 06	1.233E 08	5.692E 04	4.844E 06	1.017E 04	2.175E 03	2.718E 05	2.718E 05
0.02	0.07	3.	6.711E 07	0.7	6.822E 06	6.822E 07	3.961E 04	2.798E 06	1.197E 04	2.744E 03	2.744E 05	2.744E 05
0.03	0.11	4.	4.147E 07	0.7	6.044E 05	4.225E 05	2.996E 04	2.155E 05	0.210E 04	1.721E 03	1.721E 05	1.721E 05
0.04	0.15	5.	2.711E 07	0.7	5.225E 05	2.774E 05	2.362E 04	1.765E 05	0.215E 04	1.219E 03	1.219E 05	1.219E 05
0.05	0.19	7.	1.838E 07	0.7	5.048E 05	1.889E 05	1.916E 04	1.512E 05	0.152E 04	1.225E 03	1.513E 05	1.513E 05
0.06	0.22	9.	1.298E 07	0.7	4.227E 05	1.324E 05	1.324E 04	1.323E 05	0.132E 04	1.328E 03	1.328E 05	1.328E 05
0.07	0.25	10.	8.432E 07	0.7	3.625E 05	6.563E 05	6.563E 04	1.625E 06	0.230E 04	1.425E 03	1.425E 05	1.425E 05
0.08	0.30	12.	6.072E 07	0.6	3.166E 05	6.989E 05	6.989E 04	1.041E 06	0.104E 04	8.342E 03	8.342E 05	8.342E 05
0.09	0.33	13.	4.970E 07	0.6	2.806E 05	5.250E 05	5.250E 04	1.014E 06	0.1014E 04	9.342E 03	9.342E 05	9.342E 05
0.10	0.37	15.	3.777E 07	0.6	2.518E 05	4.029E 05	4.029E 04	9.101E 05	0.09101E 04	8.452E 03	8.452E 05	8.452E 05
0.20	0.74	29.	6.065E 05	0.5	1.205E 05	7.270E 05	4.464E 03	4.045E 05	0.1034E 04	4.055E 03	4.055E 05	4.055E 05
0.30	1.11	44.	3.195E 05	0.5	1.020E 04	2.026E 05	3.092E 03	2.507E 05	0.265E 04	8.265E 03	8.265E 05	8.265E 05
0.40	1.48	58.	2.313E 05	0.5	4.03E 04	1.652E 05	2.399E 03	1.764E 05	0.916E 04	7.916E 03	7.916E 05	7.916E 05
0.50	1.65	73.	7.246E 04	0.4	2.824E 04	1.007E 05	1.976E 03	1.355E 05	0.935E 04	5.935E 03	5.935E 05	5.935E 05
0.60	2.02	82.	4.580E 04	0.4	1.824E 04	6.454E 04	6.454E 03	1.111E 05	0.8111E 04	4.111E 03	4.111E 05	4.111E 05
0.80	2.96	117.	1.917E 04	0.3	9.140E 03	2.831E 04	1.332E 03	8.242E 04	4.094E 03	8.242E 03	8.242E 04	8.242E 04
1.00	3.70	146.	7.525E 03	0.3	4.916E 03	1.416E 04	1.097E 03	6.742E 03	0.6742E 03	6.742E 03	6.742E 04	6.742E 04
1.25	4.63	182.	1.774E 03	0.2	3.062E 03	4.053E 03	9.099E 02	9.643E 02	0.643E 02	5.870E 02	5.870E 03	5.870E 03
1.50	5.56	219.	2.703E 02	0.2	9.927E 02	1.263E 03	7.823E 02	1.4921E 02	0.14921E 02	4.147E 02	4.147E 03	4.147E 03
1.75	6.48	255.	3.195E 01	0.1	3.787E 02	4.106E 02	6.499E 02	4.4008E 02	0.44008E 02	4.827E 02	4.827E 03	4.827E 03
2.00	7.41	292.	3.144E 00	0.1	2.533E 02	1.286E 02	6.160E 02	1.799E 02	0.1799E 02	4.852E 02	4.852E 03	4.852E 03
2.50	9.26	365.	1.303E -02	0.0	7.892E 00	7.812E 03	5.177E 02	3.798E 02	0.1426E 02	3.451E 02	3.451E 03	3.451E 03
3.00	11.11	432.	0.0	1.536E -01	1.536E -01	1.536E -01	1.423E -02	2.363E -02	0.822E 01	2.322E 01	2.322E 01	2.322E 01
3.50	12.96	510.	0.0	1.026E -04	1.026E -04	1.026E -04	3.944E -02	2.655E -02	6.504E 01	2.622E 01	2.622E 01	2.622E 01
4.00	14.81	583.	0.0	0.0	0.0	0.0	3.527E -02	2.415E -02	6.504E 01	2.421E 01	2.421E 01	2.421E 01
4.50	16.67	656.	0.0	0.0	0.0	0.0	3.080E -02	2.213E -02	4.467E 01	2.207E 01	2.207E 01	2.207E 01
5.00	18.52	729.	0.0	0.0	0.0	0.0	2.001E -02	2.039E -02	3.654E 01	2.043E 01	2.043E 01	2.043E 01
6.00	22.22	875.	0.0	0.0	0.0	0.0	1.899E -02	1.753E -02	3.541E 01	1.780E 01	1.780E 01	1.780E 01
8.00	29.63	1162.	0.0	0.0	0.0	0.0	1.829E -02	1.342E -02	1.316E 01	1.365E 01	1.365E 01	1.365E 01
10.00	37.04	1458.	0.0	0.0	0.0	0.0	1.413E -02	1.073E -02	7.395E 00	1.074E 01	1.074E 01	1.074E 01

* ELECTRON MODEL S:
AEG: INNER ZONE-SOLAR MAX
NO UNCERTAINTY FACTOR WAS APPLIED TO THE MODEL DATA.

+ PROTON MODEL:
AEG-MAC: TRAPPED-PROTONS-SOLAR MAX
NO UNCERTAINTY FACTOR WAS APPLIED TO THE MODEL DATA.

** PROTON MODEL:
AEG-MAC: TRAPPED-PROTONS-SOLAR MAX
NO UNCERTAINTY FACTOR WAS APPLIED TO THE MODEL DATA.

*** PROTON MODEL:
AEG-MAC: SOLAR FLARE PROTONS AT 1 AU
FINALIZED.
FOR CUT-OFF DIPOLE SHELL OF 5 F.P.

AE17: OUTER ZONE-INTERIM MODEL WITHOUT SOLAR CYCLE DEPENDENCE.
THIS MODEL CONTAINS UPPER AND LOWER LIMITS TO ACCURATELY PREDICT SOLAR CYCLES. THE AE17-HI FAVORS A FULLER APPROXIMATION WHILE AE17-LO IS MORE REASONABLE.
ALL THE DATA SETS PRESENTLY AVAILABLE TO NSSDC.
→ THE ACTUAL-VERSION-BAS-USED FOR THESE CALCULATIONS. <<

NOTE: TO OBTAIN THE DEGREE OF CONFIDENCE ONE WISHES TO ASSIGN TO RESULTS, NAMELY THAT FOR THE ACTUAL-VERSION-BAS-USED, ONE SHOULD CALCULATE FLUXES AT THE SMALLEST VALUES WHICH WILL NOT BE ENCOUNTERED IN ACTUALITY ENCOUNTERED DIFFERENT SITES.

IT IS NOT ADVISABLE TO EXTRAPOLATE THE SOLAR FLUX SPECIFICALLY TOWARD TOWARD THE CLOUDS LINE. THE FLUXES ARE NOT MEASURED DURING THE 20TH SOLAR CYCLE: 1964-1975. NO CERTAIN INFORMATION FOR #10 AND #933 #V.

TABLE 50

ORBITAL PLUTONIUM-238-106
 PARTICLE FLUXES IN THE INNER ZONE OF THE SOLAR SYSTEM
 DURING THE 1972-1973 SOLAR CYCLE
 AND INCLINATION OF THE VEHICLE
 MAXIMUM INFORMATION
 FOR INVESTIGATION
 OF THE SOLAR SYSTEM

DOSE IN SEP-TERMINATE ALUMINUM ZEUM
 MISSION DURATION: 2,600 VERDANT

SHIELD THICKNESS		ELECTRONS*		PROTONS		TOTAL	
(ALUMINUM)	(MM)	CUTERZN (GRADS-AL)	TOTAL (GRADS-AL)	AUDUN (GRADS-AL)	TOTAL (GRADS-AL)	DUC (GRADS-AL)	TOTAL (GRADS-AL)
0.01	0.07	1.	1.60E-006	1.64E-006	1.61E-006	1.64E-006	1.64E-006
0.02	0.14	1.	1.90E-006	1.71E-006	1.91E-006	1.72E-006	1.72E-006
0.03	0.21	4.	2.51E-006	2.41E-006	2.52E-006	2.42E-006	2.42E-006
0.04	0.28	6.	3.55E-006	3.45E-006	3.56E-006	3.46E-006	3.46E-006
0.05	0.35	1.	4.55E-006	4.35E-006	4.56E-006	4.36E-006	4.36E-006
0.06	0.42	9.	7.77E-006	7.37E-006	7.78E-006	7.38E-006	7.38E-006
0.07	0.49	1.	9.00E-006	8.40E-006	9.01E-006	8.41E-006	8.41E-006
0.08	0.56	10.	1.26E-005	1.17E-005	1.27E-005	1.18E-005	1.18E-005
0.09	0.63	1.	1.48E-005	1.37E-005	1.49E-005	1.38E-005	1.38E-005
0.10	0.70	12.	1.85E-005	1.70E-005	1.86E-005	1.71E-005	1.71E-005
0.11	0.77	29.	2.25E-005	2.05E-005	2.26E-005	2.06E-005	2.06E-005
0.12	0.84	1.	2.65E-005	2.42E-005	2.66E-005	2.43E-005	2.43E-005
0.13	0.91	58.	3.06E-005	2.81E-005	3.07E-005	2.82E-005	2.82E-005
0.14	0.98	1.	3.46E-005	3.13E-005	3.47E-005	3.14E-005	3.14E-005
0.15	1.05	87.	3.97E-005	3.52E-005	3.98E-005	3.53E-005	3.53E-005
0.16	1.12	1.	4.48E-005	4.03E-005	4.49E-005	4.04E-005	4.04E-005
0.17	1.19	117.	5.00E-005	4.51E-005	5.01E-005	4.52E-005	4.52E-005
0.18	1.26	4.	5.53E-005	5.04E-005	5.54E-005	5.05E-005	5.05E-005
0.19	1.33	219.	6.16E-005	5.67E-005	6.17E-005	5.68E-005	5.68E-005
0.20	1.40	1.	6.82E-005	6.34E-005	6.83E-005	6.35E-005	6.35E-005
0.21	1.47	58.	7.50E-005	6.92E-005	7.51E-005	6.93E-005	6.93E-005
0.22	1.54	1.	8.20E-005	7.60E-005	8.21E-005	7.61E-005	7.61E-005
0.23	1.61	87.	8.90E-005	8.30E-005	8.91E-005	8.31E-005	8.31E-005
0.24	1.68	1.	9.60E-005	9.00E-005	9.61E-005	9.01E-005	9.01E-005
0.25	1.75	219.	1.03E-004	9.70E-005	1.04E-004	9.71E-005	9.71E-005
0.26	1.82	1.	1.10E-004	1.04E-004	1.11E-004	1.05E-004	1.05E-004
0.27	1.89	219.	1.17E-004	1.11E-004	1.18E-004	1.12E-004	1.12E-004
0.28	1.96	1.	1.24E-004	1.20E-004	1.25E-004	1.21E-004	1.21E-004
0.29	2.03	58.	1.31E-004	1.27E-004	1.32E-004	1.28E-004	1.28E-004
0.30	2.10	1.	1.38E-004	1.34E-004	1.39E-004	1.35E-004	1.35E-004
0.31	2.17	87.	1.45E-004	1.41E-004	1.46E-004	1.42E-004	1.42E-004
0.32	2.24	1.	1.52E-004	1.48E-004	1.53E-004	1.49E-004	1.49E-004
0.33	2.31	219.	1.59E-004	1.55E-004	1.60E-004	1.56E-004	1.56E-004
0.34	2.38	1.	1.66E-004	1.62E-004	1.67E-004	1.63E-004	1.63E-004
0.35	2.45	58.	1.73E-004	1.69E-004	1.74E-004	1.70E-004	1.70E-004
0.36	2.52	1.	1.80E-004	1.76E-004	1.81E-004	1.77E-004	1.77E-004
0.37	2.59	87.	1.87E-004	1.83E-004	1.88E-004	1.84E-004	1.84E-004
0.38	2.66	1.	1.94E-004	1.90E-004	1.95E-004	1.91E-004	1.91E-004
0.39	2.73	219.	2.01E-004	1.97E-004	2.02E-004	1.98E-004	1.98E-004
0.40	2.80	1.	2.08E-004	2.04E-004	2.09E-004	2.05E-004	2.05E-004
0.41	2.87	58.	2.15E-004	2.11E-004	2.16E-004	2.12E-004	2.12E-004
0.42	2.94	1.	2.22E-004	2.18E-004	2.23E-004	2.19E-004	2.19E-004
0.43	3.01	87.	2.29E-004	2.25E-004	2.30E-004	2.26E-004	2.26E-004
0.44	3.08	1.	2.36E-004	2.32E-004	2.37E-004	2.38E-004	2.38E-004
0.45	3.15	219.	2.43E-004	2.39E-004	2.44E-004	2.45E-004	2.45E-004
0.46	3.22	1.	2.50E-004	2.46E-004	2.51E-004	2.52E-004	2.52E-004
0.47	3.29	58.	2.57E-004	2.53E-004	2.58E-004	2.59E-004	2.59E-004
0.48	3.36	1.	2.64E-004	2.60E-004	2.65E-004	2.66E-004	2.66E-004
0.49	3.43	87.	2.71E-004	2.67E-004	2.72E-004	2.73E-004	2.73E-004
0.50	3.50	1.	2.78E-004	2.74E-004	2.79E-004	2.80E-004	2.80E-004
0.51	3.57	219.	2.85E-004	2.81E-004	2.86E-004	2.87E-004	2.87E-004
0.52	3.64	1.	2.92E-004	2.88E-004	2.93E-004	2.94E-004	2.94E-004
0.53	3.71	58.	2.99E-004	2.95E-004	3.00E-004	3.01E-004	3.01E-004
0.54	3.78	1.	3.06E-004	3.02E-004	3.07E-004	3.08E-004	3.08E-004
0.55	3.85	87.	3.13E-004	3.09E-004	3.14E-004	3.15E-004	3.15E-004
0.56	3.92	1.	3.20E-004	3.16E-004	3.21E-004	3.22E-004	3.22E-004
0.57	3.99	219.	3.27E-004	3.23E-004	3.28E-004	3.29E-004	3.29E-004
0.58	4.06	1.	3.34E-004	3.30E-004	3.35E-004	3.36E-004	3.36E-004
0.59	4.13	58.	3.41E-004	3.37E-004	3.42E-004	3.43E-004	3.43E-004
0.60	4.20	1.	3.48E-004	3.44E-004	3.49E-004	3.50E-004	3.50E-004
0.61	4.27	87.	3.55E-004	3.51E-004	3.56E-004	3.57E-004	3.57E-004
0.62	4.34	1.	3.62E-004	3.58E-004	3.63E-004	3.64E-004	3.64E-004
0.63	4.41	219.	3.69E-004	3.65E-004	3.70E-004	3.71E-004	3.71E-004
0.64	4.48	1.	3.76E-004	3.72E-004	3.77E-004	3.78E-004	3.78E-004
0.65	4.55	58.	3.83E-004	3.79E-004	3.84E-004	3.85E-004	3.85E-004
0.66	4.62	1.	3.90E-004	3.86E-004	3.91E-004	3.92E-004	3.92E-004
0.67	4.69	87.	3.97E-004	3.93E-004	4.02E-004	4.01E-004	4.01E-004
0.68	4.76	1.	4.04E-004	3.99E-004	4.05E-004	4.06E-004	4.06E-004
0.69	4.83	219.	4.11E-004	4.06E-004	4.12E-004	4.13E-004	4.13E-004
0.70	4.90	1.	4.18E-004	4.13E-004	4.19E-004	4.20E-004	4.20E-004
0.71	4.97	58.	4.25E-004	4.19E-004	4.26E-004	4.27E-004	4.27E-004
0.72	5.04	1.	4.32E-004	4.27E-004	4.33E-004	4.34E-004	4.34E-004
0.73	5.11	87.	4.39E-004	4.34E-004	4.40E-004	4.41E-004	4.41E-004
0.74	5.18	1.	4.46E-004	4.41E-004	4.47E-004	4.48E-004	4.48E-004
0.75	5.25	219.	4.53E-004	4.48E-004	4.54E-004	4.55E-004	4.55E-004
0.76	5.32	1.	4.60E-004	4.55E-004	4.61E-004	4.62E-004	4.62E-004
0.77	5.39	58.	4.67E-004	4.62E-004	4.68E-004	4.69E-004	4.69E-004
0.78	5.46	1.	4.74E-004	4.69E-004	4.75E-004	4.76E-004	4.76E-004
0.79	5.53	87.	4.81E-004	4.76E-004	4.82E-004	4.83E-004	4.83E-004
0.80	5.60	1.	4.88E-004	4.83E-004	4.94E-004	4.95E-004	4.95E-004
0.81	5.67	219.	4.95E-004	4.90E-004	5.00E-004	5.01E-004	5.01E-004
0.82	5.74	1.	5.02E-004	4.97E-004	5.07E-004	5.08E-004	5.08E-004
0.83	5.81	58.	5.09E-004	5.04E-004	5.14E-004	5.15E-004	5.15E-004
0.84	5.88	1.	5.16E-004	5.11E-004	5.21E-004	5.22E-004	5.22E-004
0.85	5.95	87.	5.23E-004	5.18E-004	5.28E-004	5.29E-004	5.29E-004
0.86	6.02	1.	5.30E-004	5.25E-004	5.35E-004	5.36E-004	5.36E-004
0.87	6.09	219.	5.37E-004	5.32E-004	5.42E-004	5.43E-004	5.43E-004
0.88	6.16	1.	5.44E-004	5.39E-004	5.50E-004	5.51E-004	5.51E-004
0.89	6.23	58.	5.51E-004	5.46E-004	5.56E-004	5.57E-004	5.57E-004
0.90	6.30	1.	5.58E-004	5.53E-004	5.63E-004	5.64E-004	5.64E-004
0.91	6.37	87.	5.65E-004	5.60E-004	5.70E-004	5.71E-004	5.71E-004
0.92	6.44	1.	5.72E-004	5.67E-004	5.77E-004	5.78E-004	5.78E-004
0.93	6.51	219.	5.79E-004	5.74E-004	5.84E-004	5.85E-004	5.85E-004
0.94	6.58	1.	5.86E-004	5.81E-004	5.91E-004	5.92E-004	5.92E-004
0.95	6.65	58.	5.93E-004	5.88E-004	5.98E-004	5.99E-004	5.99E-004
0.96	6.72	1.	6.00E-004	5.95E-004	6.05E-004	6.06E-004	6.06E-004
0.97	6.79	87.	6.07E-004	6.02E-004	6.12E-004	6.13E-004	6.13E-004
0.98	6.86	1.	6.14E-004	6.09E-004	6.19E-004	6.20E-004	6.20E-004
0.99	6.93	219.	6.21E-004	6.16E-004	6.26E-004	6.27E-004	6.27E-004
1.00	7.00	1.	6.28E-004	6.23E-004	6.33E-004	6.34E-004	6.34E-004
1.01	7.07	58.	6.35E-004	6.30E-004	6.40E-004	6.41E-004	6.41E-004
1.02	7.14	1.	6.42E-004	6.37E-004	6.50E-004	6.51E-004	6.51E-004
1.03	7.21	87.	6.49E-004	6.44E-004	6.58E-004	6.59E-004	6.59E-004
1.04	7.28	1.	6.56E-004	6.51E-004	6.65E-004	6.66E-004	6.66E-004
1.05	7.35	219.	6.63E-004	6.58E-004	6.72E-004	6.73E-004	6.73E-004
1.06	7.42	1.	6.70E-004	6.65E-004	6.80E-004	6.81E-004	6.81E-004
1.07	7.49	58.	6.77E-004	6.72E-004	6.86E-004	6.87E-004	6.87E-0

ELECTRICAL MODELS:

EE: INTRK ZONE-51AF MAX INC. INCORPORATING FACTOR WAS AFFILIATED WITH THE MUNICIPAL GOVERNMENT.

EIT: DUTEE ZONE-INTEGRIN MODEL WITH SCALAR CYCLES. FINANCIALS.
FOR ENERGY'S AEGC 100 REV. CANTERBURY AGC
LUMI LIMIT VALUET ACCOUNT FOR DISCHARGE FUNDAMENTALLY
EXISTING DATA SITE. THE ALREADY FAVERS VANFOLKES FUND
TODAY'S DATA WHILE AEGC IS MORE REPRESENTATIVE OF
ALL THE DATA SITE OFF. SOILNLY AVAILABLE IF TECHNIC.

=> THE AEGC WESTERN WAS USED FOR THESE CALCULATIONS. <<

OTON WOODL :
PHOTOGRAPHIC STYLING MAX
IN UNCERTAINITY FACTOR WAS AFFILIATED THE MUSEUM.

卷之三

THE PLAT FORMS AT THE
INTERFLUVIAL PLAINS THAT
ARE WELL SPREAD OVER.

ARTISTS : *THE BOSTON CONCERTO GROUP* (with special guest artist, *JOHN DURRANT*) will present a program of classical and contemporary music at the *Wellesley Center for the Arts*, Wellesley College, on Saturday, April 21, at 8 p.m. The program includes works by Brahms, Schubert, Beethoven, Debussy, Ravel, Prokofiev, and Stravinsky.

THE CLOTHESLINE IS DOWN AGAIN. THE CLOTHESLINE IS DOWN AGAIN.

TABLE 52

**-25E IN SEMI-INFINITE ALUMINUM MEDIUM
MISSION DURATION: 5,0000 YEARS)

SAFETY: OUTER ZONE INTERACTION WITHIN THE CLASS CYCLE CONFIDENCE BOUNDARIES ACHIEVEABLE WHEN THE USE OF CONTAINING UNITS, LOWER LIMIT VALUES, ACCOUNT FOR DISCRETE FANCY DATA AND EXISTING DATA SETS. THE ACTUAL DATA LAVES FINANCIAL BENEFIT FOR THE DATA SETS PRESENTLY AVAILABLE IN THE MARKET.

PRACTICAL MODEL:

NOTES ON THE USE OF THE CHART

سلسلة نشرات علمية

THE STAFF OF THE MAGNETIC SHIELDING AFFILIATED
74-141. OF AL EVENTS: * OF
STRUCTURE: THE SOURCE OF CONFIDENCE ONE IN SHES
ADVICE TO RECENTLY, NAFLY THAT FOR THE
SCIENTIFIC AND SIGN DRAILIN USE CALCULATED
THEIR VALUE WHICH WILL
BE ACCEPTED BY ACTUALLY ENCLUTERED
INDIVIDUALS.

IT IS NOT ADVISABLE TO EXTRAPOLATE THE SOLAR CYCLE LENGTHS FOR THEM TOWARD THE END OF THE CYCLE, WHICH ENERGIES BECAUSE OF THE DATA SETS USED IN THE CONSTRUCTION OF THE MODEL. SATELLITE FREQUENCIES MAY NOT CONTINUE DURING THE 2 CYCLES (1964-1975) DUE TO A LACK OF CCRAIN INFORMATION

ORBITAL FLUX STUDY WITH MAGNETIC POLARISATION
UNCERTAINTY FACTORS FOR APPLES AND
MAGNETIC COORDINATES AND MAPS
MANUFACTURED AND DISTRIBUTED BY
FOR INFORMATION OR ENT-ANAVATION CONTACT

THE AMERICAN ALBRIGHT MUSEUM
COLLECTIONS, 1890-1900

SHELL THICKNESS	SHELL LENGTHS.									
	S. CALUMINUM	TOTAL	INNER IN.	OUTER IN.	OUTER IN.	TOTAL	OUTER IN.	OUTER IN.	TOTAL	OUTER IN.
CONCHACEOUS	CONCAVE	CONCAVE	CONCAVE	CONCAVE	CONCAVE	CONCAVE	CONCAVE	CONCAVE	CONCAVE	CONCAVE
0.01	0.04	1.0	0.325	0.7	2.275	0.7	2.275	0.7	2.275	0.7
0.02	0.07	1.5	0.375	0.7	2.195	0.7	2.195	0.7	2.195	0.7
0.03	0.11	4.0	1.205	0.6	5.495	0.6	5.495	0.6	5.495	0.6
0.04	0.15	9.0	4.655	3.5	7.135	0.6	7.135	0.6	7.135	0.6
0.05	0.19	2.0	3.955	0.6	5.185	0.6	5.185	0.6	5.185	0.6
0.06	0.22	2.0	2.665	0.6	4.635	0.6	4.635	0.6	4.635	0.6
0.07	0.26	1.0	2.655	0.6	4.305	0.6	4.305	0.6	4.305	0.6
0.08	0.30	1.2	1.675	0.6	3.555	0.6	3.555	0.6	3.555	0.6
0.09	0.33	1.5	1.375	0.6	3.715	0.6	3.715	0.6	3.715	0.6
0.10	0.37	1.5	1.375	0.6	3.715	0.6	3.715	0.6	3.715	0.6
0.20	0.74	4.9	2.155	1.5	3.155	0.6	3.155	0.6	3.155	0.6
0.30	1.11	4.6	2.345	2.4	7.515	0.5	7.515	0.5	7.515	0.5
0.40	1.48	5.9	2.725	0.6	6.615	0.5	6.615	0.5	6.615	0.5
0.50	1.85	7.3	4.555	0.5	2.555	0.5	2.555	0.5	2.555	0.5
0.60	2.32	6.7	5.125	0.5	1.665	0.5	1.665	0.5	1.665	0.5
0.70	2.66	11.7	5.125	0.5	9.775	0.4	9.775	0.4	9.775	0.4
1.00	3.70	1.46	4.655	0.2	5.157	0.4	5.157	0.4	5.157	0.4
1.20	4.55	1.02	4.055	0.2	5.055	0.4	5.055	0.4	5.055	0.4
1.50	5.56	2.19	4.155	0.1	4.655	0.4	4.655	0.4	4.655	0.4
1.60	6.48	2.55	4.325	0.1	4.905	0.3	4.905	0.3	4.905	0.3
2.00	7.41	2.92	4.127	-0.1	4.337	0.3	4.337	0.3	4.337	0.3
2.60	9.26	3.65	6.0	-0.1	7.665	0.1	7.665	0.1	7.665	0.1
3.00	11.4	4.32	6.0	-0.1	4.885	0.0	4.885	0.0	4.885	0.0
3.50	12.06	5.10	6.0	-0.1	3.32E-03	-0.1	3.32E-03	-0.1	3.32E-03	-0.1
4.00	14.81	5.85	6.0	-0.1	0.0	0.0	0.0	0.0	0.0	0.0
4.50	16.27	6.55	6.0	-0.1	0.0	0.0	0.0	0.0	0.0	0.0
5.00	16.52	7.29	6.0	-0.1	0.0	0.0	0.0	0.0	0.0	0.0
6.00	21.22	8.75	6.0	-0.1	0.0	0.0	0.0	0.0	0.0	0.0
8.00	26.67	11.05	6.0	-0.1	0.0	0.0	0.0	0.0	0.0	0.0
10.00	37.04	14.58	6.0	-0.1	0.0	0.0	0.0	0.0	0.0	0.0

CHILDHOOD IN ILLNESS

S		GROWTH AND REPRODUCTION		INVESTMENT		LITERATURE		TOTAL	
		ANNUAL	ANNUAL	ANNUAL	ANNUAL	ANNUAL	ANNUAL	ANNUAL	ANNUAL
0.001	0.64	1.6	0.37E	C7	2.71E	C7	4.69E	0.7	4.69E
0.002	0.07	3.0	1.17E	C7	1.49E	C7	2.49E	0.7	2.49E
0.003	0.11	4.0	2.02E	C6	3.41E	C5	1.47E	0.7	1.47E
0.004	0.15	9.0	4.62E	C6	7.03E	C5	1.20E	0.7	1.20E
0.005	0.19	7.0	3.5CE	C6	4.50E	C6	0.319E	0.6	0.319E
0.006	0.22	9.0	4.62E	C6	4.61E	C6	0.507E	0.6	0.507E
0.007	0.26	10.0	5.6CE	C6	5.62E	C6	0.223E	0.6	0.223E
0.008	0.30	12.0	1.67E	C7	3.65E	C6	5.27E	1.0	5.27E
0.009	0.33	13.0	1.37E	C7	3.17E	C6	4.54E	1.0	4.54E
0.010	0.37	15.0	1.79E	C7	3.29E	C6	4.89E	0.6	4.89E
0.020	0.74	2.0	2.43E	C5	1.3CE	C5	1.651E	0.6	1.651E
0.020	1.11	4.0	6.23E	C6	7.52E	C5	0.154E	0.5	0.154E
0.040	1.48	5.0	2.07E	C6	4.64E	C5	0.821E	0.5	0.821E
0.050	1.85	7.0	9.05E	C5	2.65E	C5	3.05E	0.5	3.05E
0.060	2.22	9.0	1.12E	C5	2.65E	C5	2.01E	0.5	2.01E
0.080	2.95	11.0	1.47E	C7	5.5AE	C4	9.27E	0.4	9.27E
0.100	3.70	14.0	4.66E	C7	6.88E	C4	2.04E	0.4	2.04E
0.200	6.53	18.2	1.04E	C7	2.67E	C5	2.38E	0.4	2.38E
0.500	5.56	21.0	6.159E	C1	1.6CE	C4	1.56E	0.4	1.56E
1.250	6.48	25.5	3.730E	C1	4.0CE	C3	4.066E	0.3	4.066E
3.000	7.41	29.0	4.127E	C1	1.37E	C3	1.37E	0.3	1.37E
8.000	9.26	36.5	6.0CE	C1	7.0CE	C1	7.0CE	0.1	7.0CE
20.000	12.96	42.0	6.0CE	C1	1.39E	C1	1.39E	0.1	1.39E
50.000	14.81	58.0	0.0C	C1	1.312E	C1	1.312E	0.1	1.312E
100.000	16.52	65.0	0.0C	C1	0.0	C1	0.0	0.0	0.0
200.000	18.22	72.0	0.0C	C1	0.0	C1	0.0	0.0	0.0
400.000	19.66	11.00	0.0C	C1	0.0	C1	0.0	0.0	0.0
1000.000	37.04	14.58	3.0C	C1	0.0	C1	0.0	0.0	0.0

ELECTRON MOCCNESS:

E17: OUTER ZONE-INTEM MODEL WITHOUT SCALAR CYCLE DEPENDENCE FOR ENERGIES ABOVE 1.5 MEV. THIS MODEL CONTAINS SUPER-LOW ENERGY VALES TO ACCURATELY PREDICT THE VAN ALLEN BELT EXISTING DATA SETS. THE A17-H1 FAUCES VAN CLEEF'S FIT TO OVAL DATA WHILE A17-Z1 IS MORE REPRODUCITIVE OF ALL THE DATA SETS PRESENTLY AVAILABLE TO ASSDC.

THE PRACTICAL APPROACH TO THE DESIGN OF POLY(URIDYLIC ACID) ANALOGUE ANALOGUE

• SOLAR PRACTICE: "WHAT IS"

SOURCE: TWO PLANE PROJECTIONS AT 1 AU
AN ATTENDEE IN THE PLANE JARRY.
FOR CUTOFF DIPOLE SHELL OF S.E.R.

FIGURE 14. COMPOSITION OF ALL ELEMENTS
OF 1 AU. ELECTROMAGNETIC SHIELDING AFFILIATED
WITH THE EARTH.

PRACTICAL MODELS:

REPRODUCED BY PERMISSION OF THE PUBLISHER
NO UNCERTAINTY FACTOR WAS APPLIED TO THE MODEL DATA

TABLE 54

IT IS NOT ADVISABLE TO EXTRAPOLATE THE SCALAR-
PRESSURE COEFFICIENTS TOWARD LOWER FREQUENCIES
BECAUSE THE DATA SETS USED IN THE CONSTRUCTION OF THE MODEL ISAIED-
SCALAR PRESSURE COEFFICIENTS MADE DURING THE 20TH SCALAR
(CYCLES 1944-1957) DO NOT CONTAIN INFORMATION
FOR CYCLES 1945 AND 1950.

DOSE AT CENTER OF ALUMINUM SPHERE FOR MISSON DURATION: 50000 YEARS										
SHIED THICKNESS (ALUMINUM) Spherical Cylinders	ELECTRONS			BREMSSTRAHLING			PROTONS			TOTAL DOSE ALL SOURCES (RAD-sec)
	INNER ZN, Cyl-Spherical Cylinders	OUTER ZN, Cyl-Spherical Cylinders	TOTAL ZN, Cyl-Spherical Cylinders	THIN GLASS-AL.	MEDIUM GLASS-AL.	THICK GLASS-AL.	THIN GLASS-AL.	MEDIUM GLASS-AL.	THICK GLASS-AL.	
0.01	0.04	1.6	1.143E-38	3.713E-38	1.177E-38	4.685E-38	0.4	2.762E-38	0.6	1.978E-38
0.02	0.07	5.6	7.686E-37	2.124E-36	9.694E-37	3.763E-36	3.4	1.282E-36	0.6	1.264E-36
0.03	0.11	4.0	5.582E-37	1.646E-36	6.743E-37	3.081E-36	0.4	9.194E-36	0.2	5.160E-36
0.04	0.15	6.0	4.081E-37	1.281E-36	4.221E-37	2.560E-36	0.4	7.324E-36	0.3	3.747E-36
0.05	0.19	7.0	3.027E-37	1.362E-36	3.135E-37	2.214E-36	0.4	6.163E-36	0.2	2.637E-36
0.06	0.22	9.0	2.266E-37	9.393E-37	2.359E-37	2.035E-36	0.7	1.934E-35	0.5	2.060E-35
0.07	0.26	1.0	1.704E-37	2.888E-35	1.788E-37	1.644E-35	0.4	5.016E-35	0.5	5.504E-35
0.08	0.30	1.2	1.300E-37	6.897E-35	1.363E-37	1.423E-35	0.4	6.187E-35	0.5	6.390E-35
0.09	0.33	1.3	9.968E-38	6.148E-35	1.058E-37	1.251E-35	0.4	4.287E-35	0.5	4.305E-35
0.10	0.37	1.5	7.687E-38	5.191E-35	8.237E-38	1.102E-35	0.4	3.982E-35	0.5	2.377E-35
0.20	0.74	29.	1.123E-36	8.242E-35	1.405E-36	0.531E-35	0.2	2.437E-35	0.5	2.655E-35
0.30	1.11	44.	3.881E-36	1.915E-35	5.798E-36	3.426E-35	0.3	1.785E-35	0.5	1.656E-35
0.40	1.66	58.	1.962E-36	1.356E-35	3.321E-36	2.647E-35	0.3	1.419E-35	0.5	1.762E-35
0.50	1.95	73.	1.107E-35	9.590E-35	2.156E-35	1.688E-35	0.3	1.128E-35	0.5	1.376E-35
0.60	2.22	87.	7.927E-36	6.282E-35	1.272E-35	1.012E-35	0.3	8.015E-36	0.5	2.526E-35
0.80	2.66	117.	4.008E-36	3.591E-34	7.593E-34	1.444E-33	0.3	8.205E-34	0.4	1.608E-35
1.00	3.17	146.	2.113E-36	2.121E-34	4.236E-34	1.194E-33	0.4	1.103E-33	0.4	1.142E-35
1.25	4.63	192.	7.805E-37	1.256E-34	2.922E-34	5.878E-34	0.4	6.100E-34	0.4	8.399E-36
1.50	5.56	219.	1.065E-36	6.923E-35	1.789E-34	9.459E-34	0.2	5.486E-34	0.4	5.510E-34
1.75	6.46	255.	2.881E-36	3.352E-35	3.664E-34	7.422E-34	0.2	5.004E-34	0.4	6.175E-34
2.00	7.41	292.	4.075E-36	1.479E-35	5.179E-35	6.635E-34	0.2	4.052E-34	0.4	5.795E-34
2.50	9.26	365.	1.594E-01	1.396E-01	1.347E-01	5.549E-02	0.2	4.529E-02	0.4	4.412E-04
3.00	1.12	432.	0.0	5.202E-03	5.202E-03	5.202E-03	0.2	3.902E-03	0.4	3.924E-04
3.50	1.26	510.	0.0	1.573E-03	3.573E-03	4.131E-03	0.2	3.433E-02	0.4	3.934E-04
4.00	1.49	583.	0.0	1.573E-03	0.0	0.0	0.2	3.292E-02	0.4	3.648E-04
5.00	1.88	666.	0.0	0.0	0.0	0.0	0.2	3.071E-02	0.4	3.048E-04
6.00	2.22	825.	0.0	0.0	0.0	0.0	0.2	3.302E-02	0.4	3.217E-04
6.00	2.26	873.	0.0	0.0	0.0	0.0	0.2	3.081E-02	0.4	3.235E-04
10.00	37.04	1458.	0.0	0.0	0.0	0.0	0.2	2.994E-02	0.4	2.424E-04
10.00	37.04	1476.	0.0	0.0	0.0	0.0	0.2	3.350E-02	0.4	3.388E-04

ECCLESIA 5 DEI 33

1.66: INNER ZONE - SOLAR MAX NO UNCERTAINTY EAST TO

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SOLPRO: SOLAR FLARE PRECTIONS AT 1 AU
LUSATIENNALE PLANETARY
FIG. 24.10E DISSIPATIVE SHELL OF S.F.B.

FIG. 11: OUTER ZONE-INTERIM MODEL WITHOUT SOLAR CYCLE DEPENDENCE.
FOR ENERGIES ABOVE 1.5 MFV. THIS MODEL CONTAINS URGENT
DATA FROM THE GEOTAIL MAGNETIC FIELD SHIFTING APPLIED

NOTE: δ DENOTES THE DEGREE OF CONFIDENCE ONE ASSIGNS TO RESULTS, NAMELY THAT FOR THE δ PERCENTAGE OF THE TIME THE PREDICTION IS CORRECT.

ALL THE DATA SETS PRESENTLY AVAILABLE TO NSSDC.

THE HISTORY OF THE CHURCH OF ENGLAND

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N MODEL:

TIAA-CREF PENSIONS—SDI LAB MAX

L DATA

IT IS NOT ADVISABLE TO EXTRAPOLATE THE SOLAR ROTATION SPECTRA TOWARDS LOWER AND TOWARDS HIGHER FREQUENCIES BECAUSE THE DATA SET USED IN THE CONSTRUCTION OF THE MODEL IS BASED ON OBSERVATIONS MADE DURING THE 20TH SOLAR CYCLE (1964-1975) DC NOT CONTAIN INFORMATION

MISSION DURATION: 50000 YEARS

* ELECTRON MODEL S:
AEG: INNER ZONE
NO UNCERTA

+ SOLAR PROTON MODEL:
SOLPRO: SOLAR FLARE
CHARTS: CHARTS

AET17: OUTER ZONE-INTERIM MODEL WITHOUT SCALAR CYCLE DEPENDENCE.
FOR ENERGIES ABOVE 1.5 MeV. THIS MODEL CONTAINS AN UPPER
LIMIT FOR THE ENERGY AT WHICH THE MODEL IS APPLIED.
THE ENERGY IS DETERMINED BY THE NUMBER OF SCATTERING VECTORS
IN THE DATA SETS. THE AET17-41 FALLOFF VARIATION IS
APPLIED TO ALL THE DATA SETS. MORE REPRESENTATIVE USE
OF THE DATA SETS PRESENTLY AVAILABLE TO NSSDC.
NOTE: 2 DEGREES OF CONFIDENCE CAN WISHES
TO ASSIGN TO RESULTS. NAMELY THAT FOR THE
SPECIFIC MISSION BALIKA THE CALCULATED
FLUXES ARE THE SMALLEST VALUES WHICH WILL
NOT BE AFFECTIONED BY ACTUALLY ENCOUNTERED
INTERFACED.

* * PROTON MODEL :
AP-MAC: TRAP NO UN

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IT IS NOT ADVISABLE TO EXTRAPOLATE THE SOLAR PROTON SPECTRA NEITHER TOWARDS LOWER NOR TOWARDS HIGHER ENERGIES BECAUSE THE DATA SETS USED IN THE CONSTRUCTION OF THE MODEL (SALE) ARE LIMITED TO A SUITE OF MEASUREMENTS MADE DURING THE 20TH SOLAR CYCLE (1964-1975) WHICH DO NOT CONTAIN INFORMATION

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DCSE AT CENTER CP ALUMINUM SPIDER 25
MISSION DURATION: 5,0000 YEARS)

ELECTRON MODELS:

FIGURE 6: INNER ZONE-SOLAR MAX NO UNCERTAINTY FACTOR WAS APPLIED TO THE MODEL DATA

NSDC: OUTER ZONE-INTERIOR MODEL WITH THE SOLAR CYCLE DEPENDENCE.
1. THIS MODEL CONTAINS NO UNDERLYING PHYSICAL MECHANISMS.
2. THE DATA SETS TO ACCOUNT FOR DISCREPANCY BETWEEN
EXISTING DATA AND THE AEI-11 FAVORABLE COLLABORATION.
3. THE DATA SETS ARE AVAILABLE TO ALL THE DATA PRESENTLY AVAILABLE TO NSDC.

SOLAR POWER PLANT

4.4.4: * DENTAL SPECIMENS ARE COLLECTED AND CALCULATED FOR THE ACTUAL SIZE OF THE MOUTH. THE DENTAL SPECIMENS ARE THEN USED TO DETERMINE THE POSITION OF THE TEETH IN THE MOUTH. THE DENTAL SPECIMENS ARE THEN USED TO DETERMINE THE POSITION OF THE TEETH IN THE MOUTH.

IT IS NOT ADVISABLE TO EXTRAPOLATE THE SOLAR PROTON SPECTRA NEITHER TOWARDS LOWER NOR TOWARDS HIGHER ENERGIES BECAUSE THE DATA SETS USED IN THE CONSTRUCTION OF THE MODEL (SATELLITE MEASUREMENTS OF 20TH SOLAR CYCLE 1947-1975) DO NOT CONTAIN INFORMATION

1921-57

SHIELD THICKNESS		ELECTRONS		TOTAL	
(ALUMINIUM)	T	INNER 2N	CUTER 2N	2N	2N - ALU
0.00	0.00	0.00	0.00	0.00	0.00
0.01	0.01	0.00	0.00	0.00	0.00
0.02	0.02	0.00	0.00	0.00	0.00
0.03	0.03	0.00	0.00	0.00	0.00
0.04	0.04	0.00	0.00	0.00	0.00
0.05	0.05	0.00	0.00	0.00	0.00
0.06	0.06	0.00	0.00	0.00	0.00
0.07	0.07	0.00	0.00	0.00	0.00
0.08	0.08	0.00	0.00	0.00	0.00
0.09	0.09	0.00	0.00	0.00	0.00
0.10	0.10	0.00	0.00	0.00	0.00
0.11	0.11	0.00	0.00	0.00	0.00
0.12	0.12	0.00	0.00	0.00	0.00
0.13	0.13	0.00	0.00	0.00	0.00
0.14	0.14	0.00	0.00	0.00	0.00
0.15	0.15	0.00	0.00	0.00	0.00
0.16	0.16	0.00	0.00	0.00	0.00
0.17	0.17	0.00	0.00	0.00	0.00
0.18	0.18	0.00	0.00	0.00	0.00
0.19	0.19	0.00	0.00	0.00	0.00
0.20	0.20	0.00	0.00	0.00	0.00
0.21	0.21	0.00	0.00	0.00	0.00
0.22	0.22	0.00	0.00	0.00	0.00
0.23	0.23	0.00	0.00	0.00	0.00
0.24	0.24	0.00	0.00	0.00	0.00
0.25	0.25	0.00	0.00	0.00	0.00
0.26	0.26	0.00	0.00	0.00	0.00
0.27	0.27	0.00	0.00	0.00	0.00
0.28	0.28	0.00	0.00	0.00	0.00
0.29	0.29	0.00	0.00	0.00	0.00
0.30	0.30	0.00	0.00	0.00	0.00
0.31	0.31	0.00	0.00	0.00	0.00
0.32	0.32	0.00	0.00	0.00	0.00
0.33	0.33	0.00	0.00	0.00	0.00
0.34	0.34	0.00	0.00	0.00	0.00
0.35	0.35	0.00	0.00	0.00	0.00
0.36	0.36	0.00	0.00	0.00	0.00
0.37	0.37	0.00	0.00	0.00	0.00
0.38	0.38	0.00	0.00	0.00	0.00
0.39	0.39	0.00	0.00	0.00	0.00
0.40	0.40	0.00	0.00	0.00	0.00
0.41	0.41	0.00	0.00	0.00	0.00
0.42	0.42	0.00	0.00	0.00	0.00
0.43	0.43	0.00	0.00	0.00	0.00
0.44	0.44	0.00	0.00	0.00	0.00
0.45	0.45	0.00	0.00	0.00	0.00
0.46	0.46	0.00	0.00	0.00	0.00
0.47	0.47	0.00	0.00	0.00	0.00
0.48	0.48	0.00	0.00	0.00	0.00
0.49	0.49	0.00	0.00	0.00	0.00
0.50	0.50	0.00	0.00	0.00	0.00
0.51	0.51	0.00	0.00	0.00	0.00
0.52	0.52	0.00	0.00	0.00	0.00
0.53	0.53	0.00	0.00	0.00	0.00
0.54	0.54	0.00	0.00	0.00	0.00
0.55	0.55	0.00	0.00	0.00	0.00
0.56	0.56	0.00	0.00	0.00	0.00
0.57	0.57	0.00	0.00	0.00	0.00
0.58	0.58	0.00	0.00	0.00	0.00
0.59	0.59	0.00	0.00	0.00	0.00
0.60	0.60	0.00	0.00	0.00	0.00
0.61	0.61	0.00	0.00	0.00	0.00
0.62	0.62	0.00	0.00	0.00	0.00
0.63	0.63	0.00	0.00	0.00	0.00
0.64	0.64	0.00	0.00	0.00	0.00
0.65	0.65	0.00	0.00	0.00	0.00
0.66	0.66	0.00	0.00	0.00	0.00
0.67	0.67	0.00	0.00	0.00	0.00
0.68	0.68	0.00	0.00	0.00	0.00
0.69	0.69	0.00	0.00	0.00	0.00
0.70	0.70	0.00	0.00	0.00	0.00
0.71	0.71	0.00	0.00	0.00	0.00
0.72	0.72	0.00	0.00	0.00	0.00
0.73	0.73	0.00	0.00	0.00	0.00
0.74	0.74	0.00	0.00	0.00	0.00
0.75	0.75	0.00	0.00	0.00	0.00
0.76	0.76	0.00	0.00	0.00	0.00
0.77	0.77	0.00	0.00	0.00	0.00
0.78	0.78	0.00	0.00	0.00	0.00
0.79	0.79	0.00	0.00	0.00	0.00
0.80	0.80	0.00	0.00	0.00	0.00
0.81	0.81	0.00	0.00	0.00	0.00
0.82	0.82	0.00	0.00	0.00	0.00
0.83	0.83	0.00	0.00	0.00	0.00
0.84	0.84	0.00	0.00	0.00	0.00
0.85	0.85	0.00	0.00	0.00	0.00
0.86	0.86	0.00	0.00	0.00	0.00
0.87	0.87	0.00	0.00	0.00	0.00
0.88	0.88	0.00	0.00	0.00	0.00
0.89	0.89	0.00	0.00	0.00	0.00
0.90	0.90	0.00	0.00	0.00	0.00
0.91	0.91	0.00	0.00	0.00	0.00
0.92	0.92	0.00	0.00	0.00	0.00
0.93	0.93	0.00	0.00	0.00	0.00
0.94	0.94	0.00	0.00	0.00	0.00
0.95	0.95	0.00	0.00	0.00	0.00
0.96	0.96	0.00	0.00	0.00	0.00
0.97	0.97	0.00	0.00	0.00	0.00
0.98	0.98	0.00	0.00	0.00	0.00
0.99	0.99	0.00	0.00	0.00	0.00
1.00	1.00	0.00	0.00	0.00	0.00

FIELD TICKNESS

EFFECTS

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TOTAL

ELECTRON MODEL:

ELECTION MODELS: **STAFF: TURNER 70 DEF-COLLAGE MAX**

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NO-UNCERTAINTY-FAC1R-LAS AFFILIATE TO THE NCCC DATA.

AET7: OUTER ZONE-INTERIM MODEL WITH 1 SCALAR CYCLE CERTAINTY.
FOR ENERGIES ABOVE 10 MEV. THIS CELL COUNTS UP TO 6 LOWER LIMIT VALUES TO ACCOUNT FOR DISCREPANCY BETWEEN EXISTING DATA SETS.
TO OBTAIN DATA WHILE JETFLY-12 IS IN CYCLE REPRESENTATIVE ALL THE DATA SETS CURRENTLY AVAILABLE TO NCCC.

CHAPTER 10: CLIFFS IN THERAPEUTIC CONTEXT

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INFECTION IS A VISIBLE, TO X-RAYABLE, TRIVISUAL EFFECT OF SPECIFIC AND INTRINSICLY LEADING CAUSES WHICH ARE LEADERS OF INFECTION OR THE LOCAL ISOLATE WHICH CAUSES MACROSCOPIC MANIFESTATIONS WHICH ARE CLINICALLY IDENTIFIED AS AN INFECTION.

DATE OF ALUMINUM SHEET
MANUFACTURE: 5 JUNE 1961
MISSION DURATION: 5 JUNE 1961

SPELLED IN FRENCH		CALCULATED IN FRENCH		LINEAR FRENCH		SOUND-ALIKE FRENCH	
S	T	S	T	S	T	S	T
1.01	C.CA	1.		C.CC	CC	1.452	27
0.02	D.DT	-75		D.DT	DT	1.452	27
0.03	D.DT	0.1	4.	D.DT	DT	1.452	27
2.04	D.DT	0.1	5.	D.DT	DT	1.452	27
0.05	D.DT	0.1	6.	D.DT	DT	1.452	27
0.06	D.DT	0.2	1.	D.DT	DT	1.452	27
0.07	D.DT	0.2	2.	D.DT	DT	1.452	27
0.08	D.DT	0.2	3.	D.DT	DT	1.452	27
0.09	D.DT	0.2	4.	D.DT	DT	1.452	27
0.10	D.DT	0.2	5.	D.DT	DT	1.452	27
0.11	D.DT	0.2	6.	D.DT	DT	1.452	27
0.12	D.DT	0.2	7.	D.DT	DT	1.452	27
0.13	D.DT	0.2	8.	D.DT	DT	1.452	27
0.14	D.DT	0.2	9.	D.DT	DT	1.452	27
0.15	D.DT	0.2	10.	D.DT	DT	1.452	27
0.16	D.DT	0.2	11.	D.DT	DT	1.452	27
0.17	D.DT	0.2	12.	D.DT	DT	1.452	27
0.18	D.DT	0.2	13.	D.DT	DT	1.452	27
0.19	D.DT	0.2	14.	D.DT	DT	1.452	27
0.20	D.DT	0.2	15.	D.DT	DT	1.452	27
0.21	D.DT	0.2	16.	D.DT	DT	1.452	27
0.22	D.DT	0.2	17.	D.DT	DT	1.452	27
0.23	D.DT	0.2	18.	D.DT	DT	1.452	27
0.24	D.DT	0.2	19.	D.DT	DT	1.452	27
0.25	D.DT	0.2	20.	D.DT	DT	1.452	27
0.26	D.DT	0.2	21.	D.DT	DT	1.452	27
0.27	D.DT	0.2	22.	D.DT	DT	1.452	27
0.28	D.DT	0.2	23.	D.DT	DT	1.452	27
0.29	D.DT	0.2	24.	D.DT	DT	1.452	27
0.30	D.DT	0.2	25.	D.DT	DT	1.452	27
0.31	D.DT	0.2	26.	D.DT	DT	1.452	27
0.32	D.DT	0.2	27.	D.DT	DT	1.452	27
0.33	D.DT	0.2	28.	D.DT	DT	1.452	27
0.34	D.DT	0.2	29.	D.DT	DT	1.452	27
0.35	D.DT	0.2	30.	D.DT	DT	1.452	27
0.36	D.DT	0.2	31.	D.DT	DT	1.452	27
0.37	D.DT	0.2	32.	D.DT	DT	1.452	27
0.38	D.DT	0.2	33.	D.DT	DT	1.452	27
0.39	D.DT	0.2	34.	D.DT	DT	1.452	27
0.40	D.DT	0.2	35.	D.DT	DT	1.452	27
0.41	D.DT	0.2	36.	D.DT	DT	1.452	27
0.42	D.DT	0.2	37.	D.DT	DT	1.452	27
0.43	D.DT	0.2	38.	D.DT	DT	1.452	27
0.44	D.DT	0.2	39.	D.DT	DT	1.452	27
0.45	D.DT	0.2	40.	D.DT	DT	1.452	27
0.46	D.DT	0.2	41.	D.DT	DT	1.452	27
0.47	D.DT	0.2	42.	D.DT	DT	1.452	27
0.48	D.DT	0.2	43.	D.DT	DT	1.452	27
0.49	D.DT	0.2	44.	D.DT	DT	1.452	27
0.50	D.DT	0.2	45.	D.DT	DT	1.452	27
0.51	D.DT	0.2	46.	D.DT	DT	1.452	27
0.52	D.DT	0.2	47.	D.DT	DT	1.452	27
0.53	D.DT	0.2	48.	D.DT	DT	1.452	27
0.54	D.DT	0.2	49.	D.DT	DT	1.452	27
0.55	D.DT	0.2	50.	D.DT	DT	1.452	27
0.56	D.DT	0.2	51.	D.DT	DT	1.452	27
0.57	D.DT	0.2	52.	D.DT	DT	1.452	27
0.58	D.DT	0.2	53.	D.DT	DT	1.452	27
0.59	D.DT	0.2	54.	D.DT	DT	1.452	27
0.60	D.DT	0.2	55.	D.DT	DT	1.452	27
0.61	D.DT	0.2	56.	D.DT	DT	1.452	27
0.62	D.DT	0.2	57.	D.DT	DT	1.452	27
0.63	D.DT	0.2	58.	D.DT	DT	1.452	27
0.64	D.DT	0.2	59.	D.DT	DT	1.452	27
0.65	D.DT	0.2	60.	D.DT	DT	1.452	27
0.66	D.DT	0.2	61.	D.DT	DT	1.452	27
0.67	D.DT	0.2	62.	D.DT	DT	1.452	27
0.68	D.DT	0.2	63.	D.DT	DT	1.452	27
0.69	D.DT	0.2	64.	D.DT	DT	1.452	27
0.70	D.DT	0.2	65.	D.DT	DT	1.452	27
0.71	D.DT	0.2	66.	D.DT	DT	1.452	27
0.72	D.DT	0.2	67.	D.DT	DT	1.452	27
0.73	D.DT	0.2	68.	D.DT	DT	1.452	27
0.74	D.DT	0.2	69.	D.DT	DT	1.452	27
0.75	D.DT	0.2	70.	D.DT	DT	1.452	27
0.76	D.DT	0.2	71.	D.DT	DT	1.452	27
0.77	D.DT	0.2	72.	D.DT	DT	1.452	27
0.78	D.DT	0.2	73.	D.DT	DT	1.452	27
0.79	D.DT	0.2	74.	D.DT	DT	1.452	27
0.80	D.DT	0.2	75.	D.DT	DT	1.452	27
0.81	D.DT	0.2	76.	D.DT	DT	1.452	27
0.82	D.DT	0.2	77.	D.DT	DT	1.452	27
0.83	D.DT	0.2	78.	D.DT	DT	1.452	27
0.84	D.DT	0.2	79.	D.DT	DT	1.452	27
0.85	D.DT	0.2	80.	D.DT	DT	1.452	27
0.86	D.DT	0.2	81.	D.DT	DT	1.452	27
0.87	D.DT	0.2	82.	D.DT	DT	1.452	27
0.88	D.DT	0.2	83.	D.DT	DT	1.452	27
0.89	D.DT	0.2	84.	D.DT	DT	1.452	27
0.90	D.DT	0.2	85.	D.DT	DT	1.452	27
0.91	D.DT	0.2	86.	D.DT	DT	1.452	27
0.92	D.DT	0.2	87.	D.DT	DT	1.452	27
0.93	D.DT	0.2	88.	D.DT	DT	1.452	27
0.94	D.DT	0.2	89.	D.DT	DT	1.452	27
0.95	D.DT	0.2	90.	D.DT	DT	1.452	27
0.96	D.DT	0.2	91.	D.DT	DT	1.452	27
0.97	D.DT	0.2	92.	D.DT	DT	1.452	27
0.98	D.DT	0.2	93.	D.DT	DT	1.452	27
0.99	D.DT	0.2	94.	D.DT	DT	1.452	27
1.00	D.DT	0.2	95.	D.DT	DT	1.452	27

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TOTAL

בְּרִיתֵינוּ וְעָמֹדֶנוּ

SYNTHETIC POLY(1,4-PHENYLICOLIC ACID)

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אפריל ינואר 1950 סטטיסטיקה של SHELL LTD 55.0%

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THE JOURNAL OF CLIMATE

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THE DEGREES OF CONFIDENCE IN THEORIES

THE CALLER
WAS A FRIENDLY OLD MAN.

THE SMALLER THE NUMBER, THE GREATER THE VALUE WHICH WILL

IS IT POSSIBLE TO ACTUALLY ACCUMULATE

卷之三

THE SCLAF EXTRAPOLATE ADJUSTABLE THE SCLAF

THERMALLY STABILIZED POLY(URIDYLIC ACID) ANALOGUE 11

THE MUSEUM OF THE STATE OF MASSACHUSETTS

REVIEWS DURING THE 20TH CENTURY

THE JOURNAL OF CLIMATE VOLUME 17, NUMBER 11, NOVEMBER 2004

卷之三

TABLE 59

THE JOURNAL OF CLIMATE

ELECTION NO. 2015: —
ADM: PINTO, RONALD - AN MAX
ADM: MUNICIPALITY OF EASTMAN - IN THE CAPITAL CITY.

卷之三

RECORDED IN THE NAME OF THE SOCIETY FOR THE
ADVANCEMENT OF SCIENCE, NAMELY THAT FOR THE
SPECIFIC MISSION JOURNAL WHICH IS CALLED
THE "SCIENTIFIC AND INDUSTRIAL JOURNAL OF
THE SOCIETY FOR THE ADVANCEMENT OF SCIENCE."
THE SOCIETY FOR THE ADVANCEMENT OF SCIENCE,
LONDON, APRIL 1, 1851.

Digitized by srujanika@gmail.com

卷之三

Tag 60

DIMENSION "H" AT GHI ENVIRONMENT: NXLX1:S-MAX 600THR 1667KM FOR SOL MAX

FIGURE 1

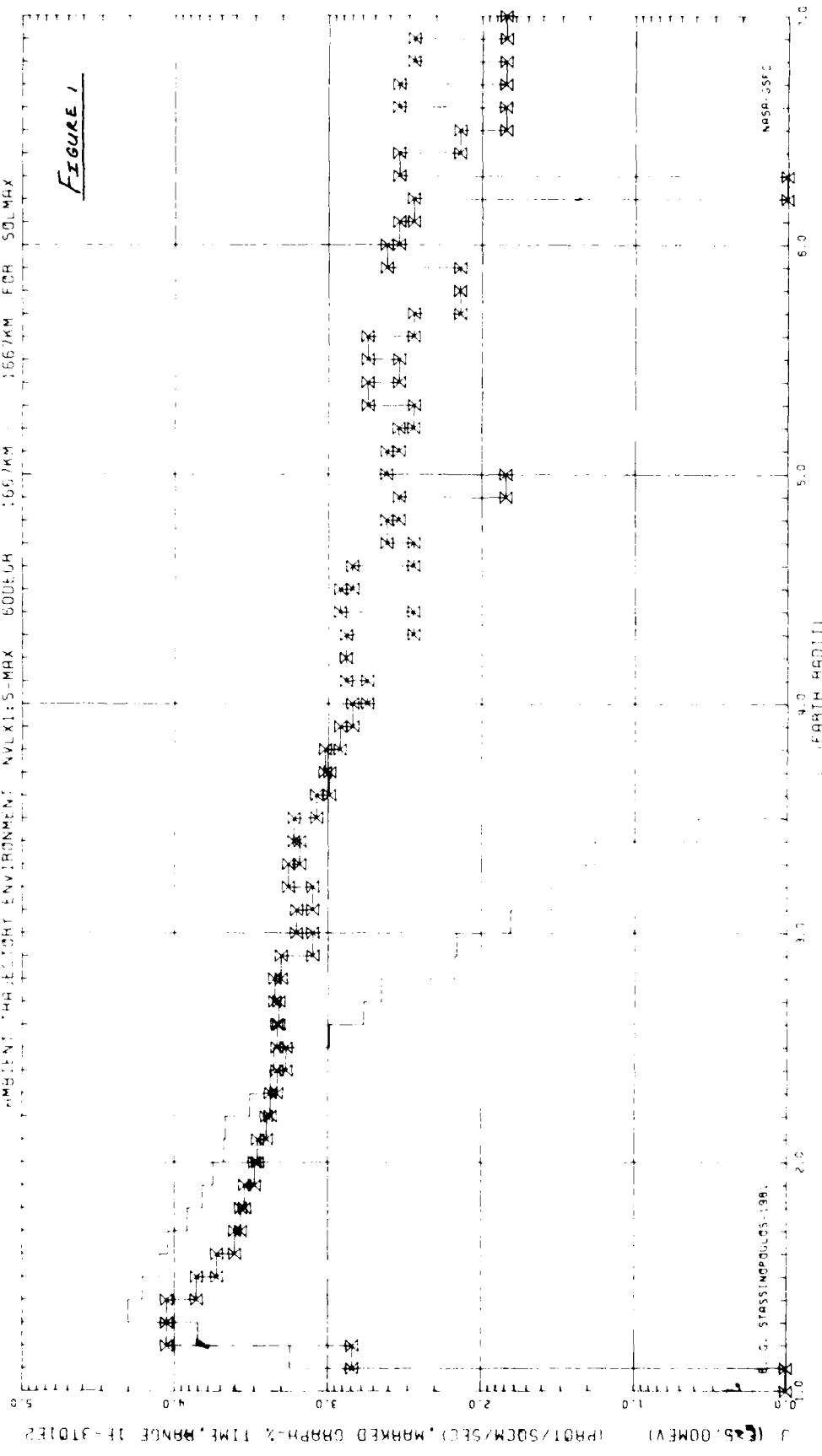
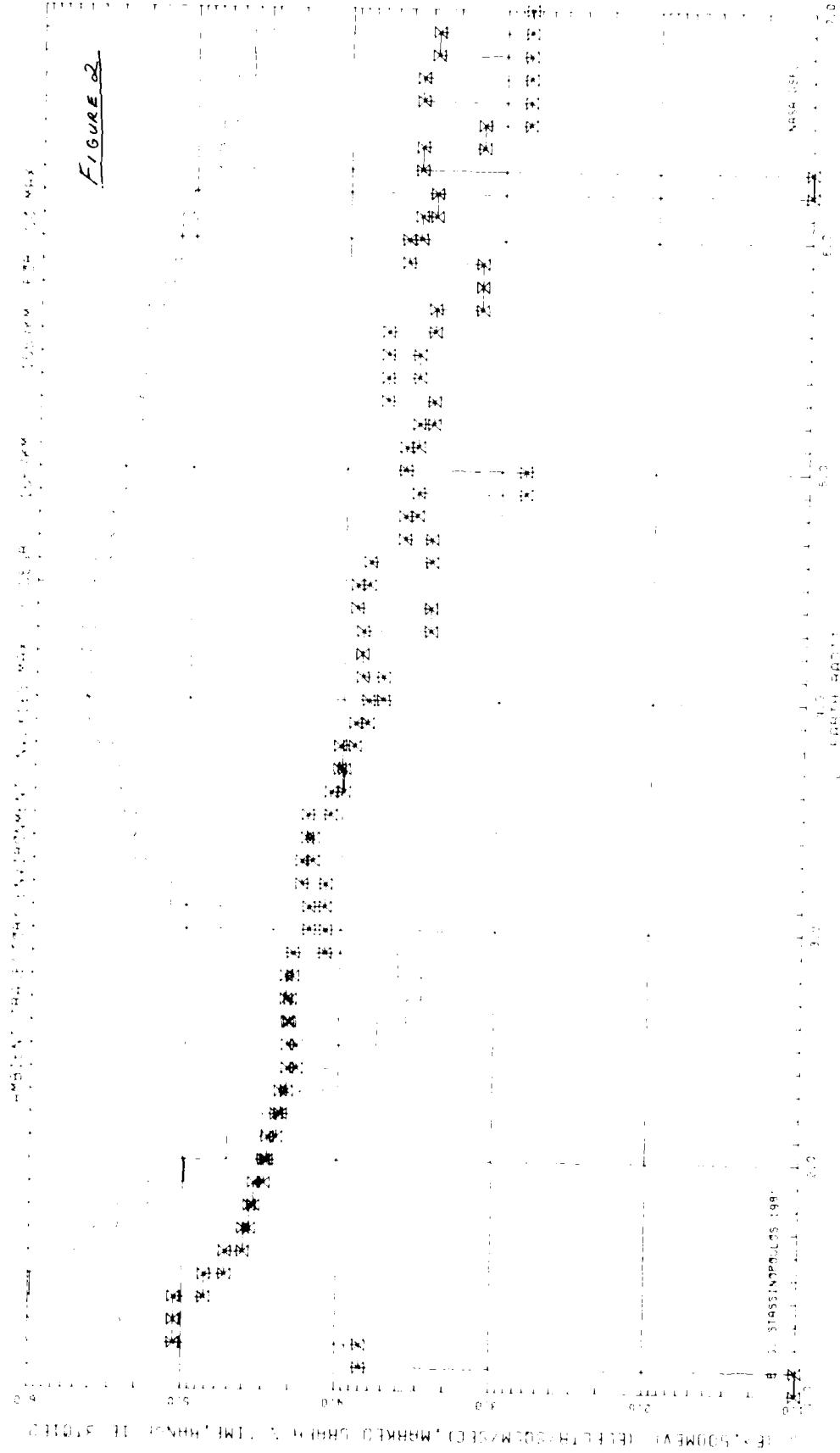
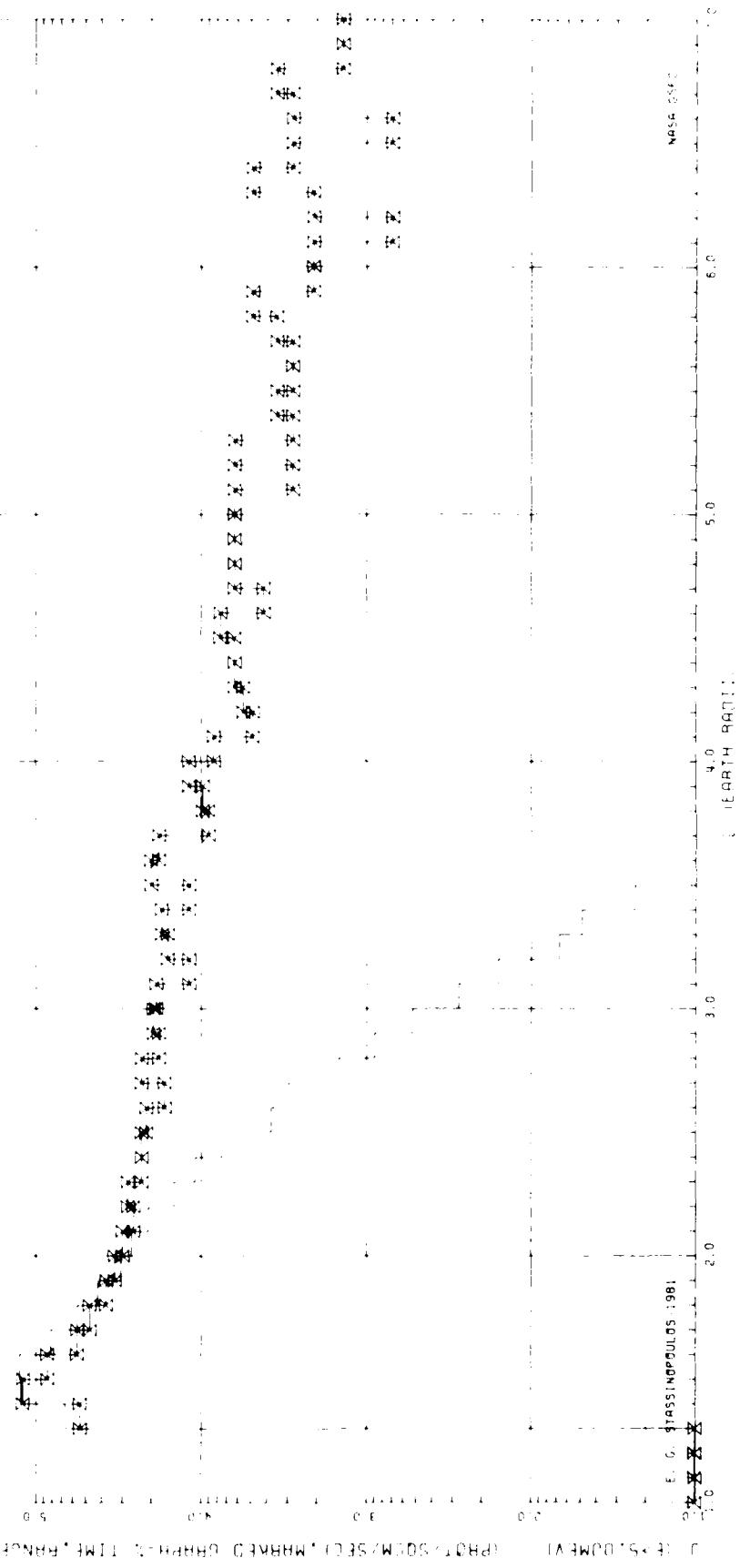


FIGURE 2



COMBINING HIGH-LEVEL ENVIRONMENTAL KNOWLEDGE FROM CATEGORICAL DATA WITH QUANTITATIVE DATA

FIGURE 3



CHINESE NAME: CHENG YUAN HUA
ENGLISH NAME: CHENG YUAN HUA
BORN: 1910
DECEASED: 1985
AGE: 75

FIGURE 4

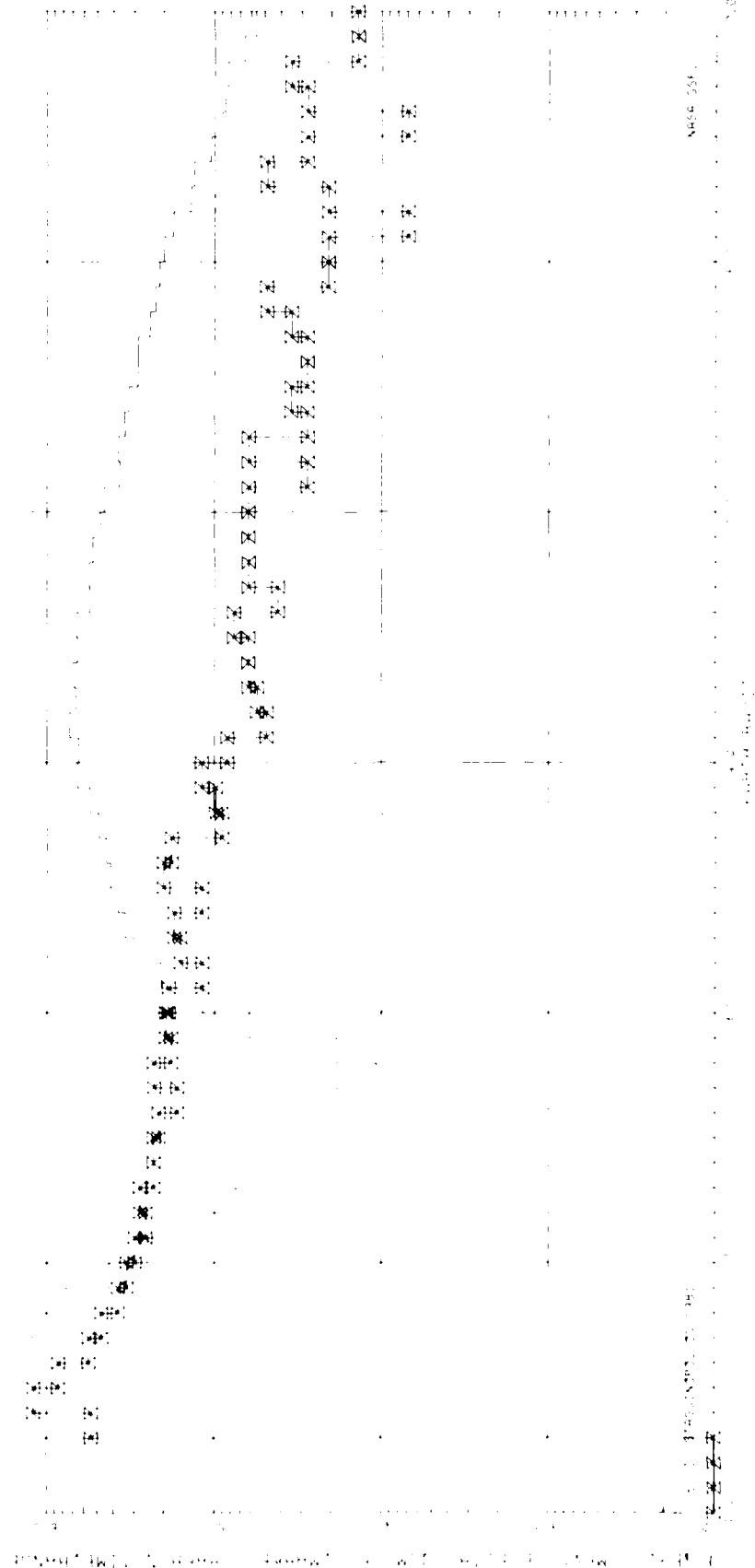
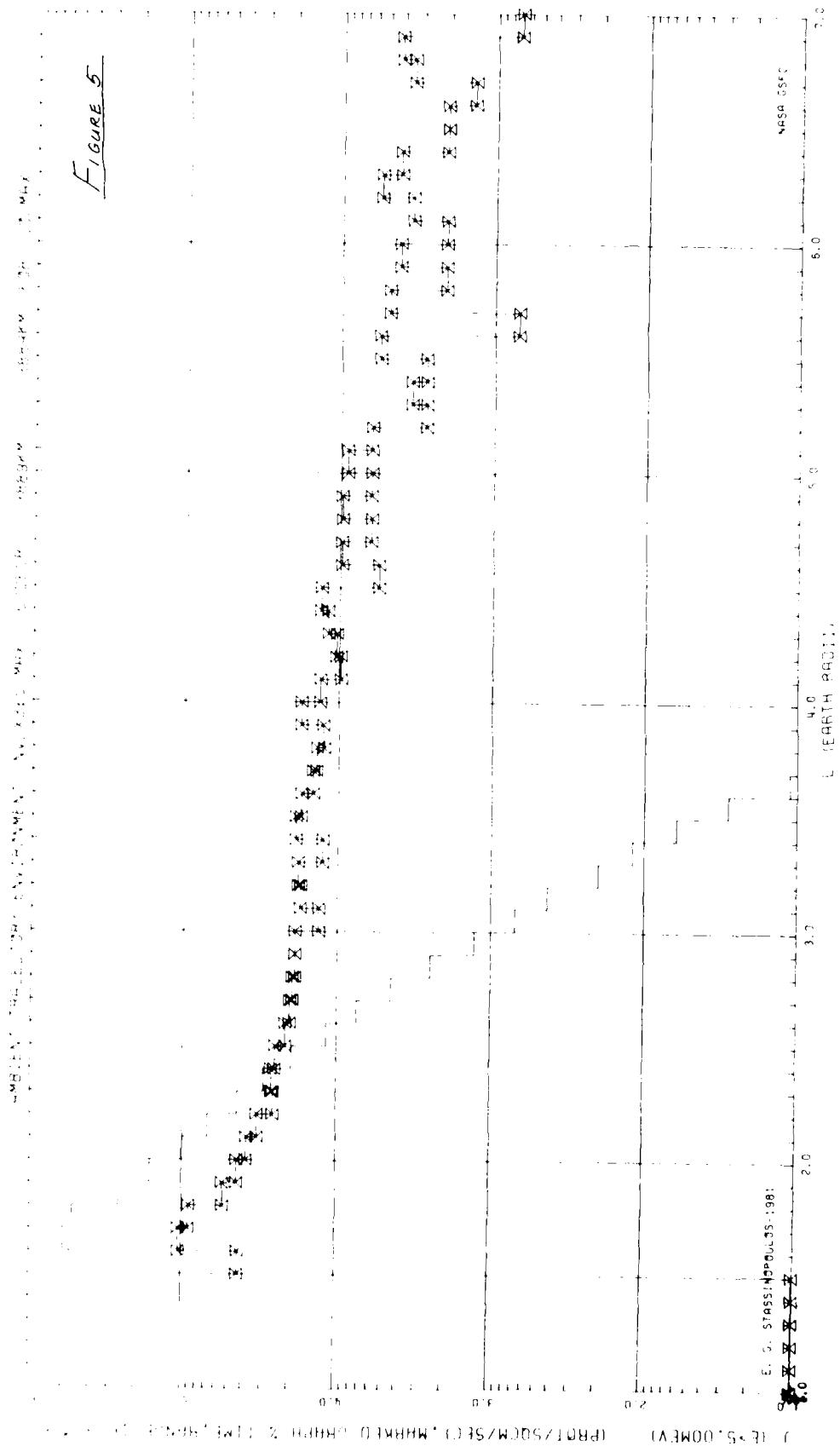
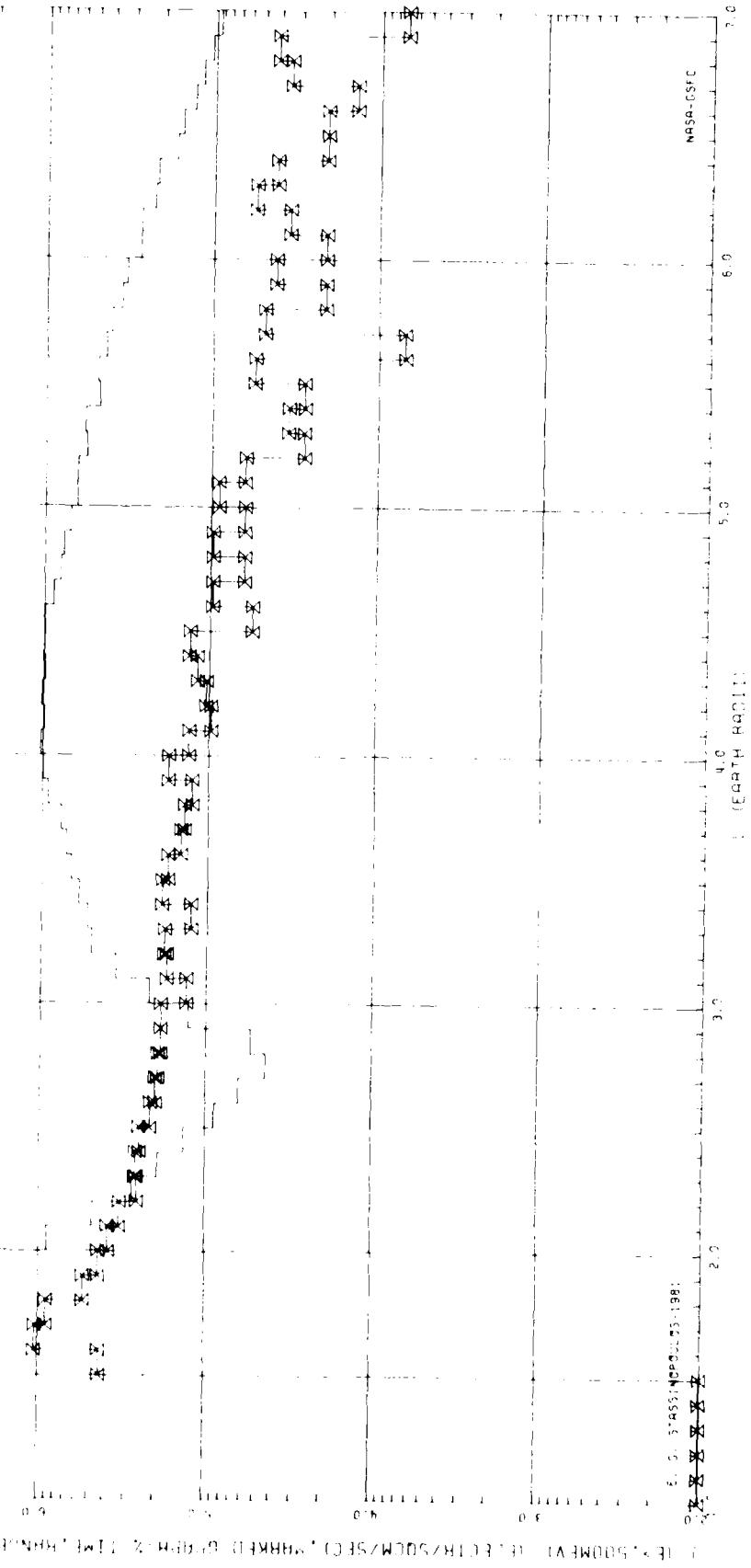


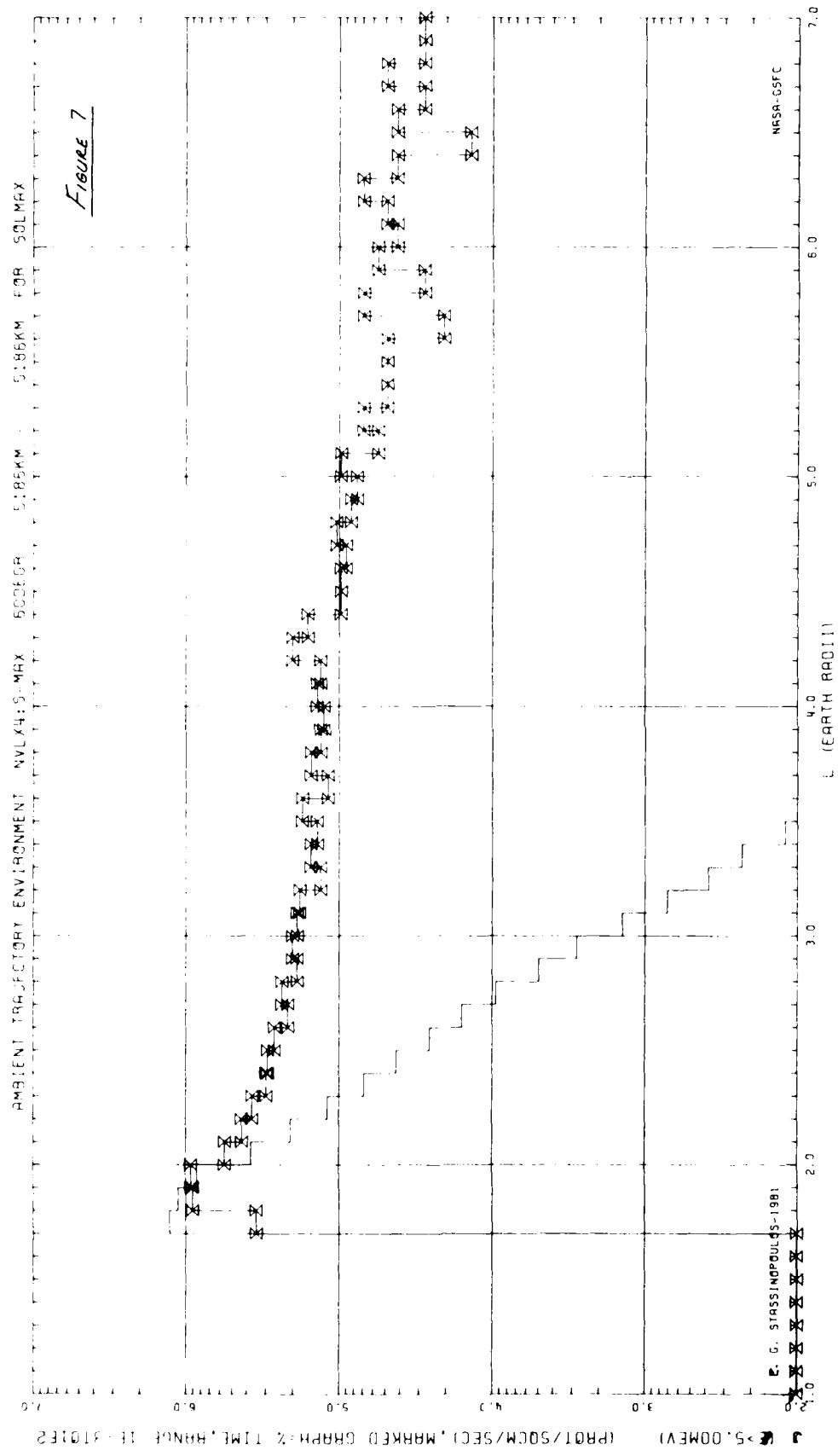
FIGURE 5



AMBIENT ATMOSPHERIC ENVIRONMENT - NV A315 MHz FREQUENCY SPECTRUM MEASUREMENTS

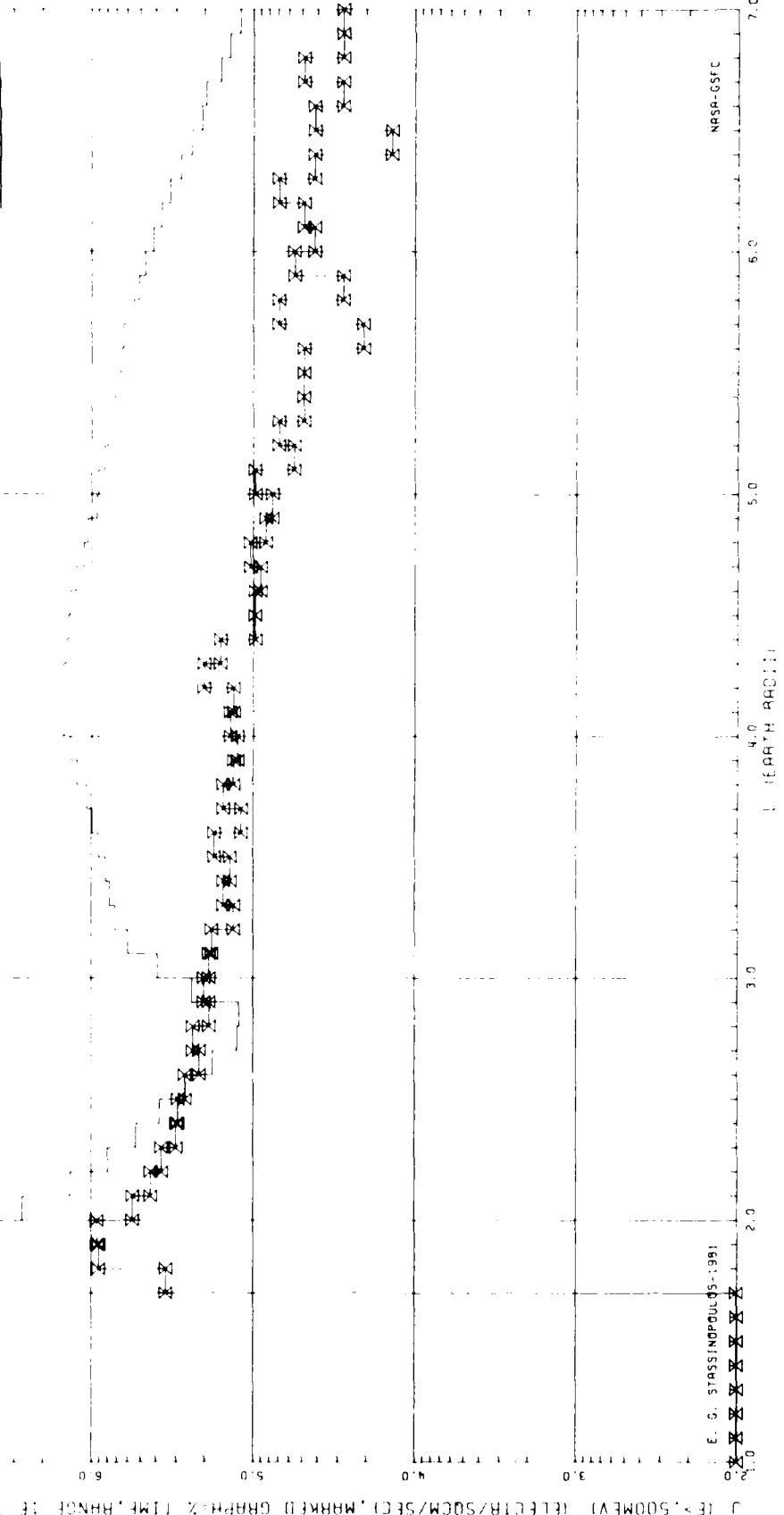
Figure 6





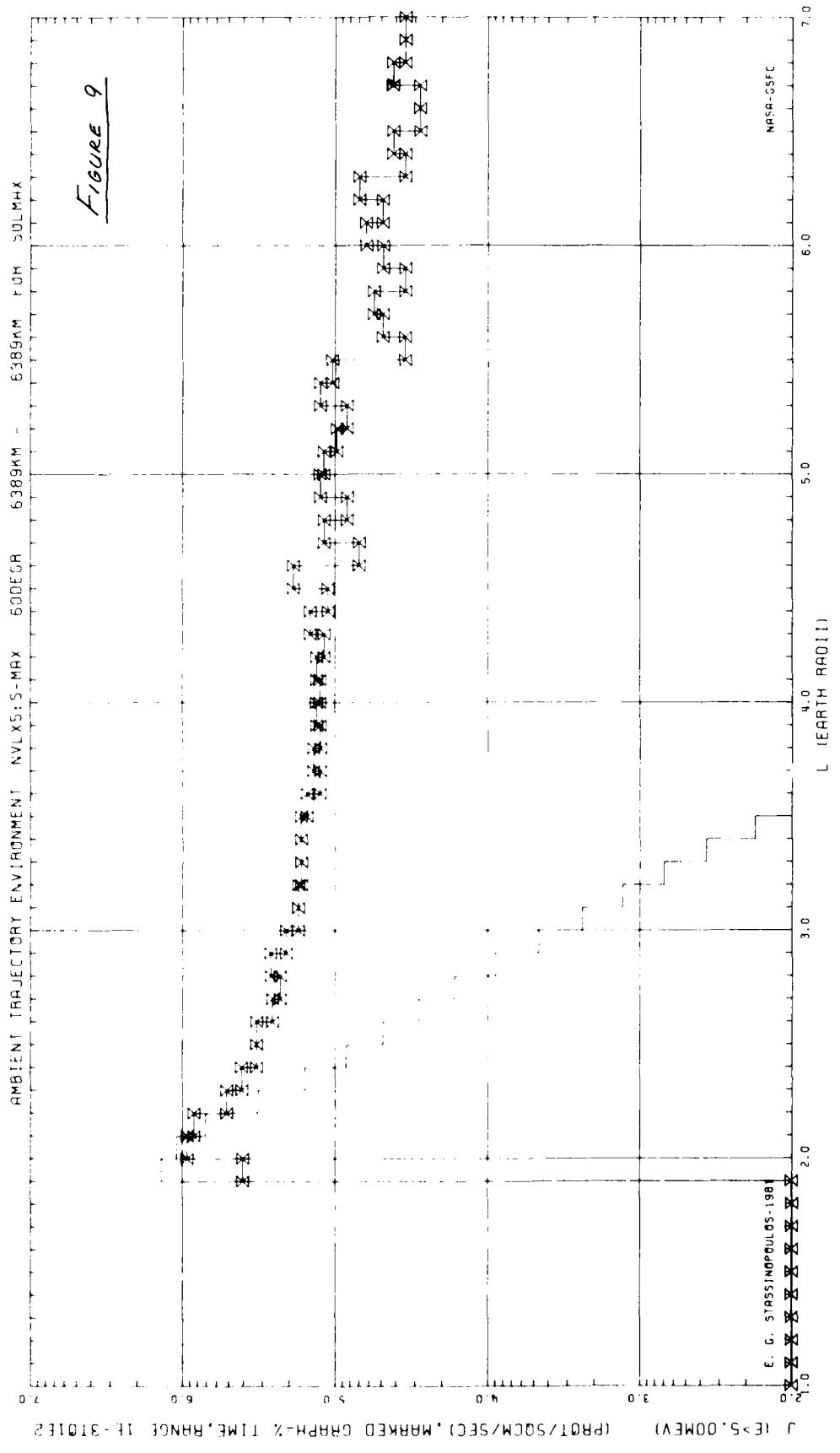
AMBIENT PHOTOCOXY ENVIRONMENT NO. X-5 MAX EARTH 5186KM FOR 100W

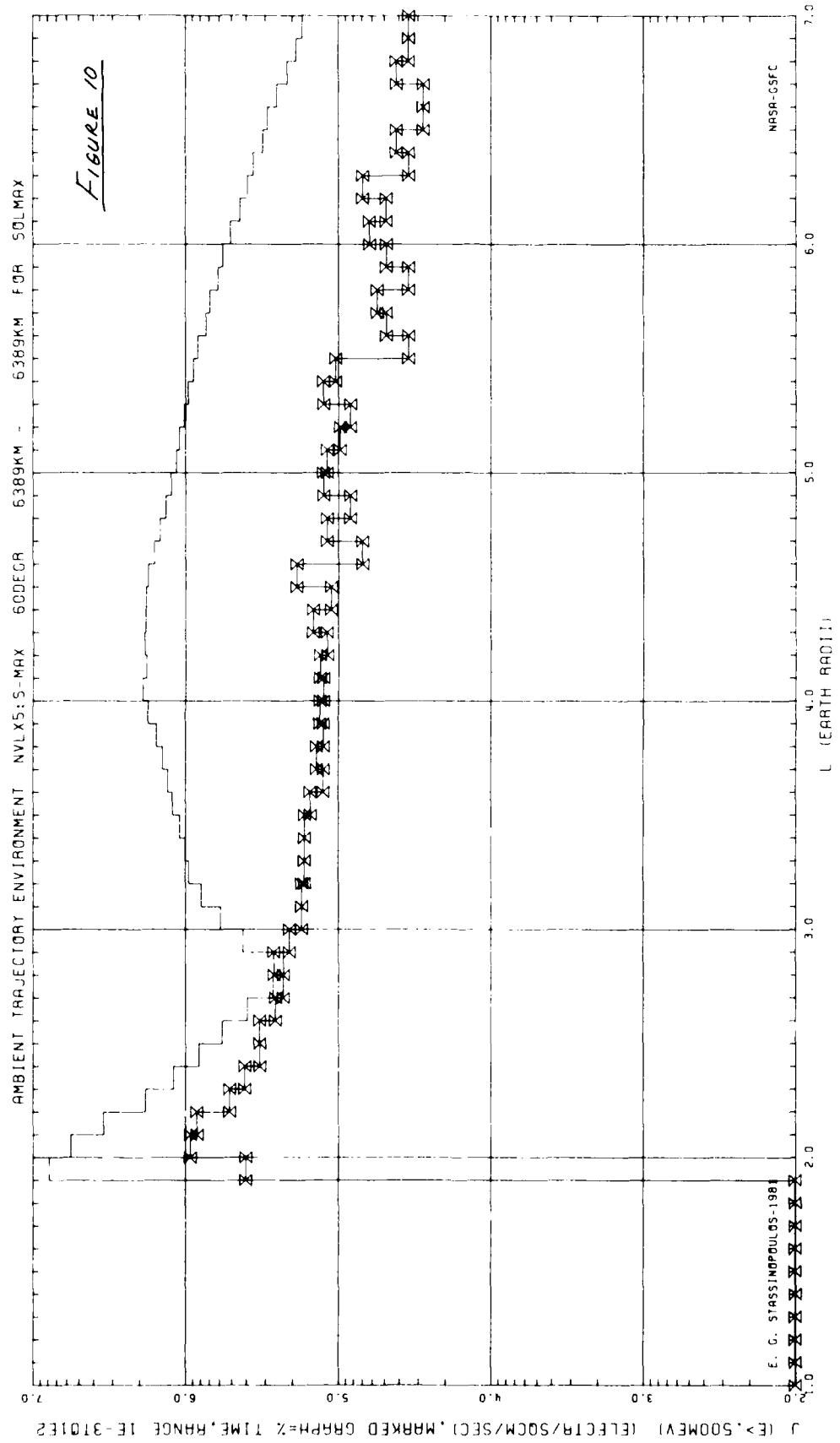
Figure 8

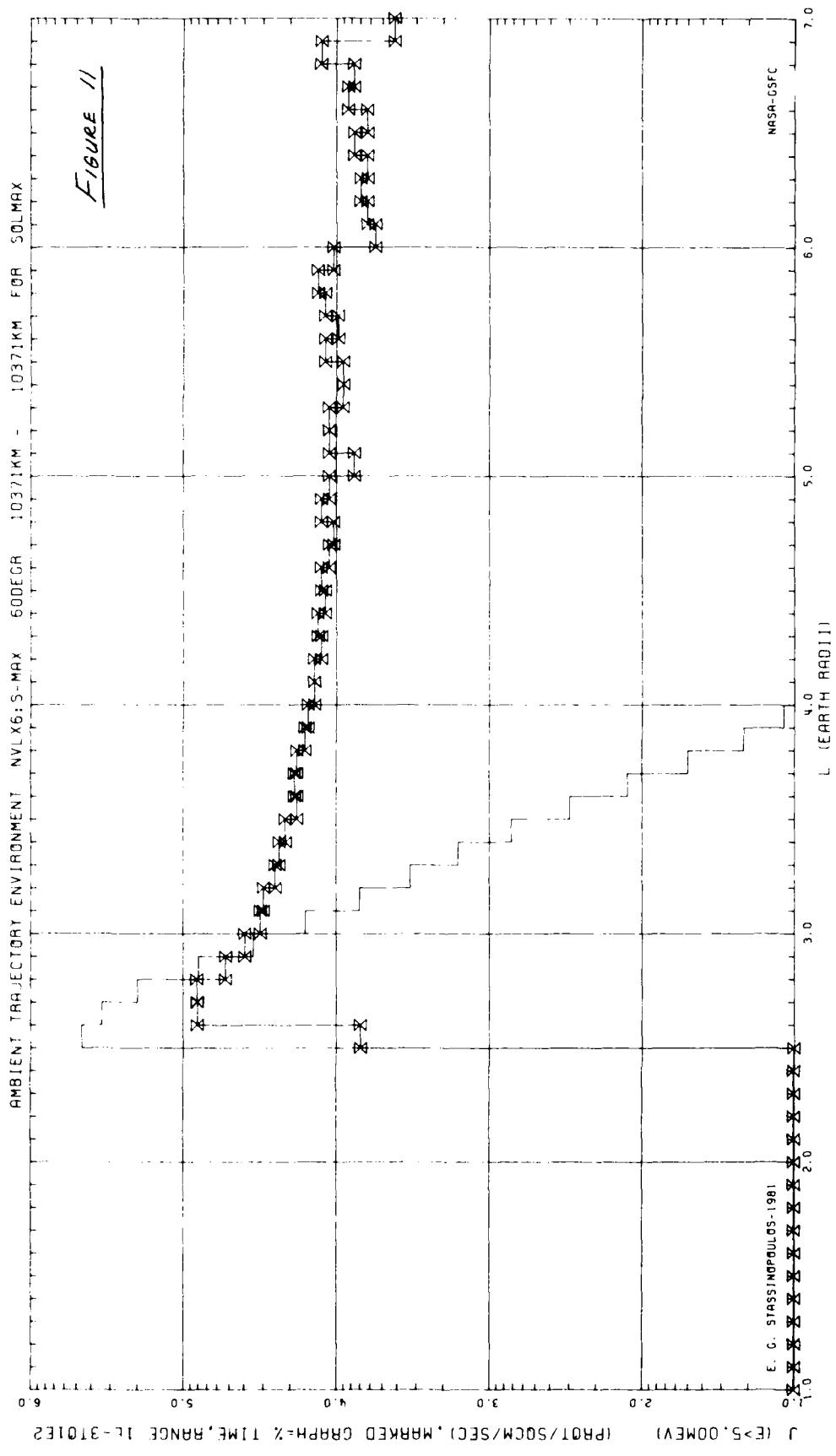


E. G. STASSINOPULOS - 1991

2

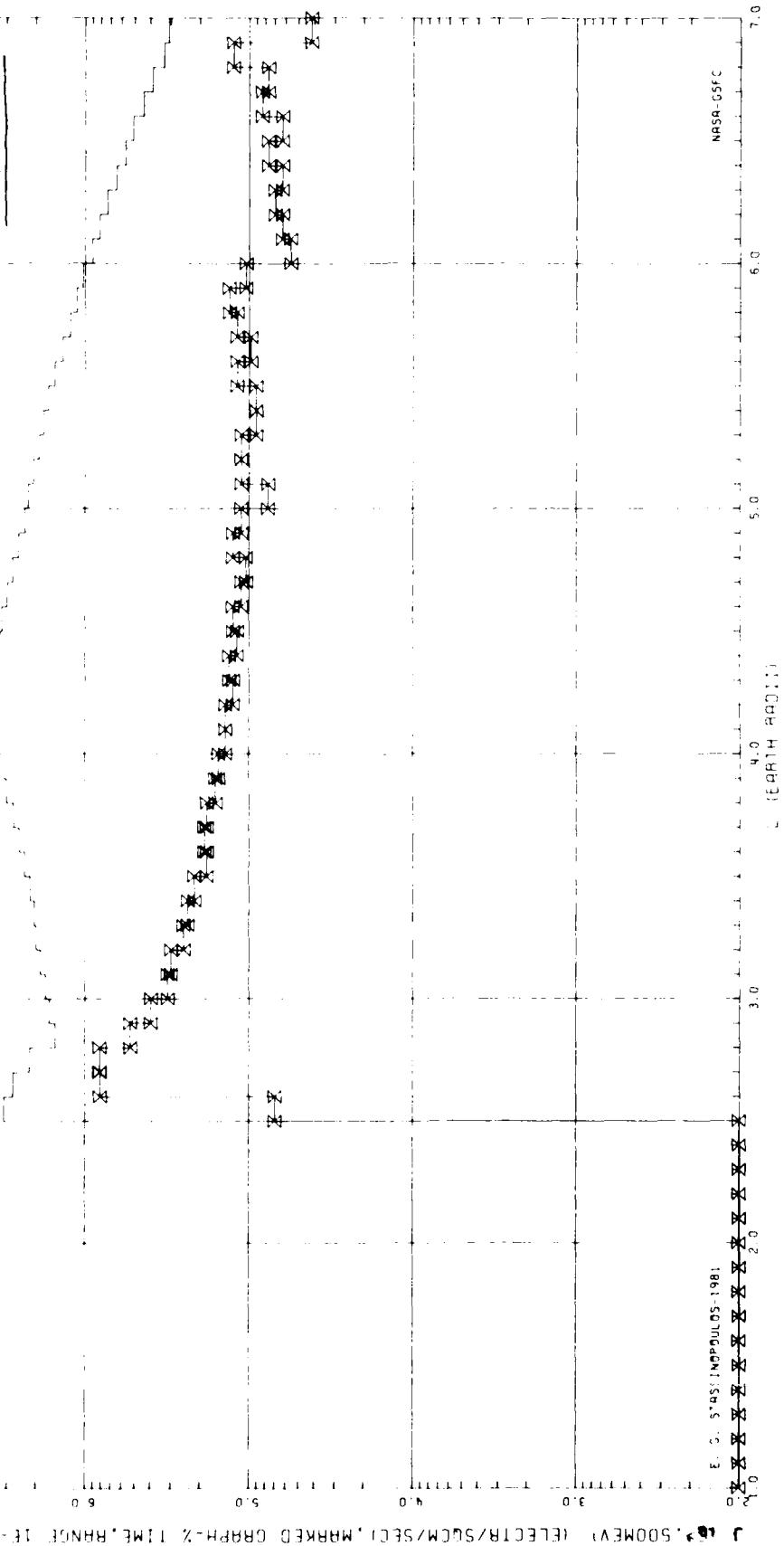


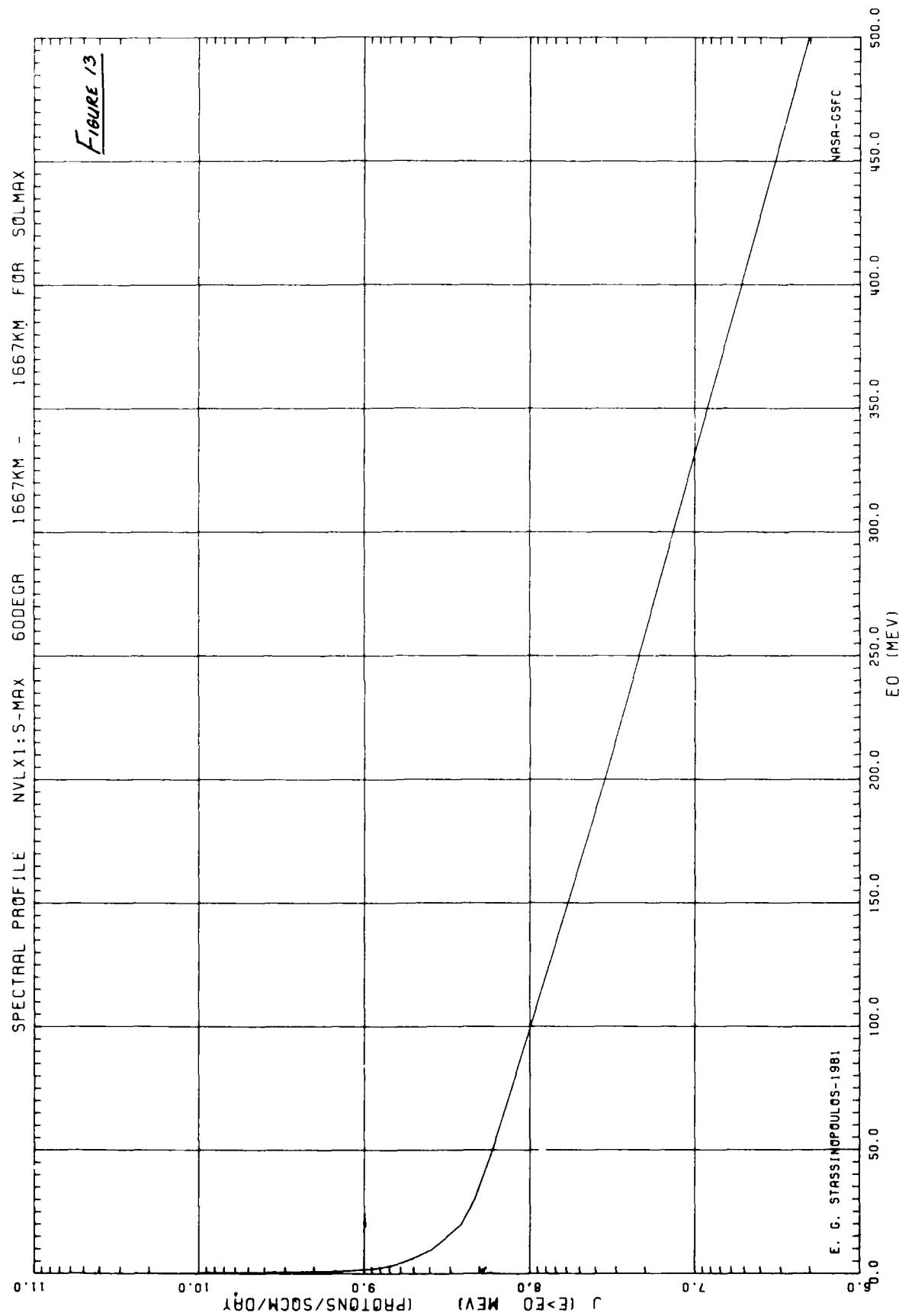


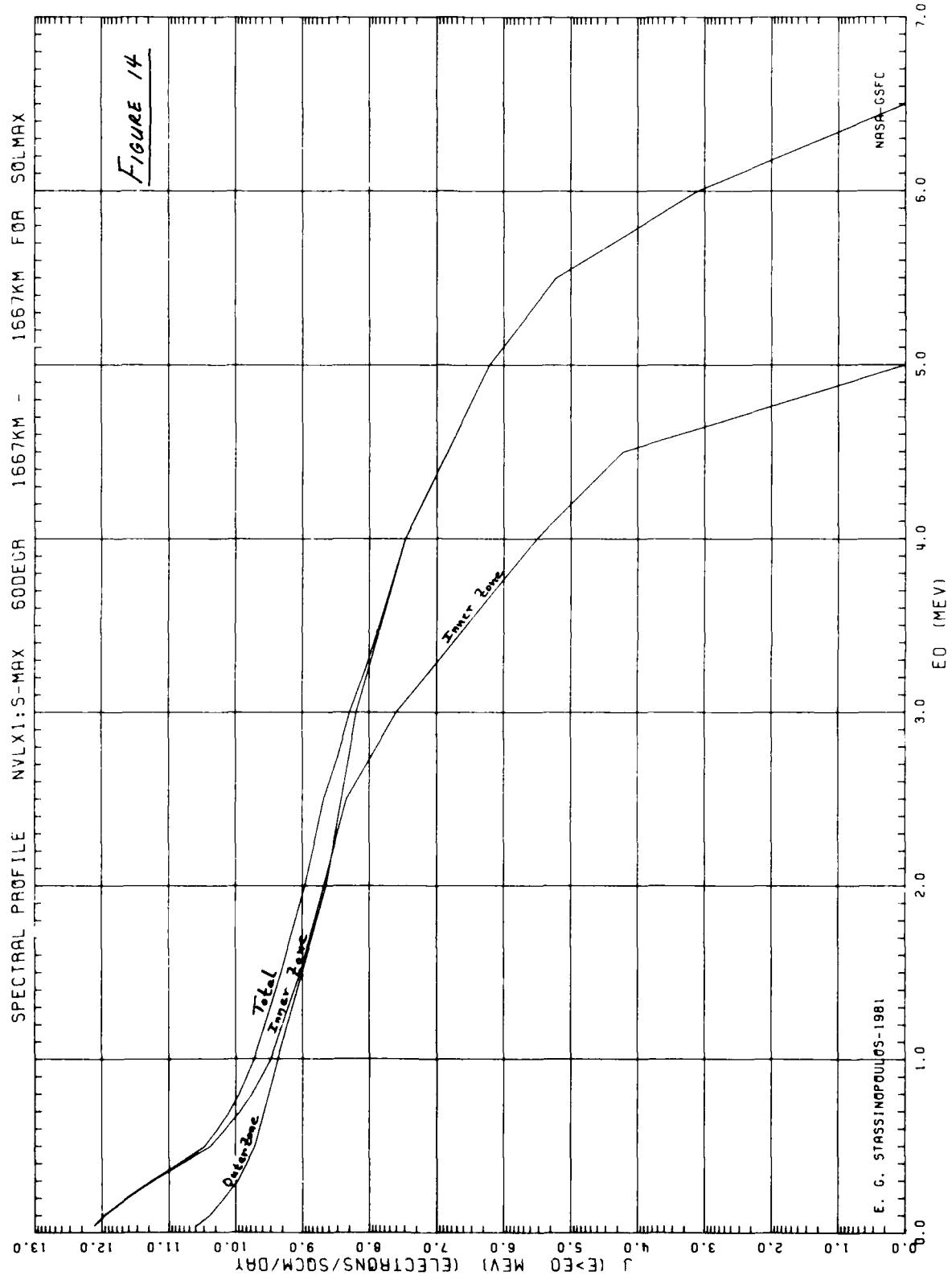


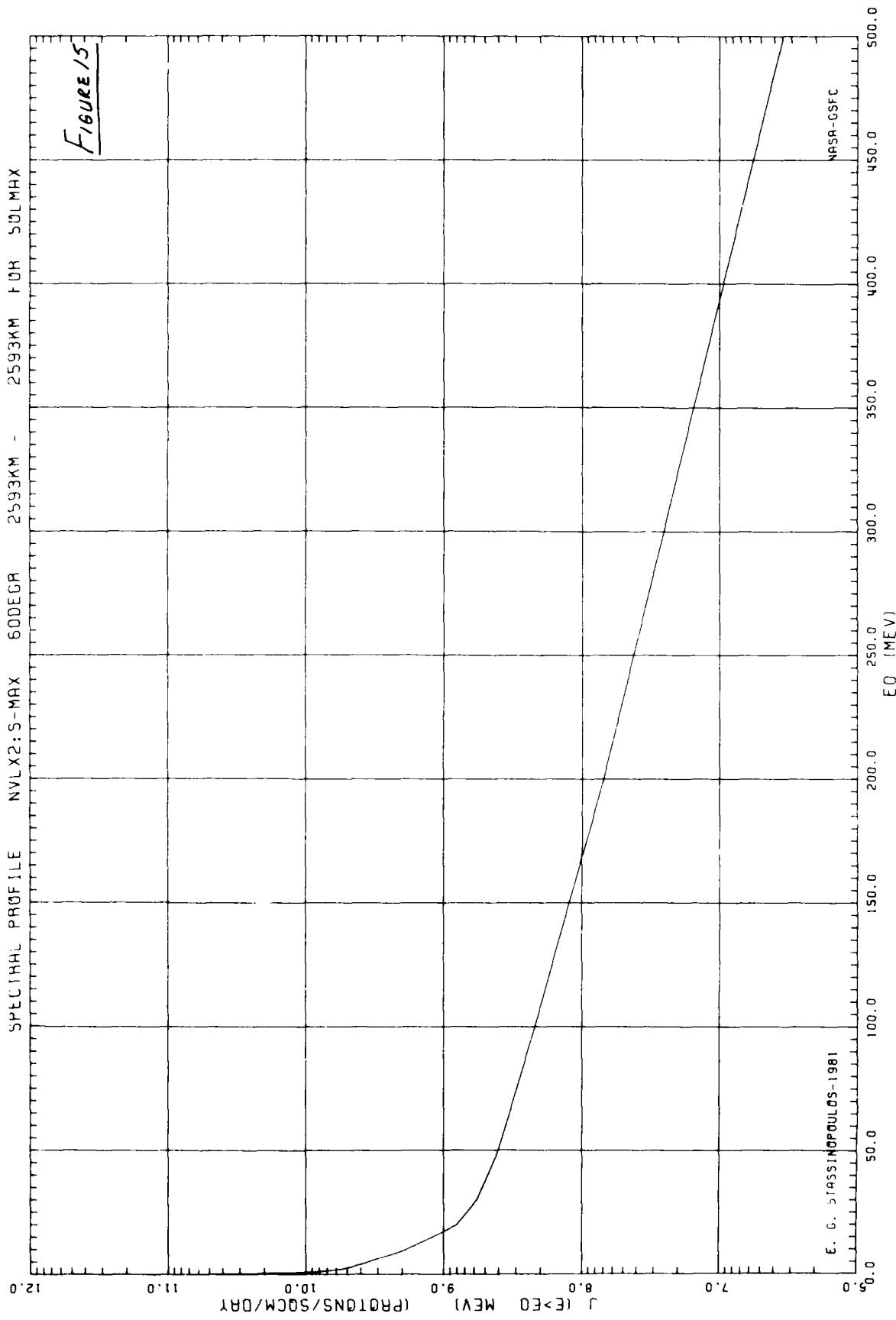
AMBIENT TRAJECTORY ENVIRONMENT LEVELS: 5-MAX 630EGR 1037NM = 1037KM FOR SOLAR MAX EFFECTIVE DENSITY (TEN TO THE MINUS EIGHTTH POWER) FOR VARIOUS DISTANCES

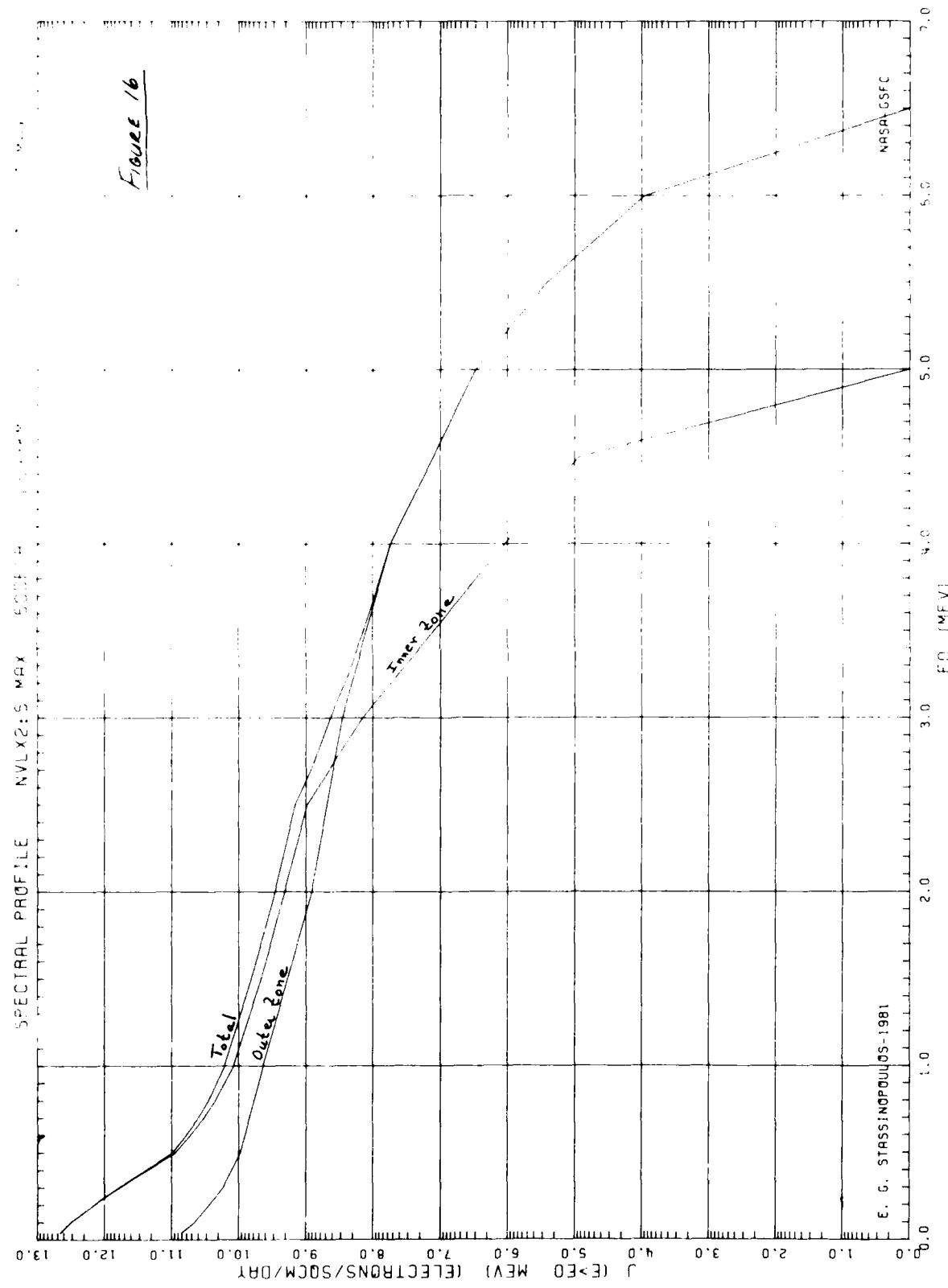
Figure 12

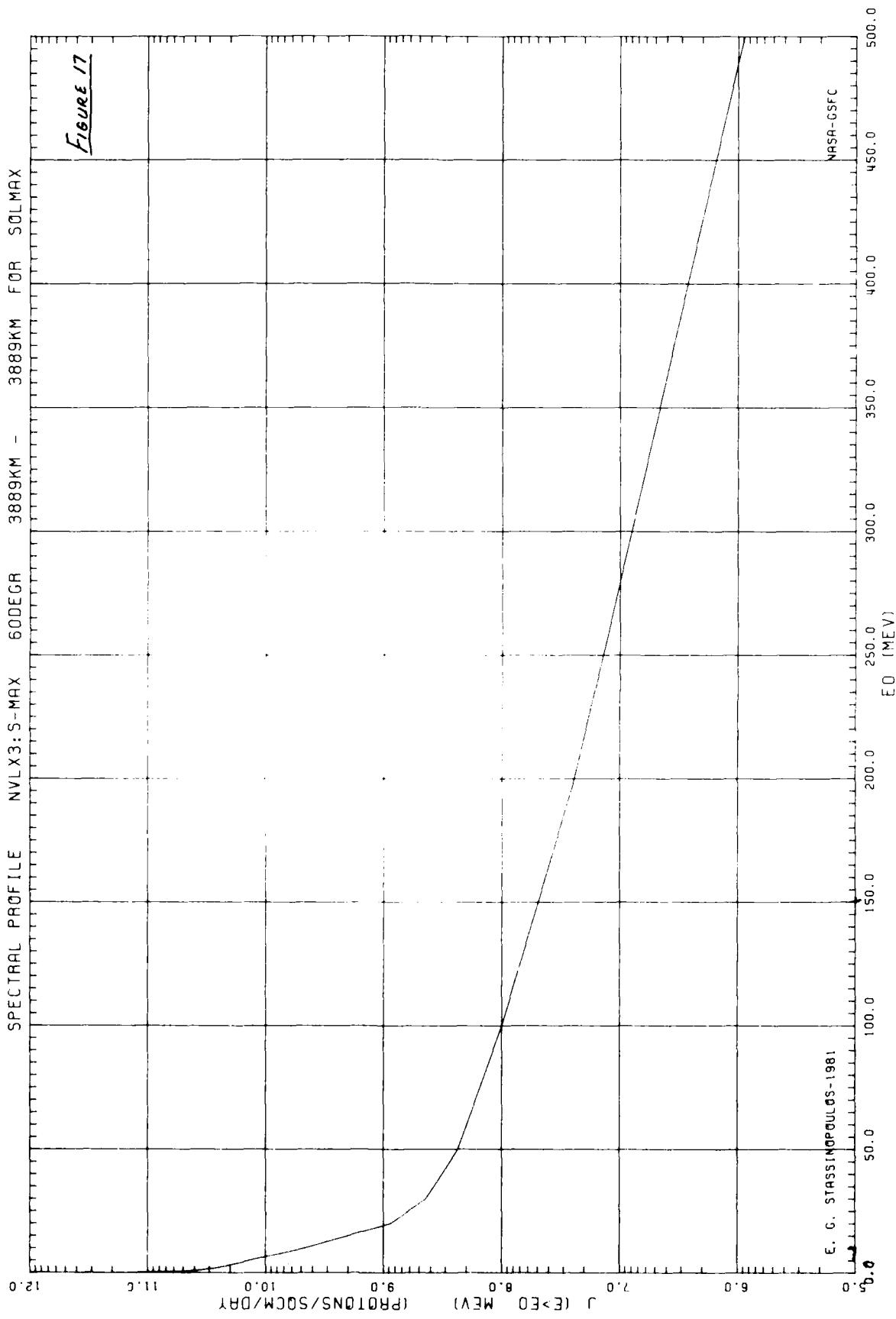


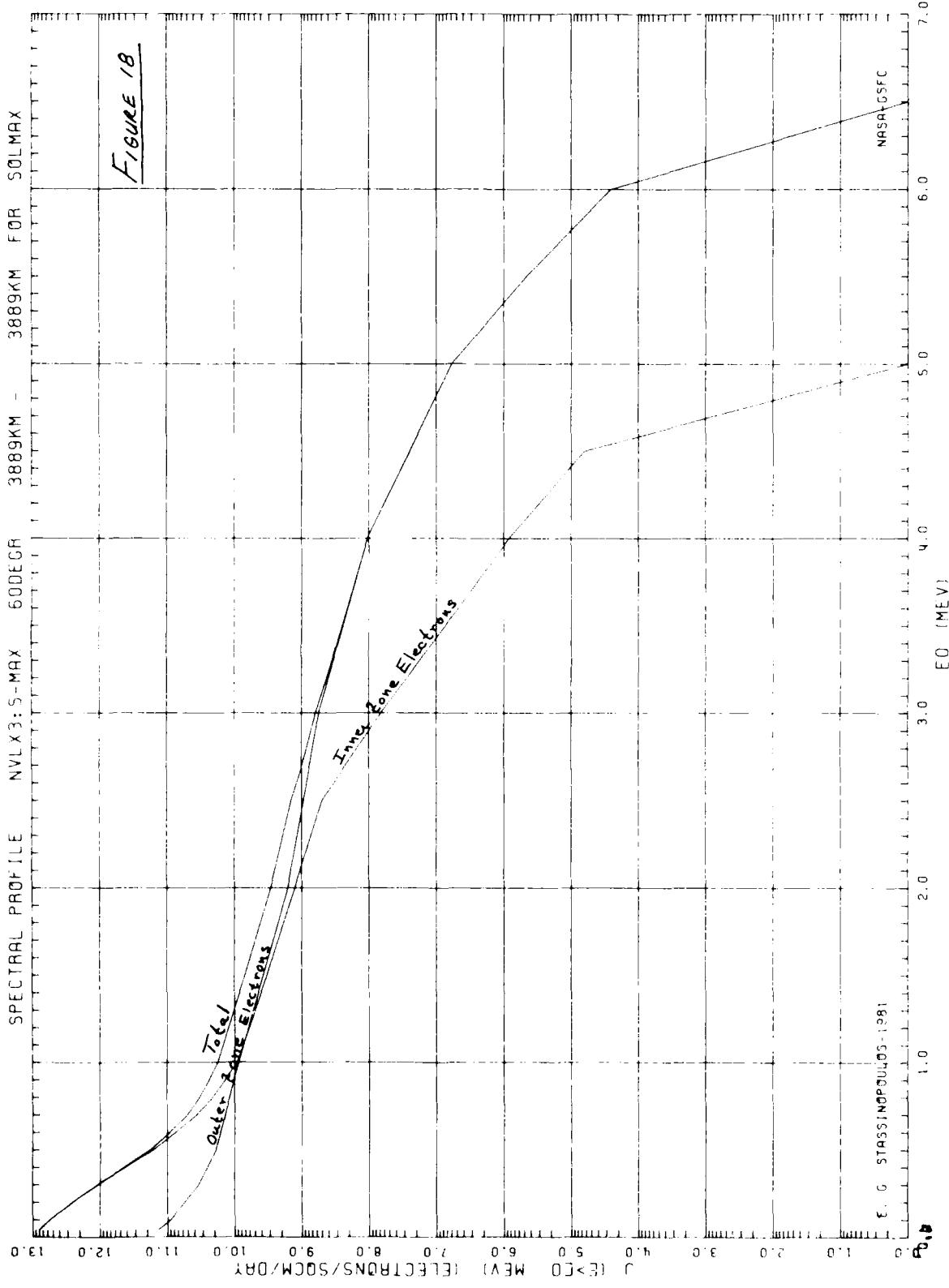










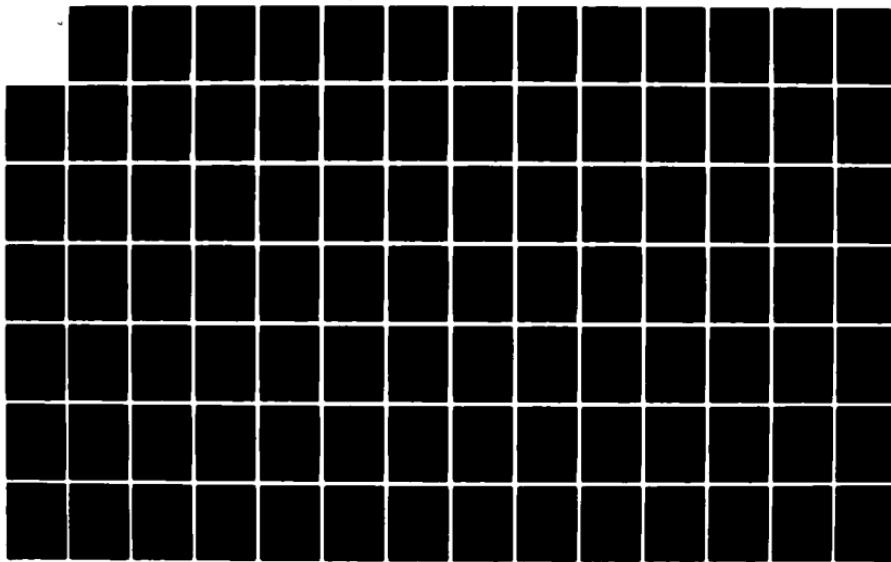


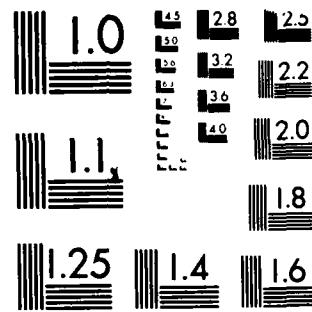
AD-A141 849 ORBITAL RADIATION STUDY FOR INCLINED CIRCULAR
TRAJECTORIES(U) NATIONAL AERONAUTICS AND SPACE
ADMINISTRATION GREENBELT MD GO.. E G STASSINOPoulos

UNCLASSIFIED NOV 81 NASA-GSFC-X-601-81-28

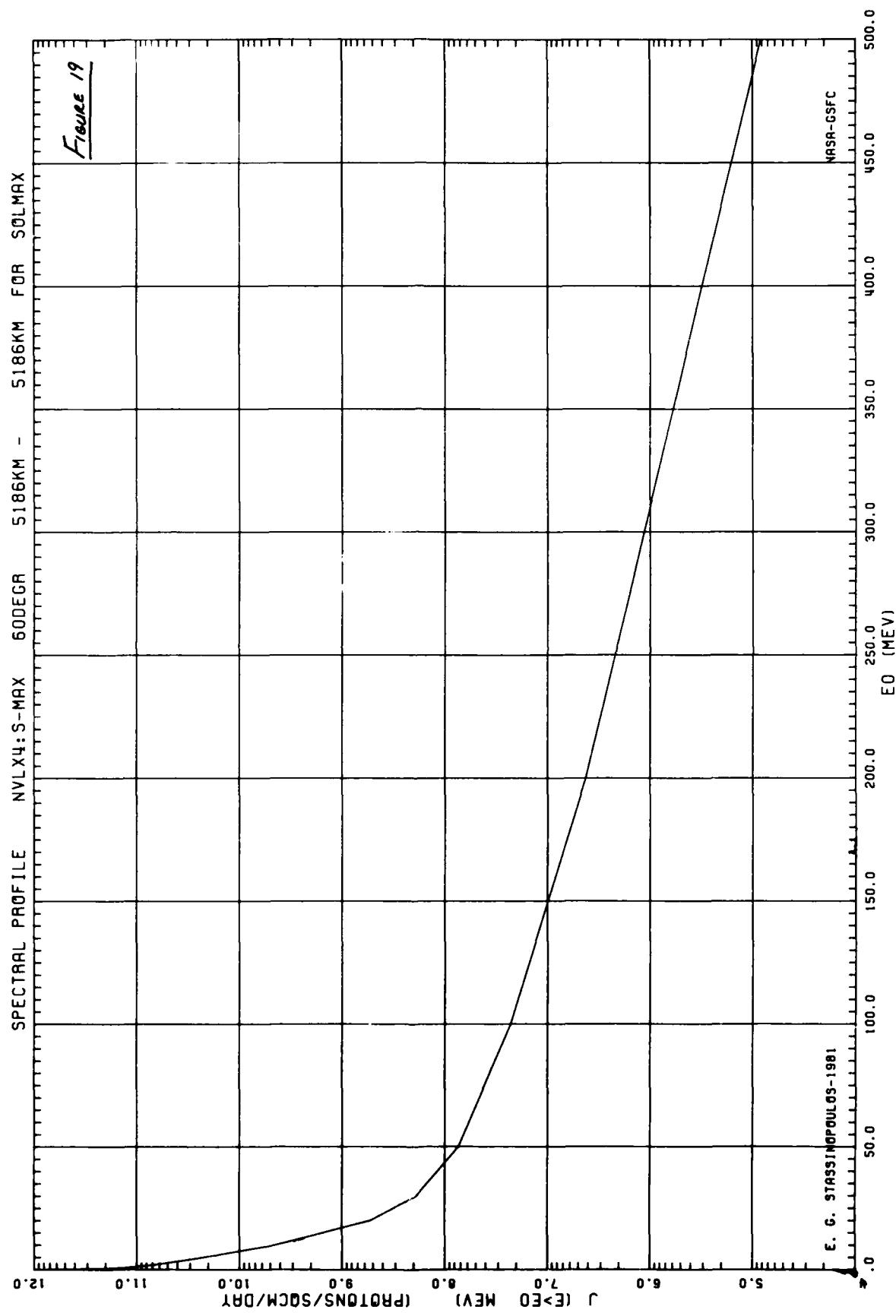
2/5
F/G 22/3

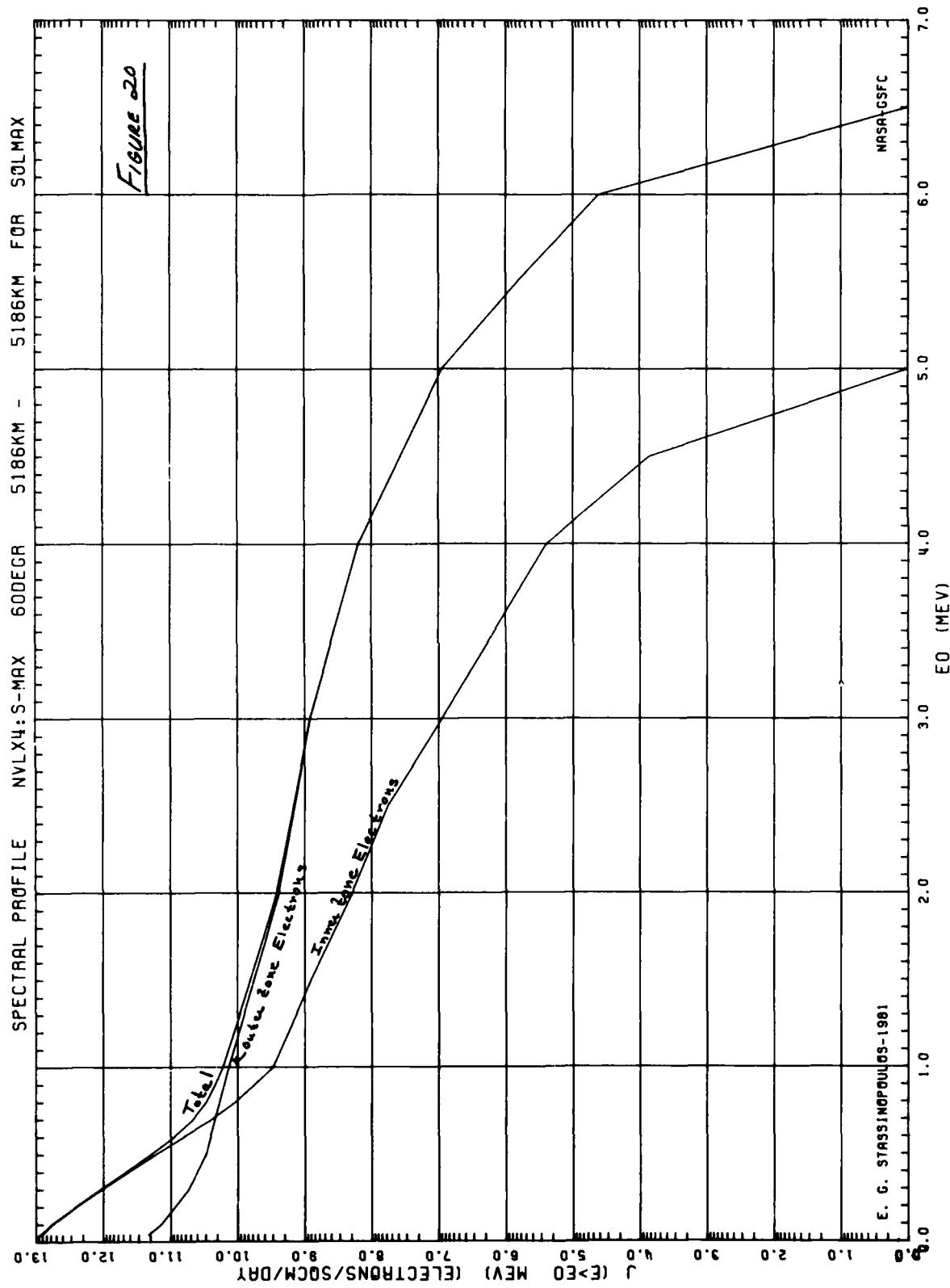
NL

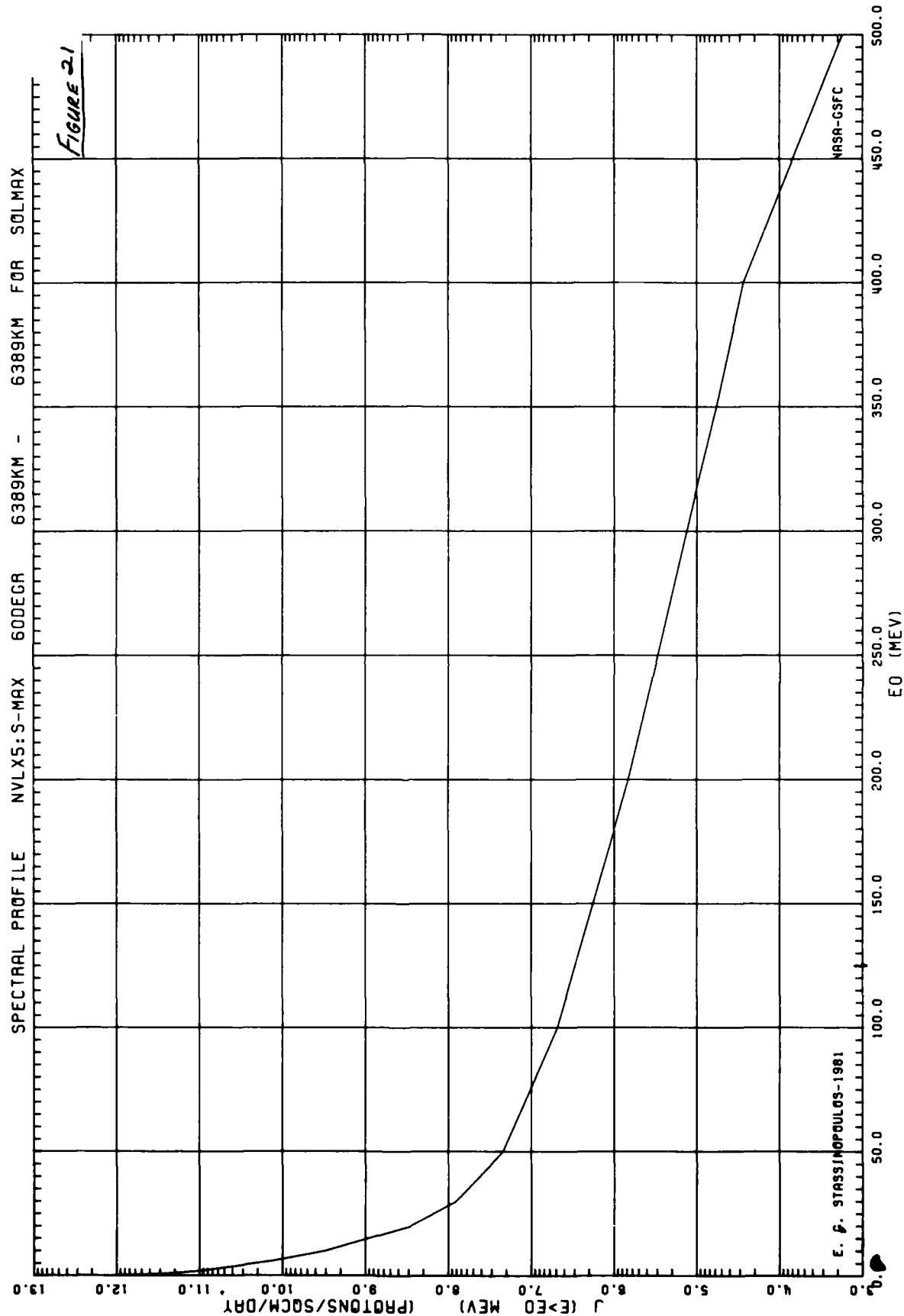


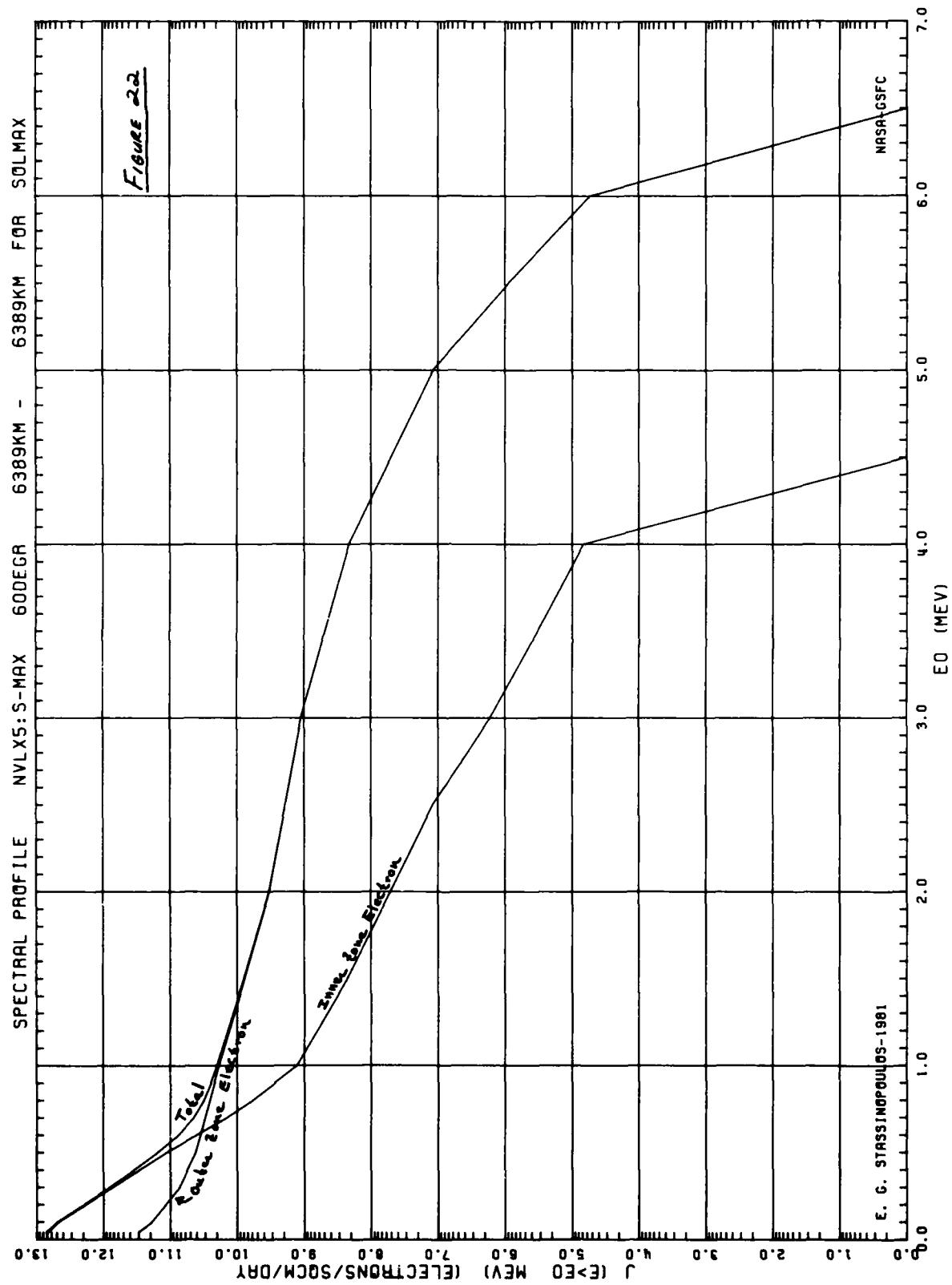


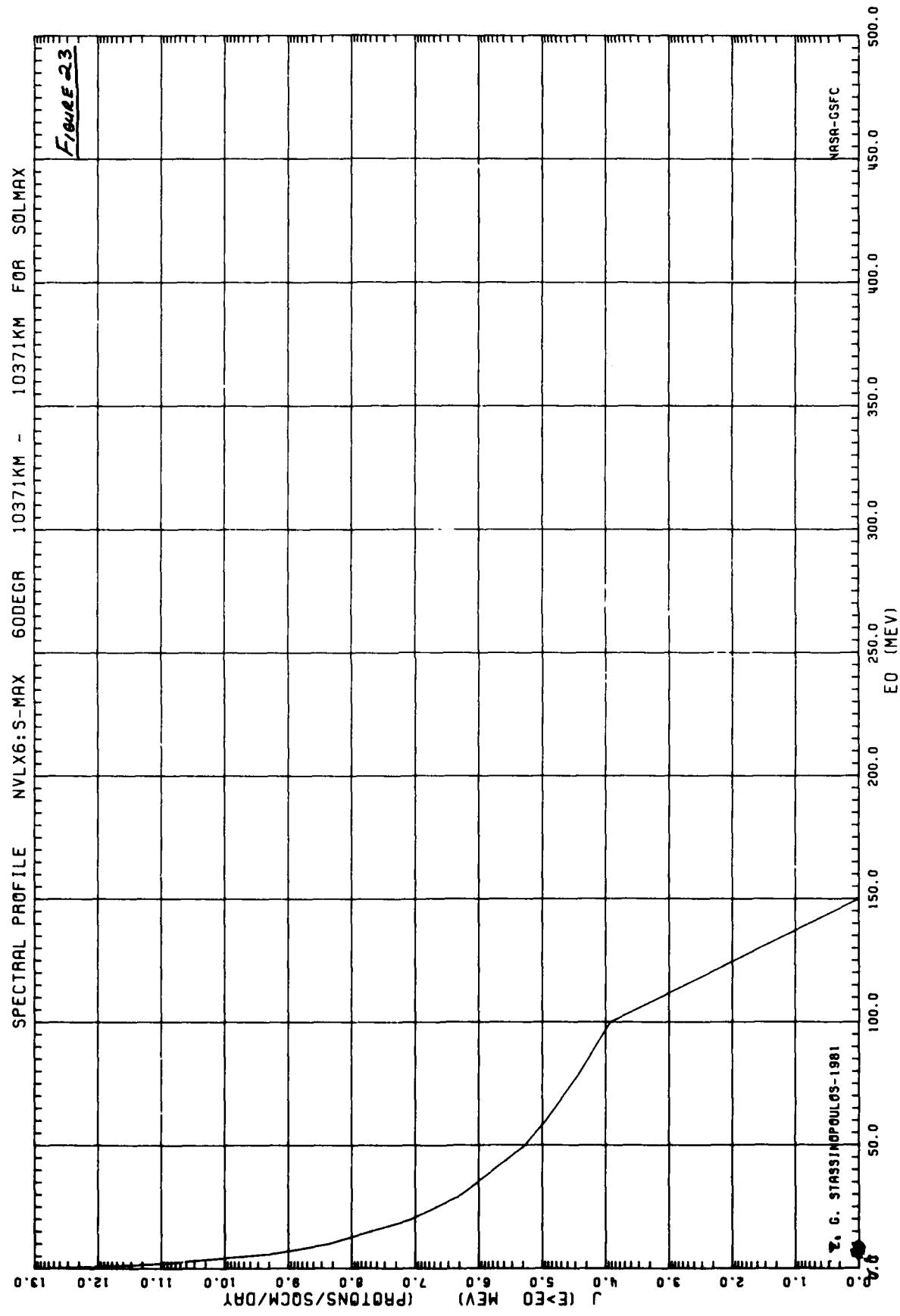
MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS 1963 A











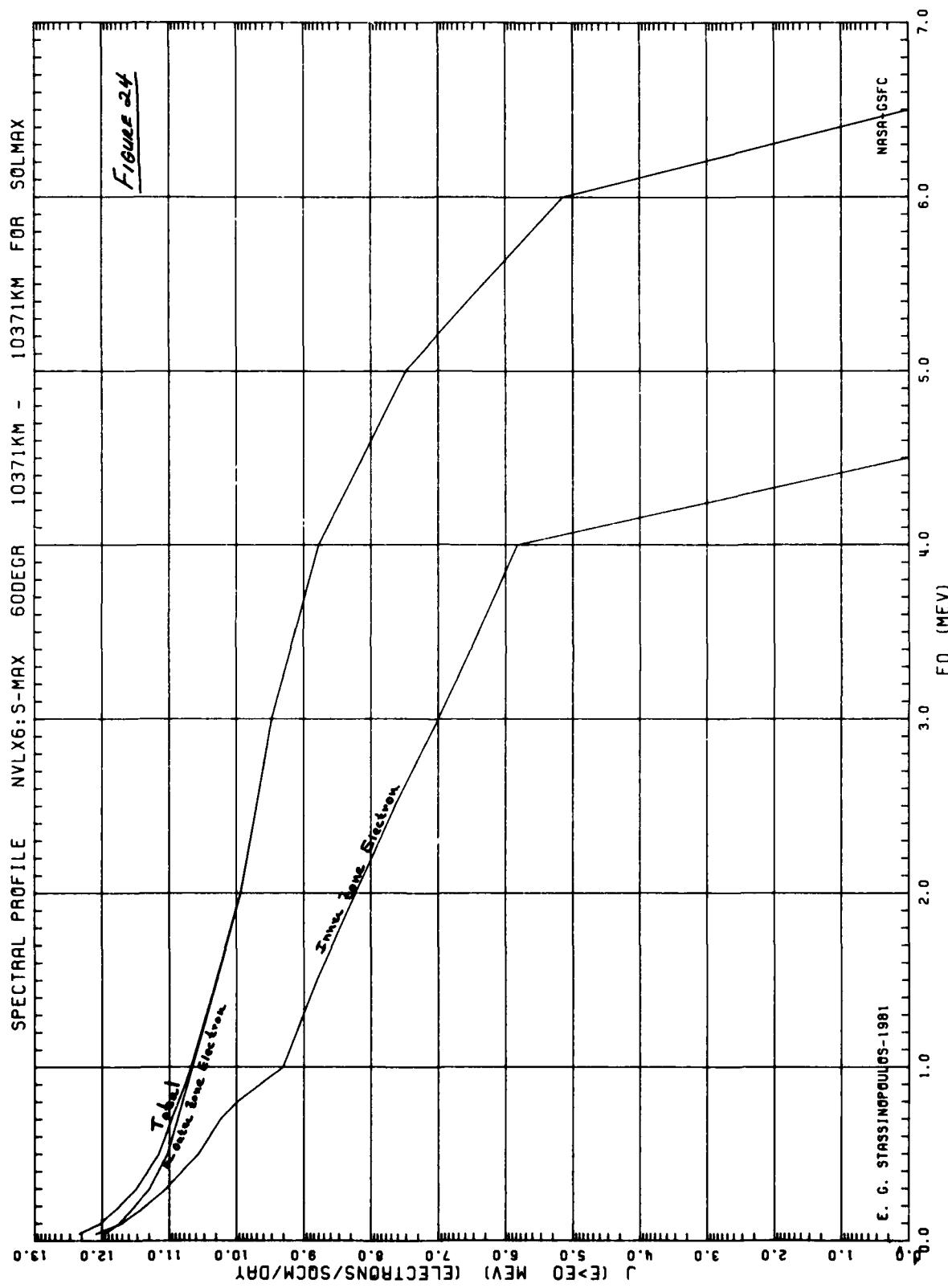
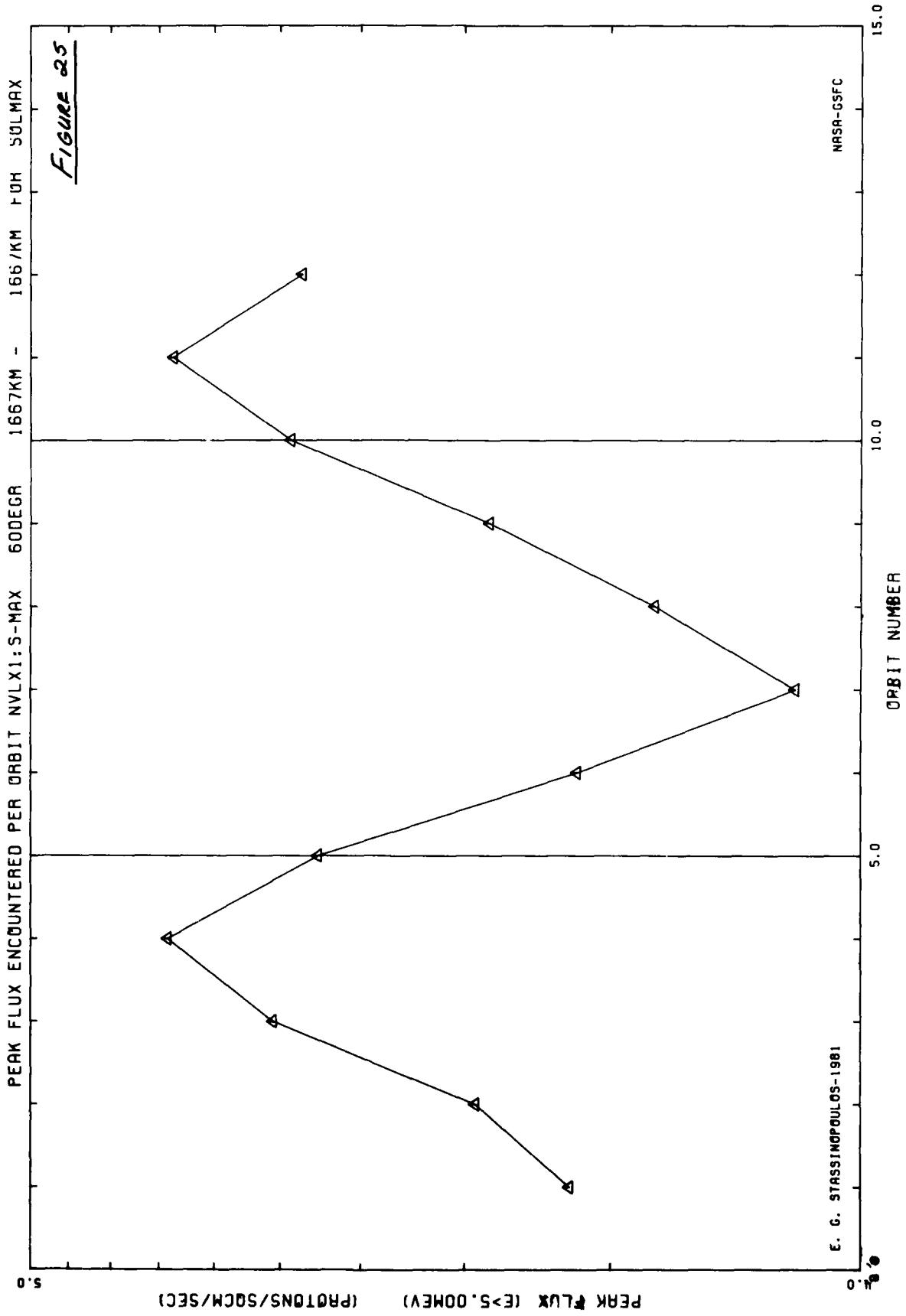
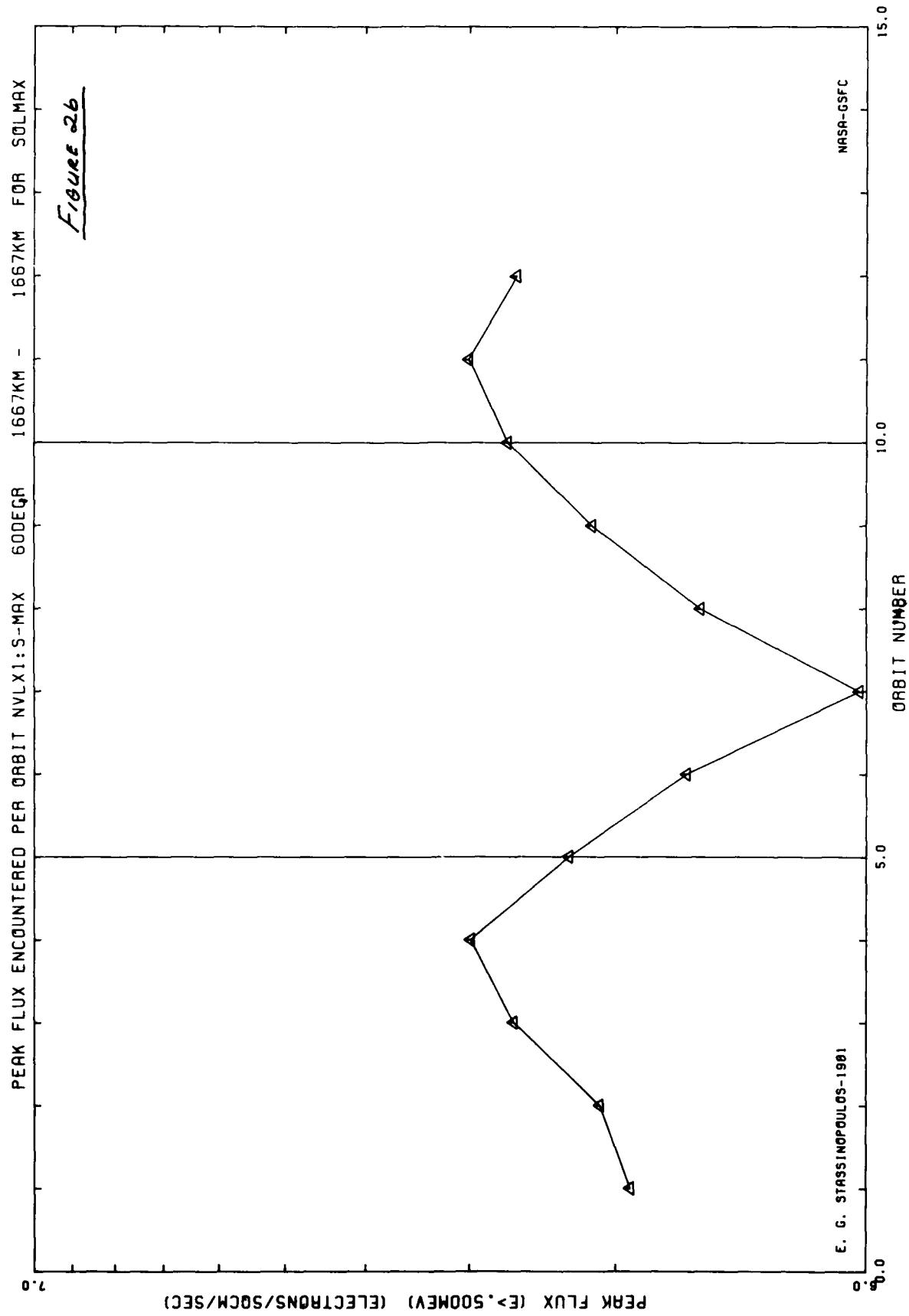
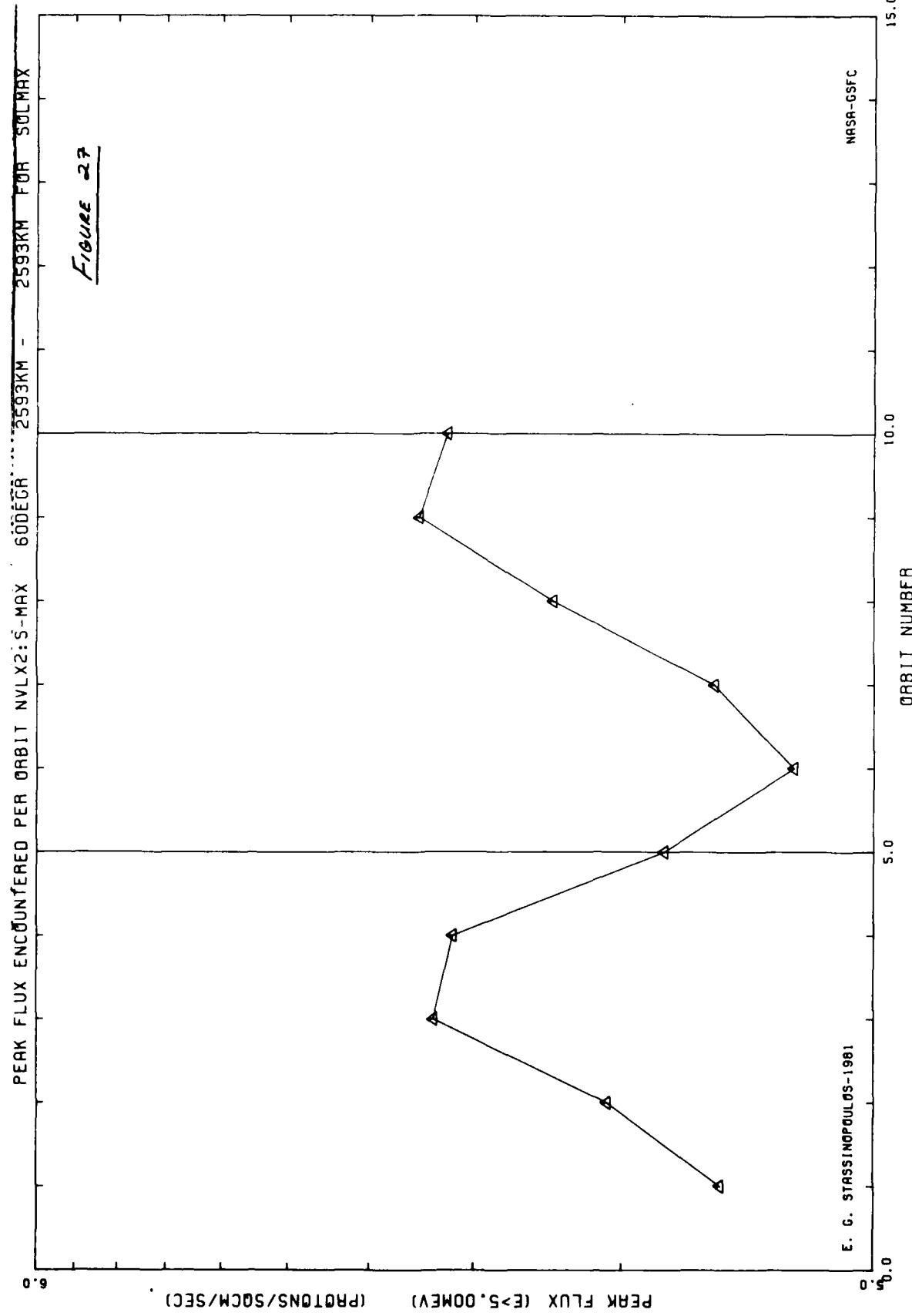
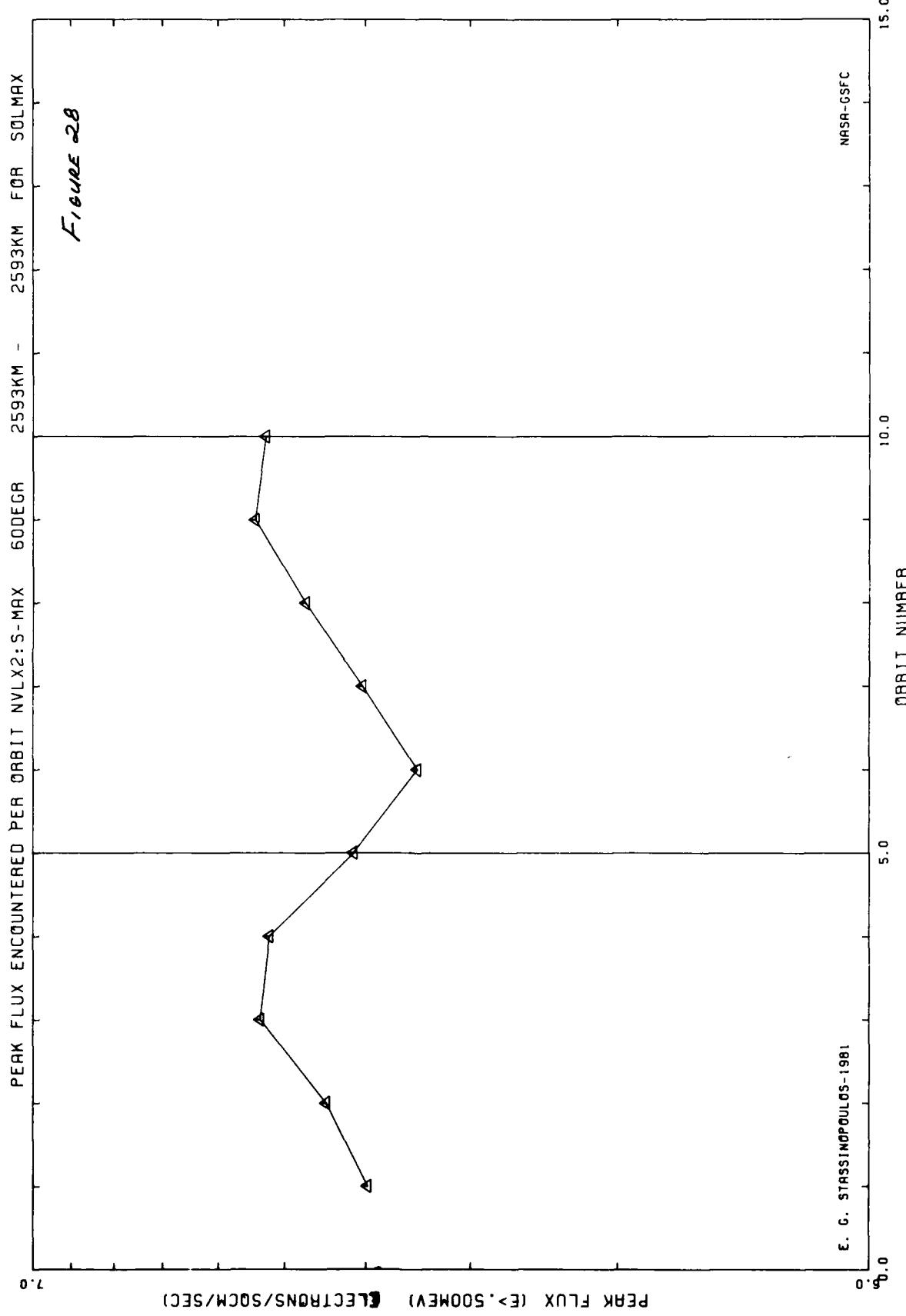


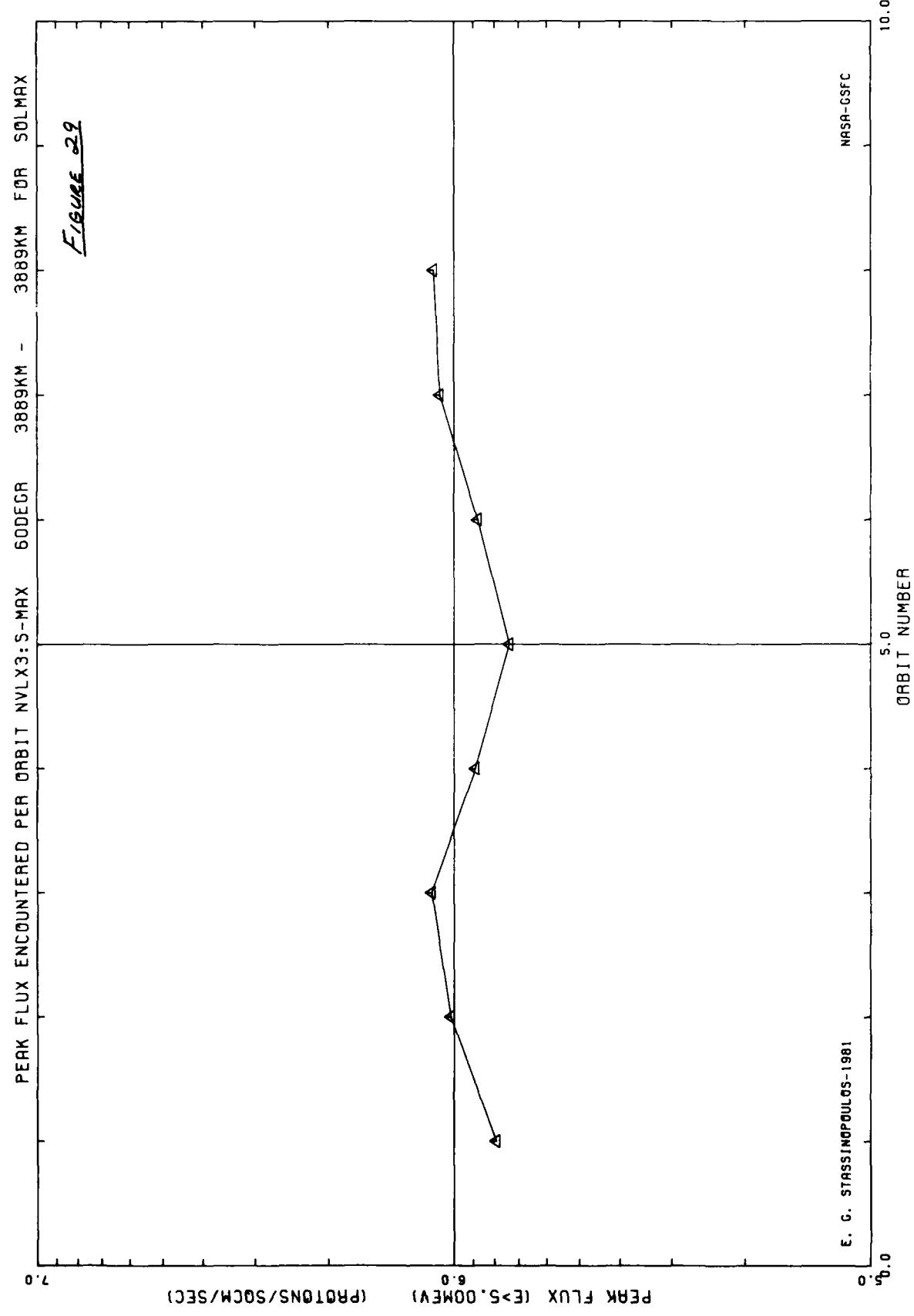
Figure 25

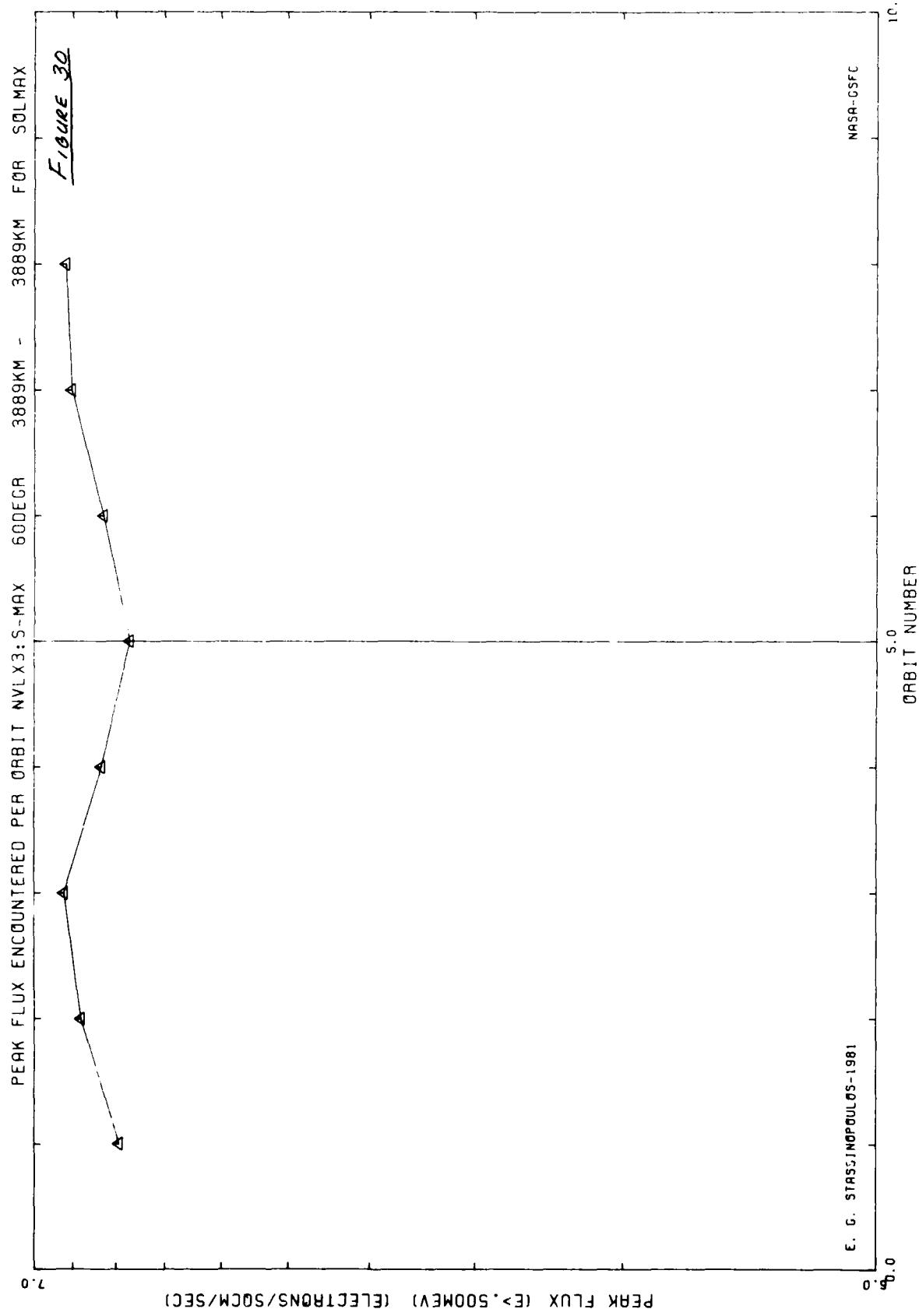


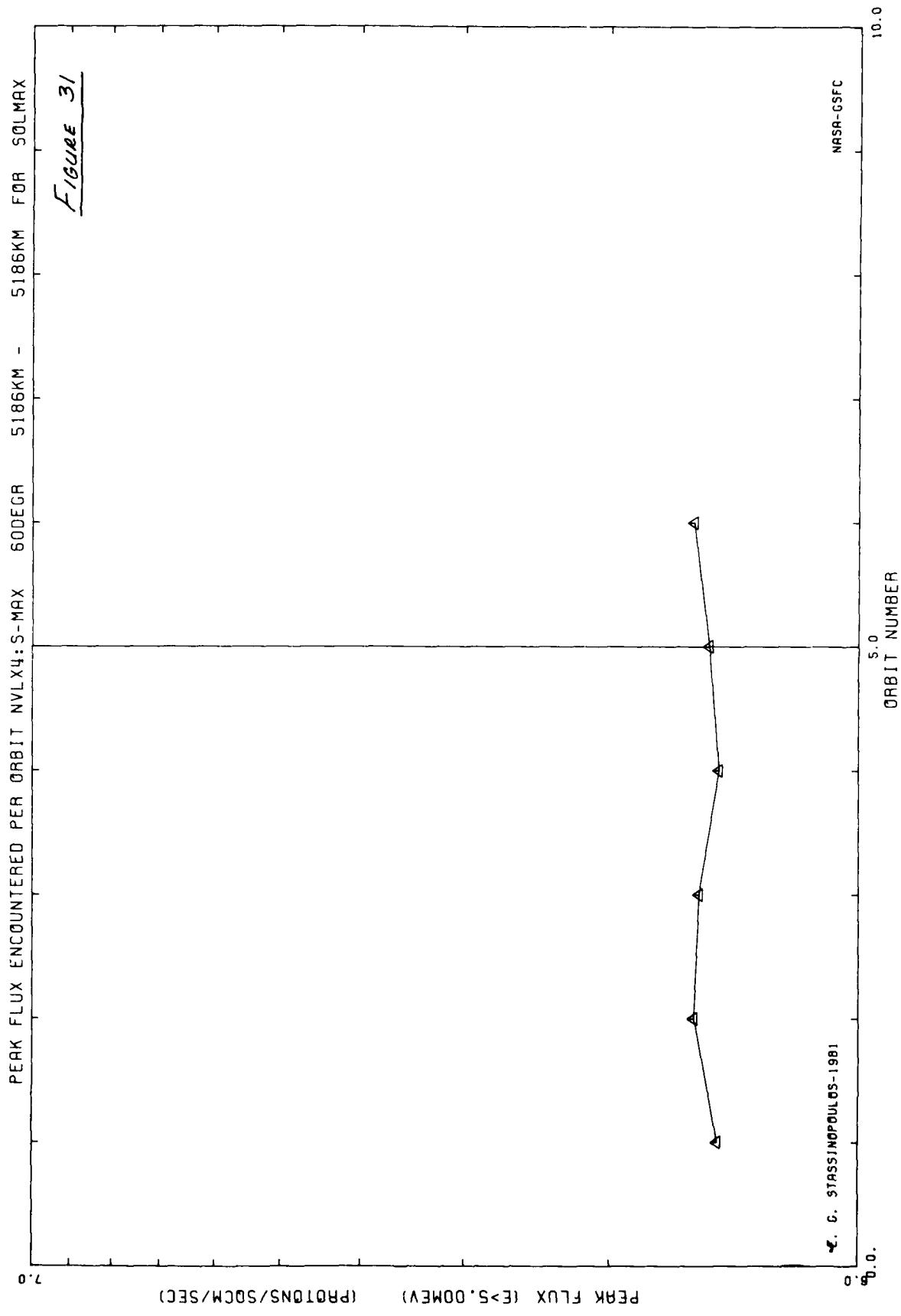


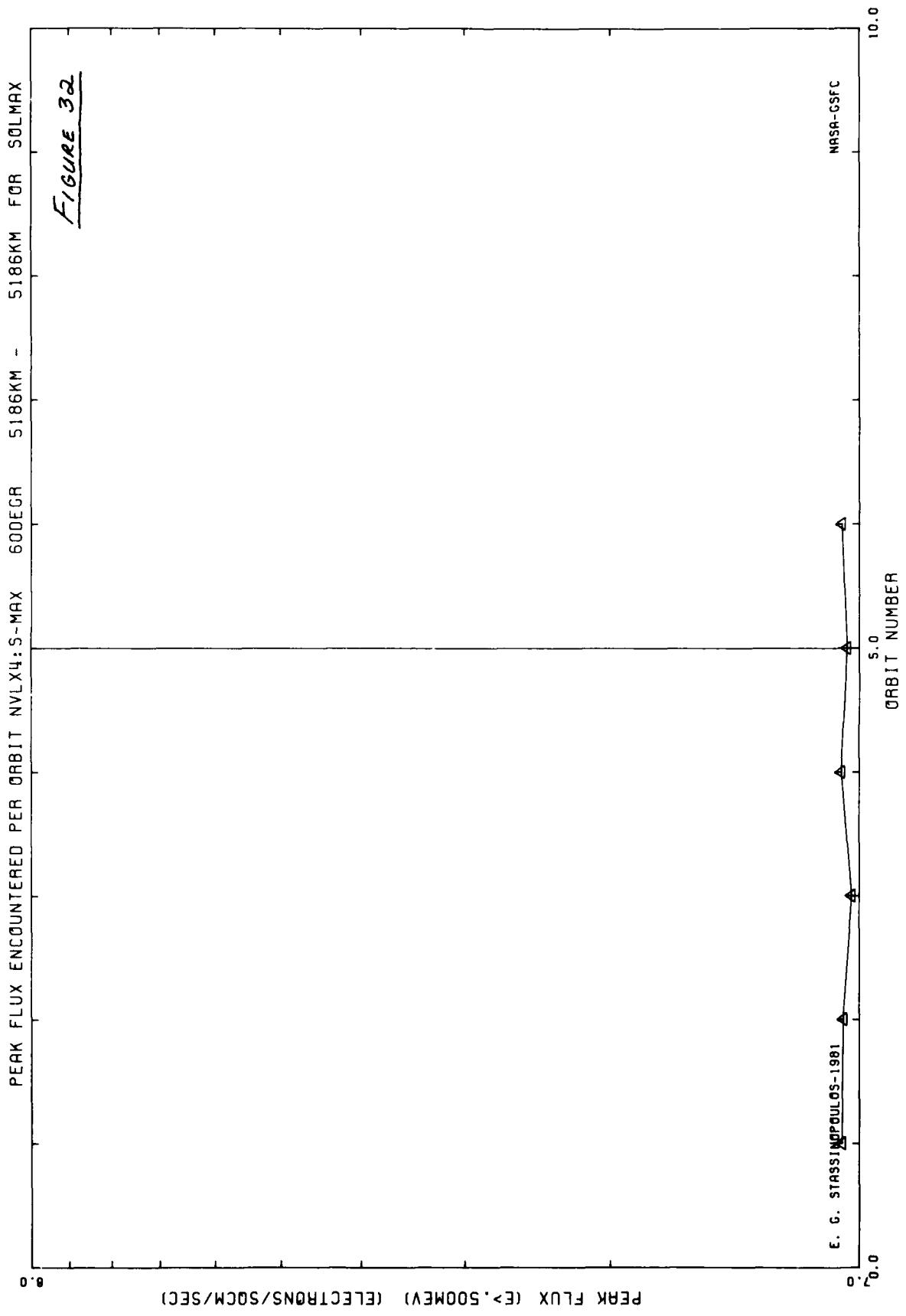


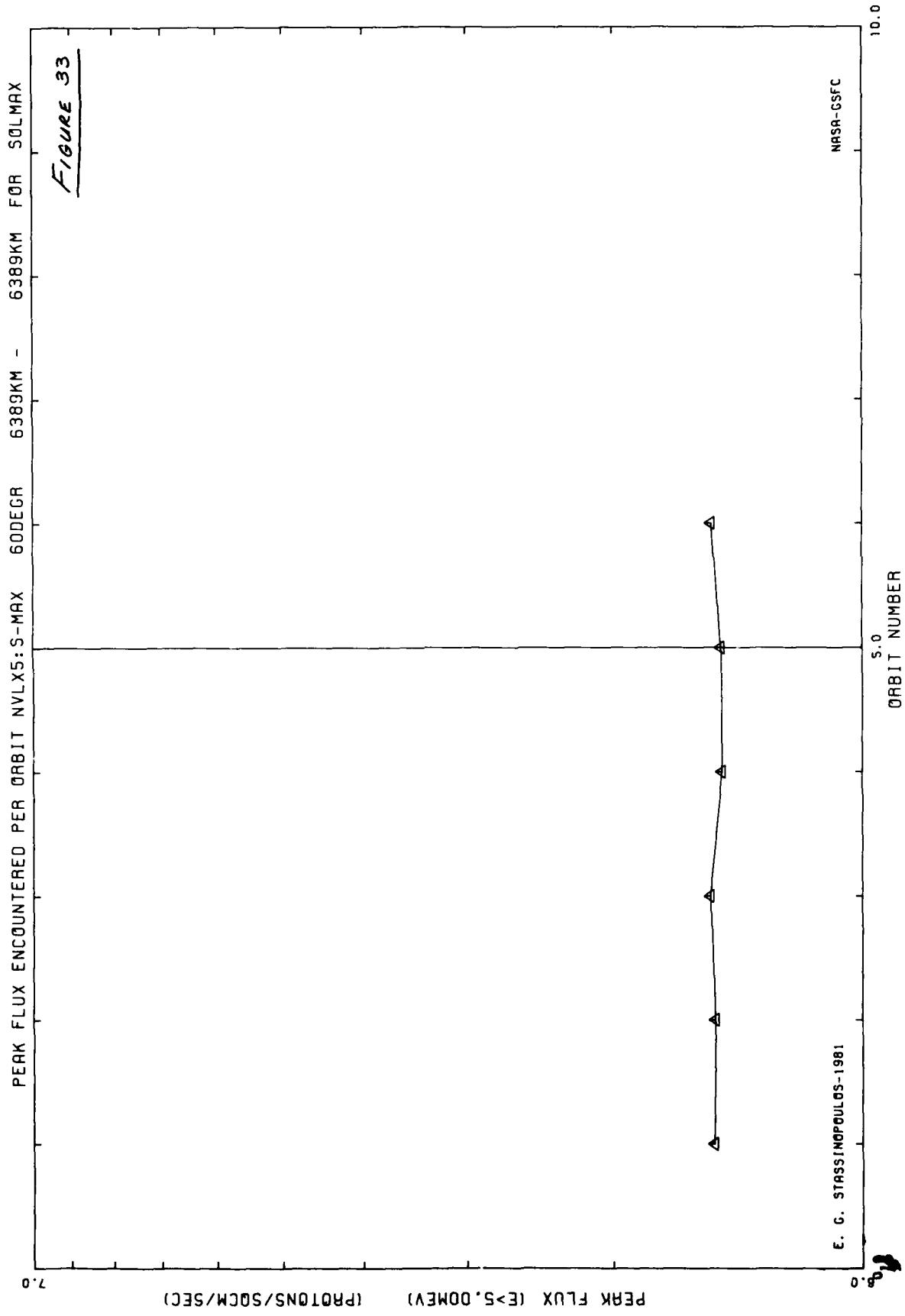


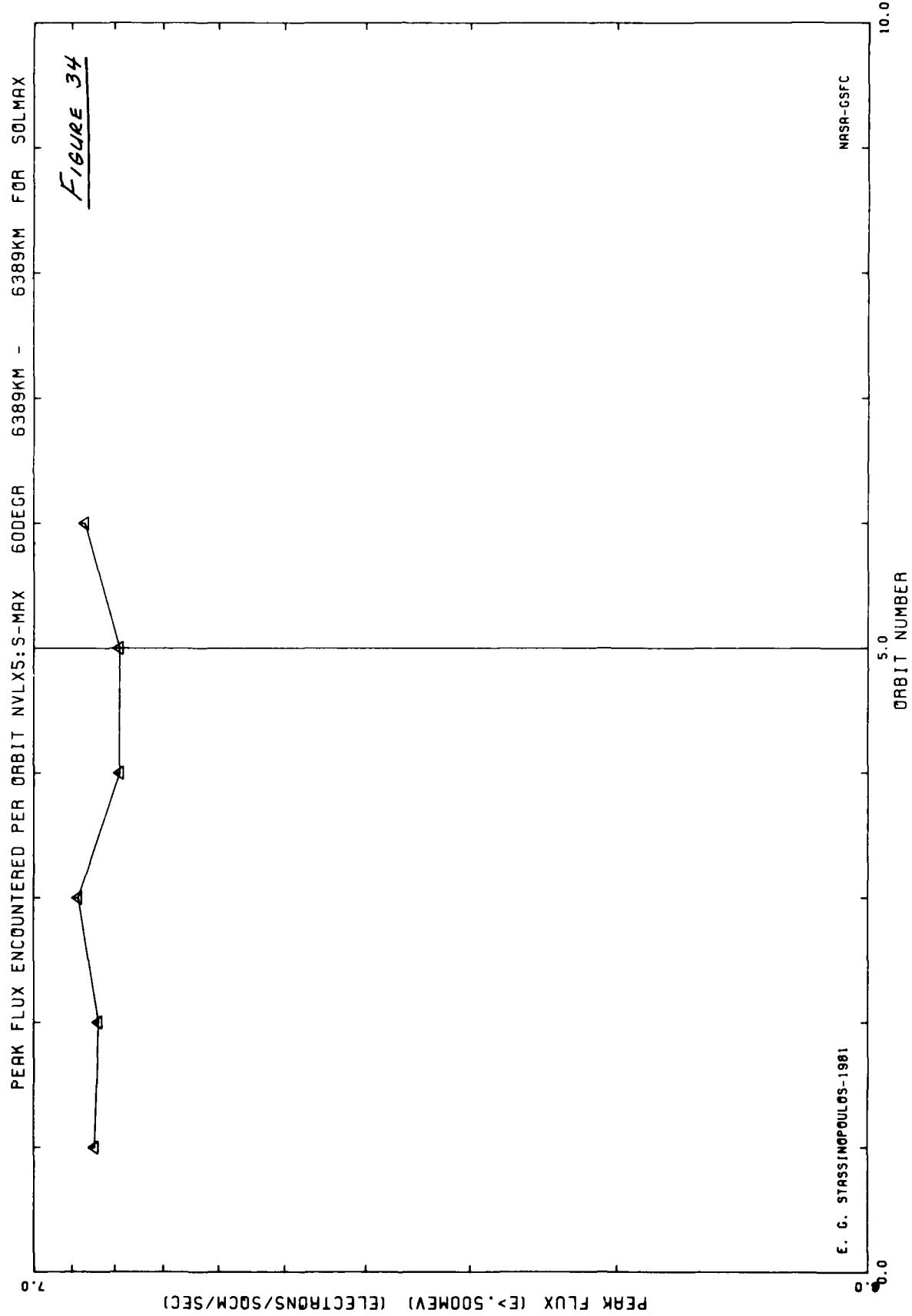


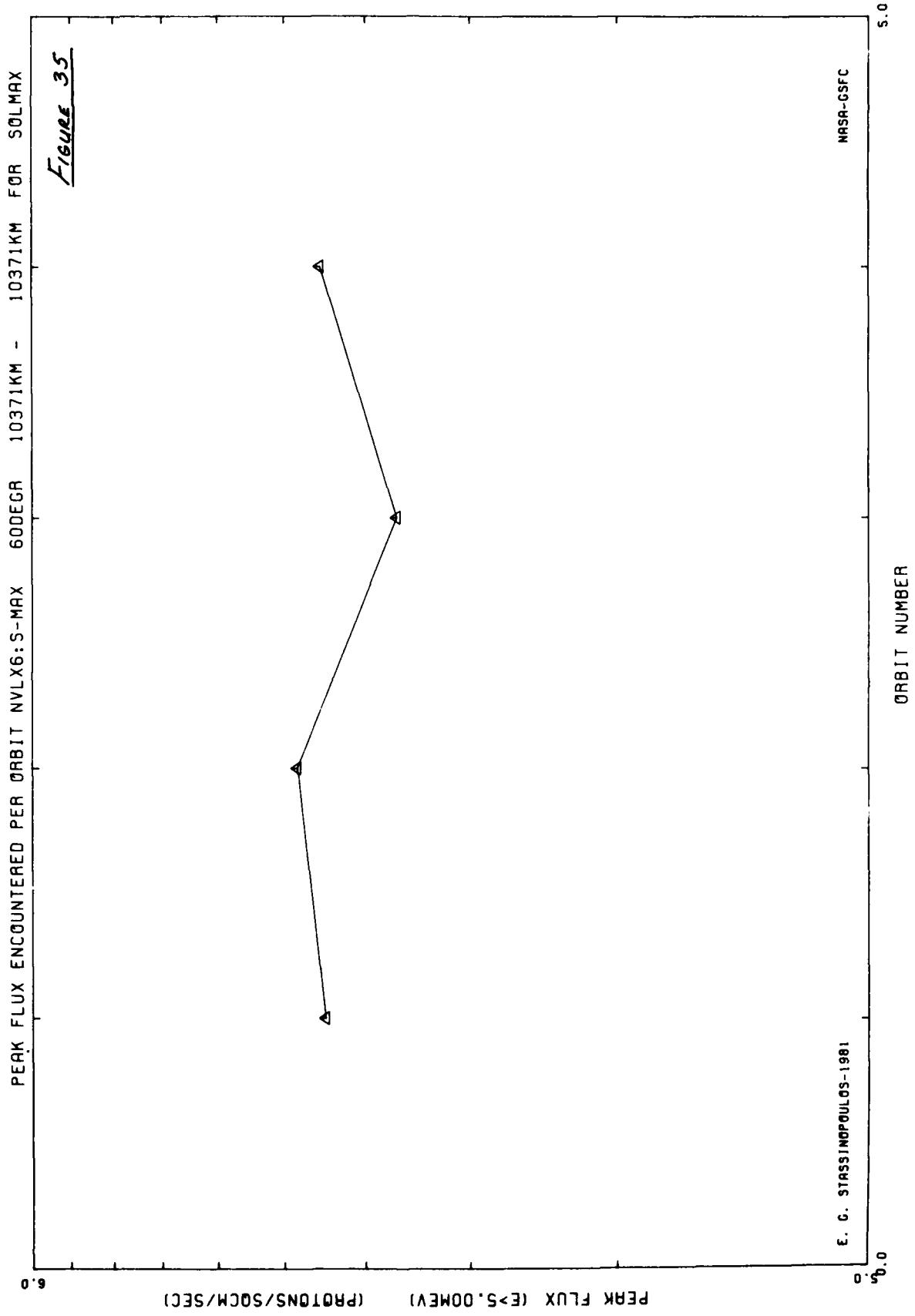


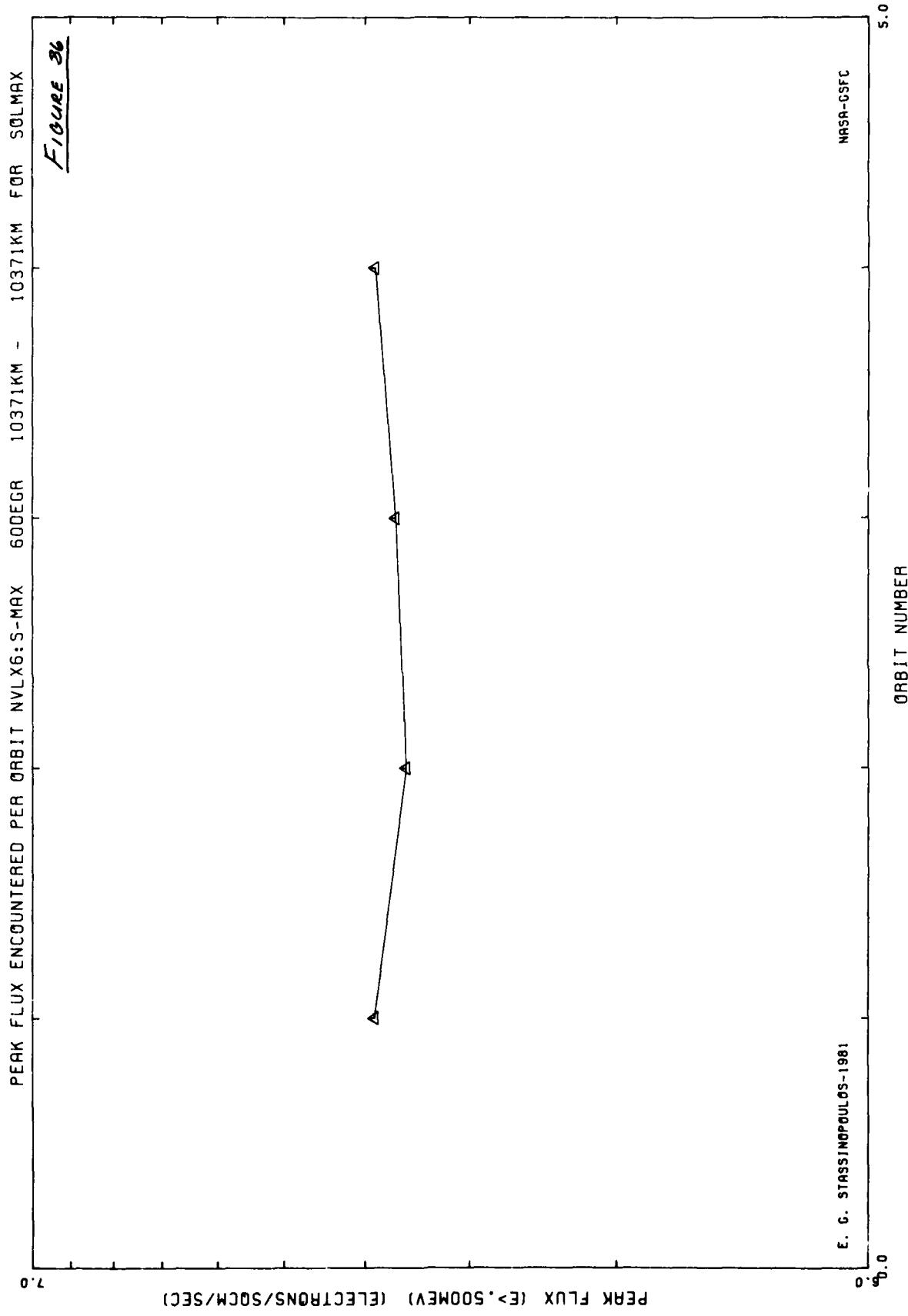


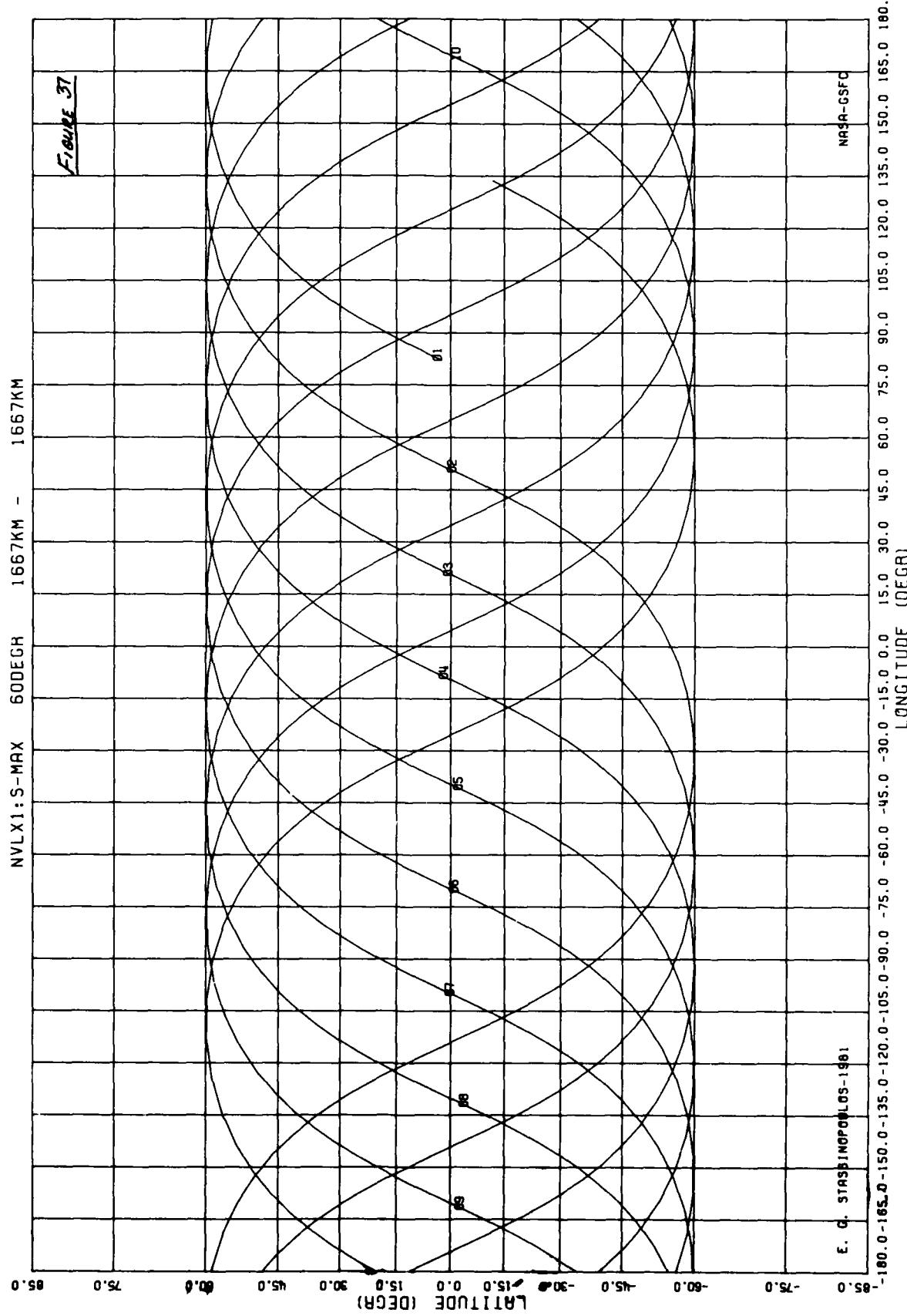


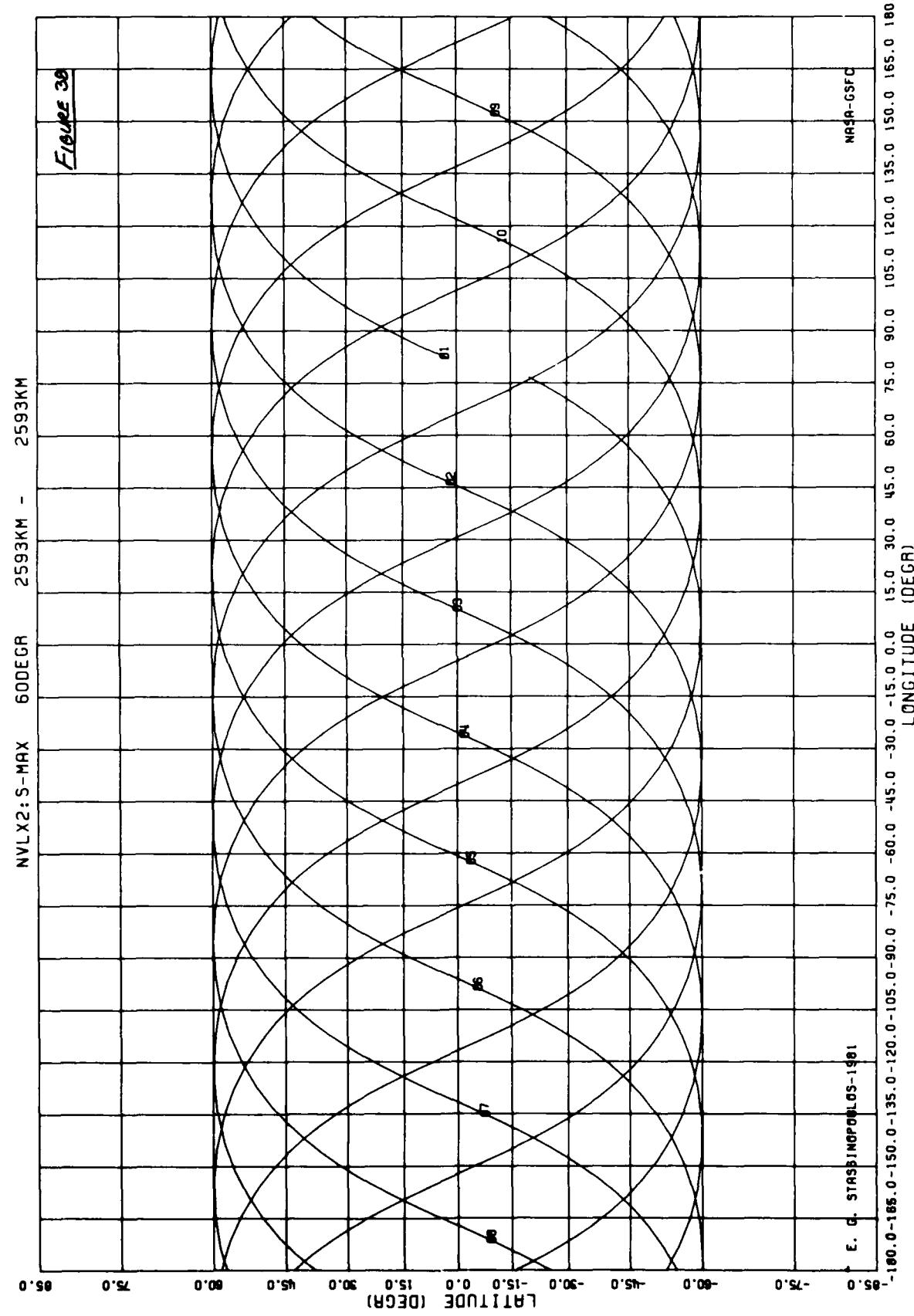


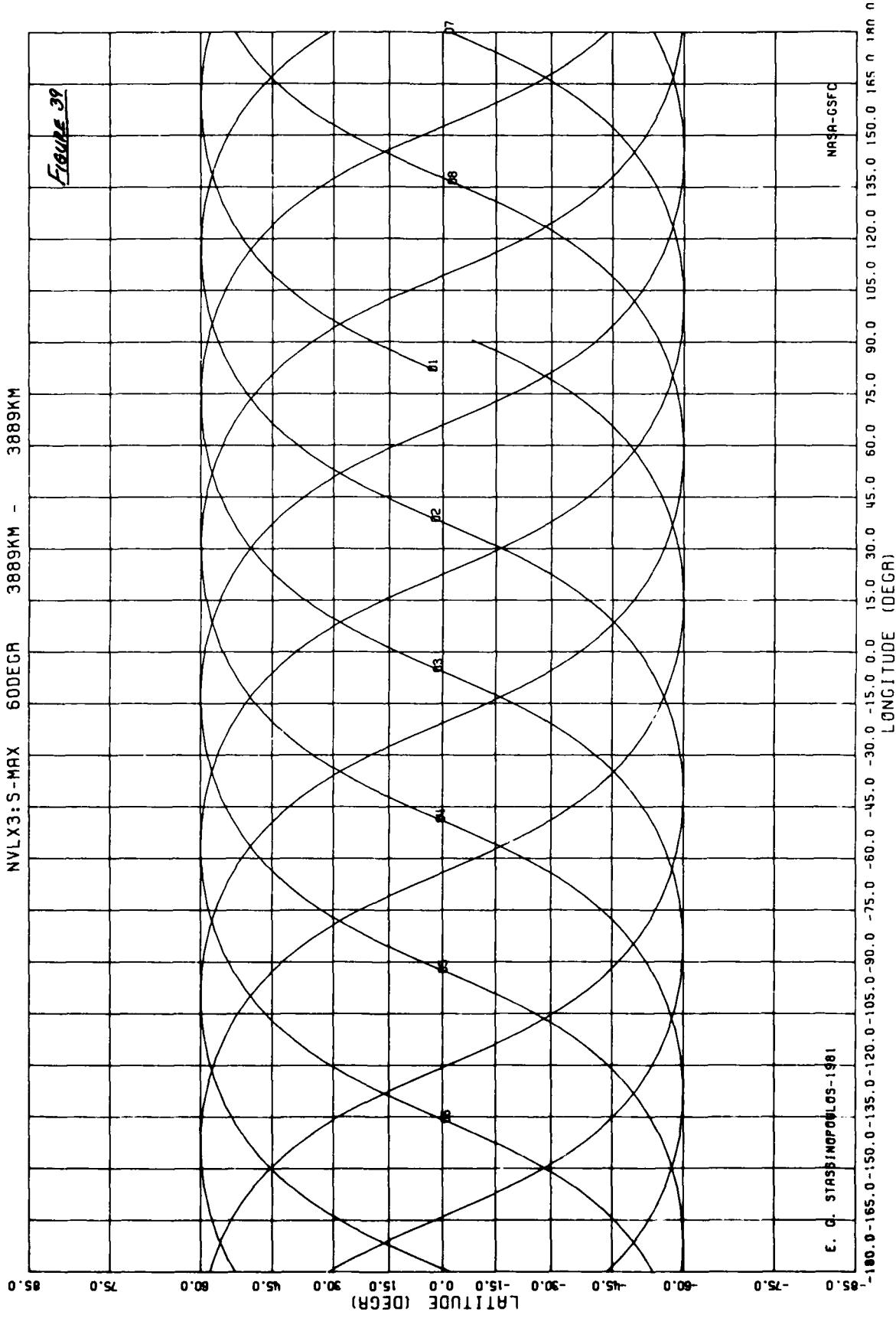


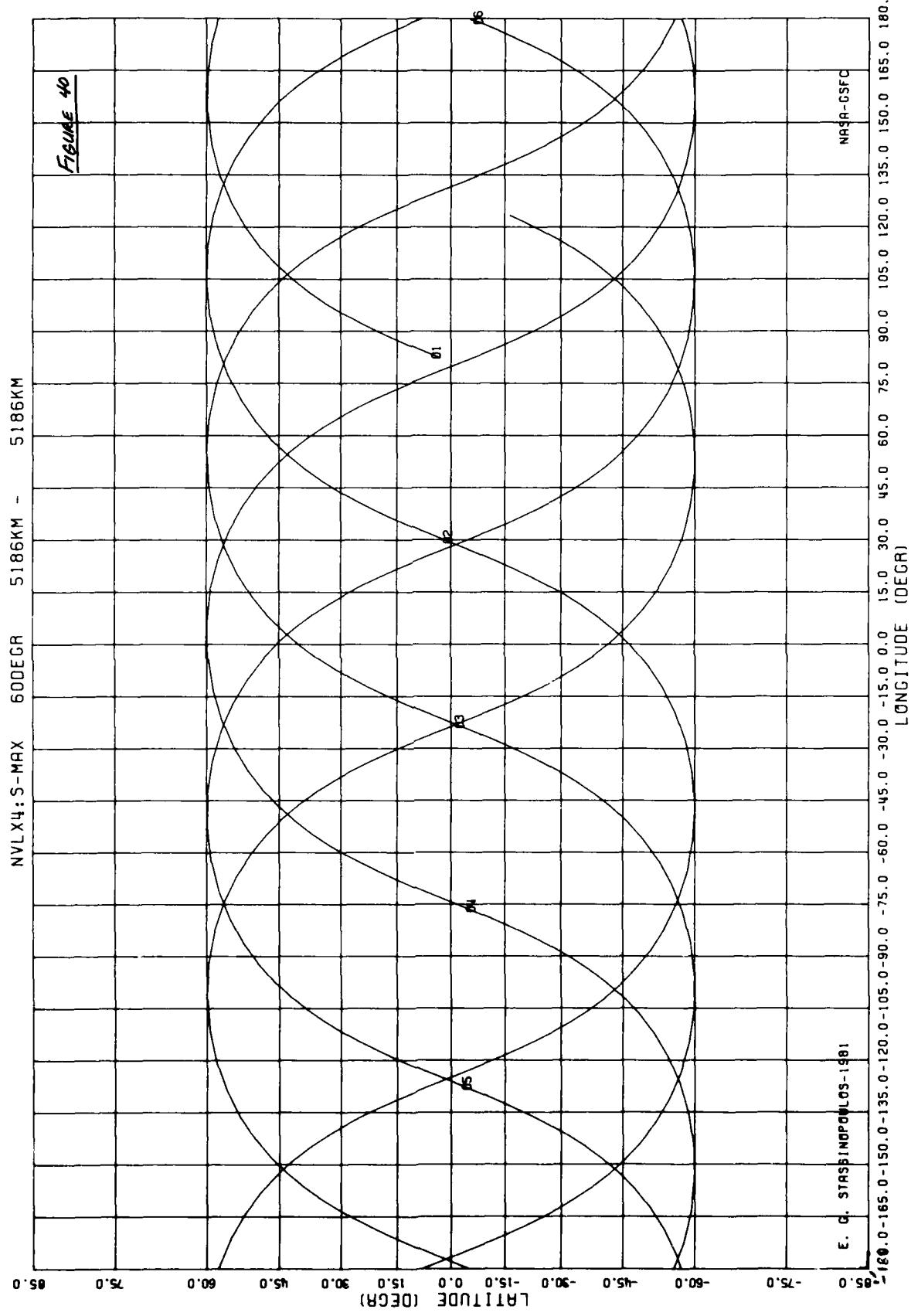


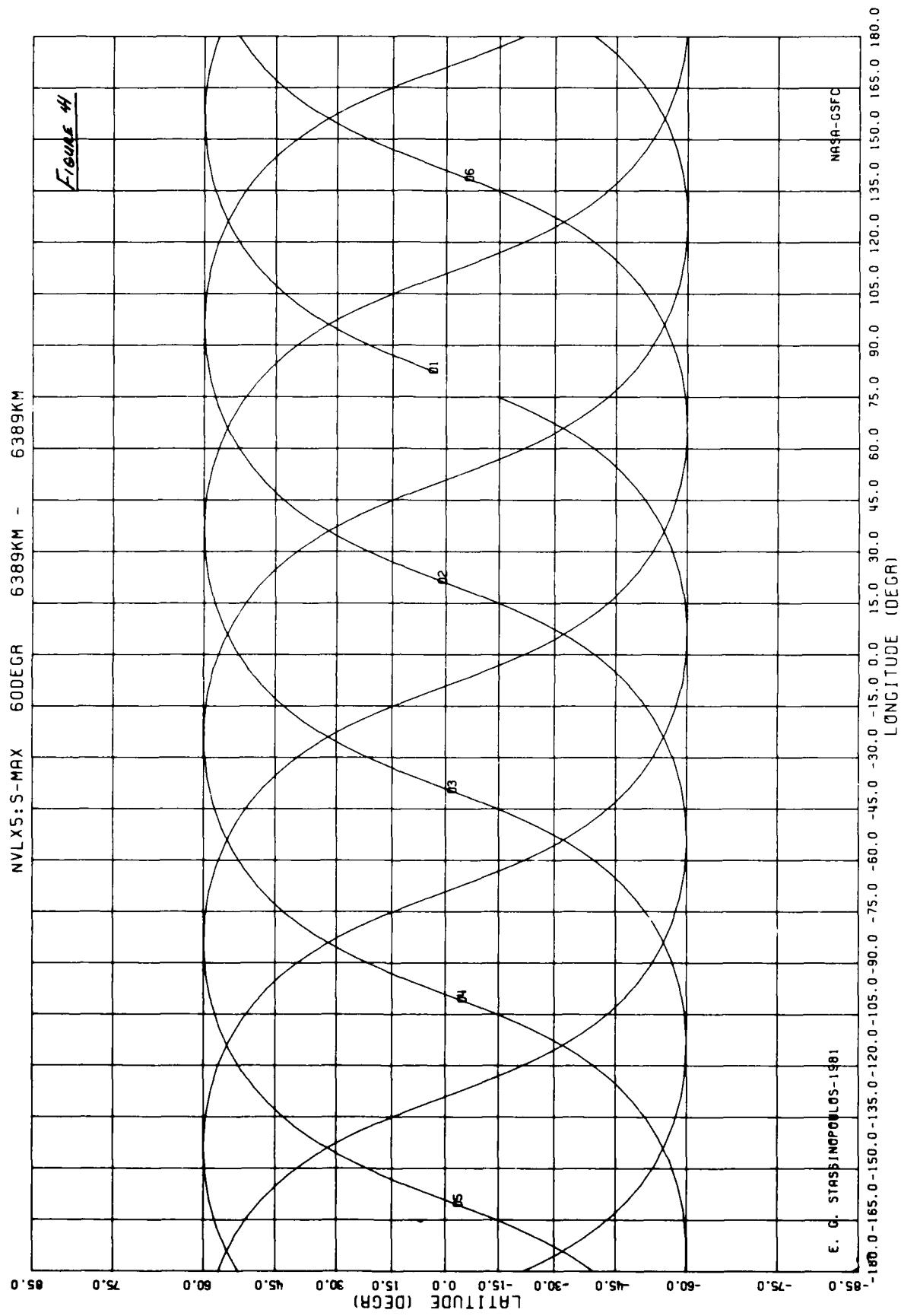


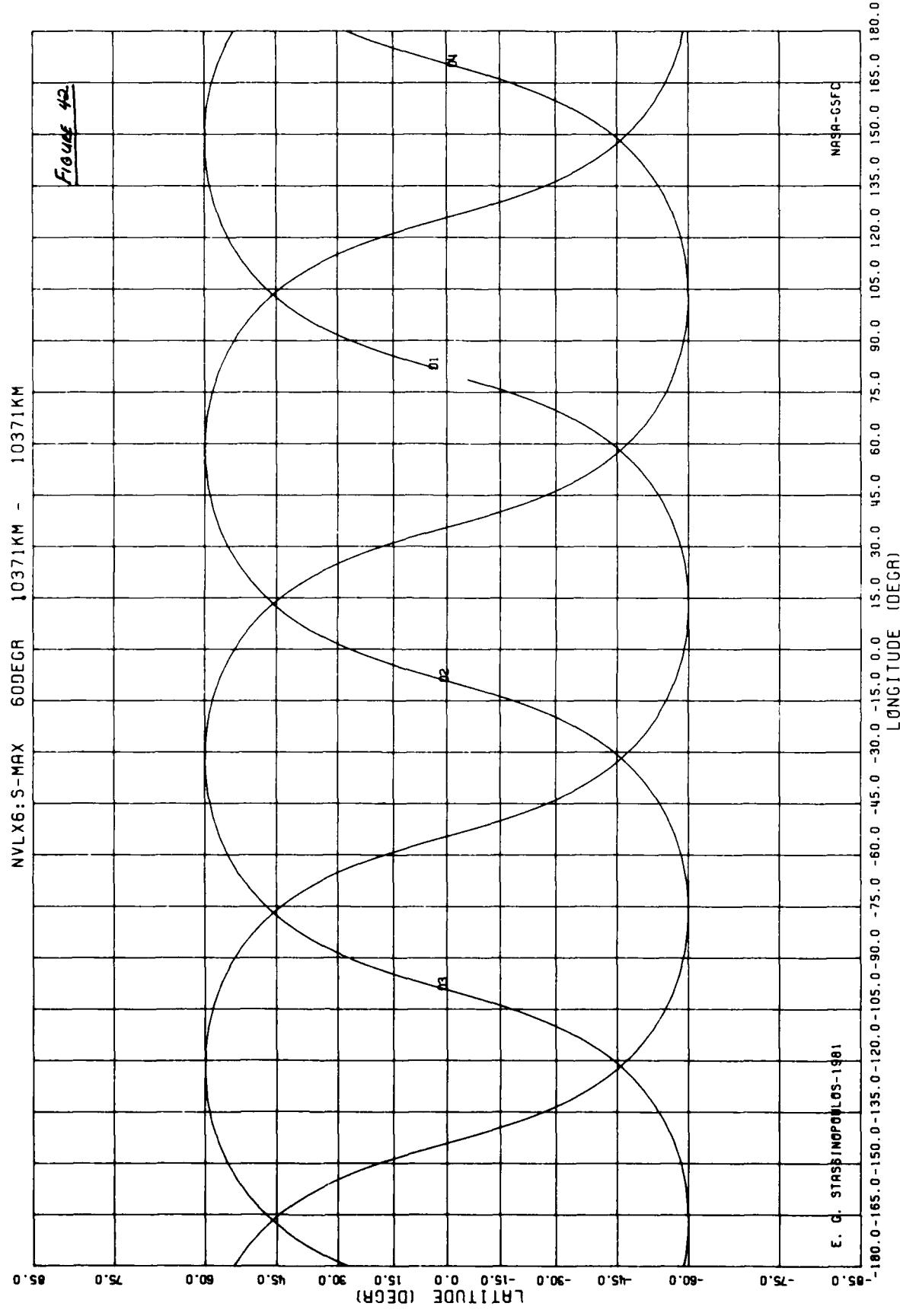


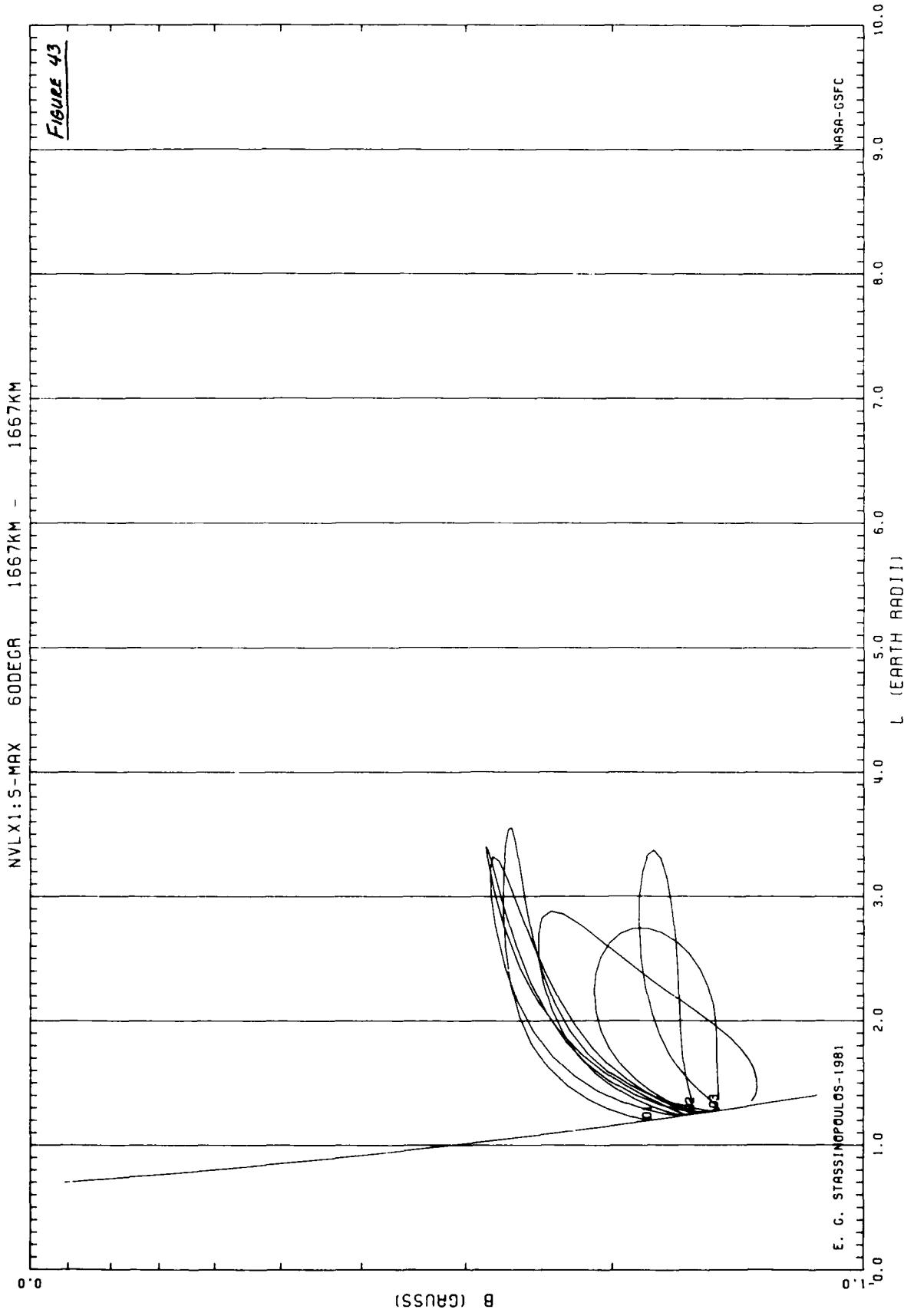


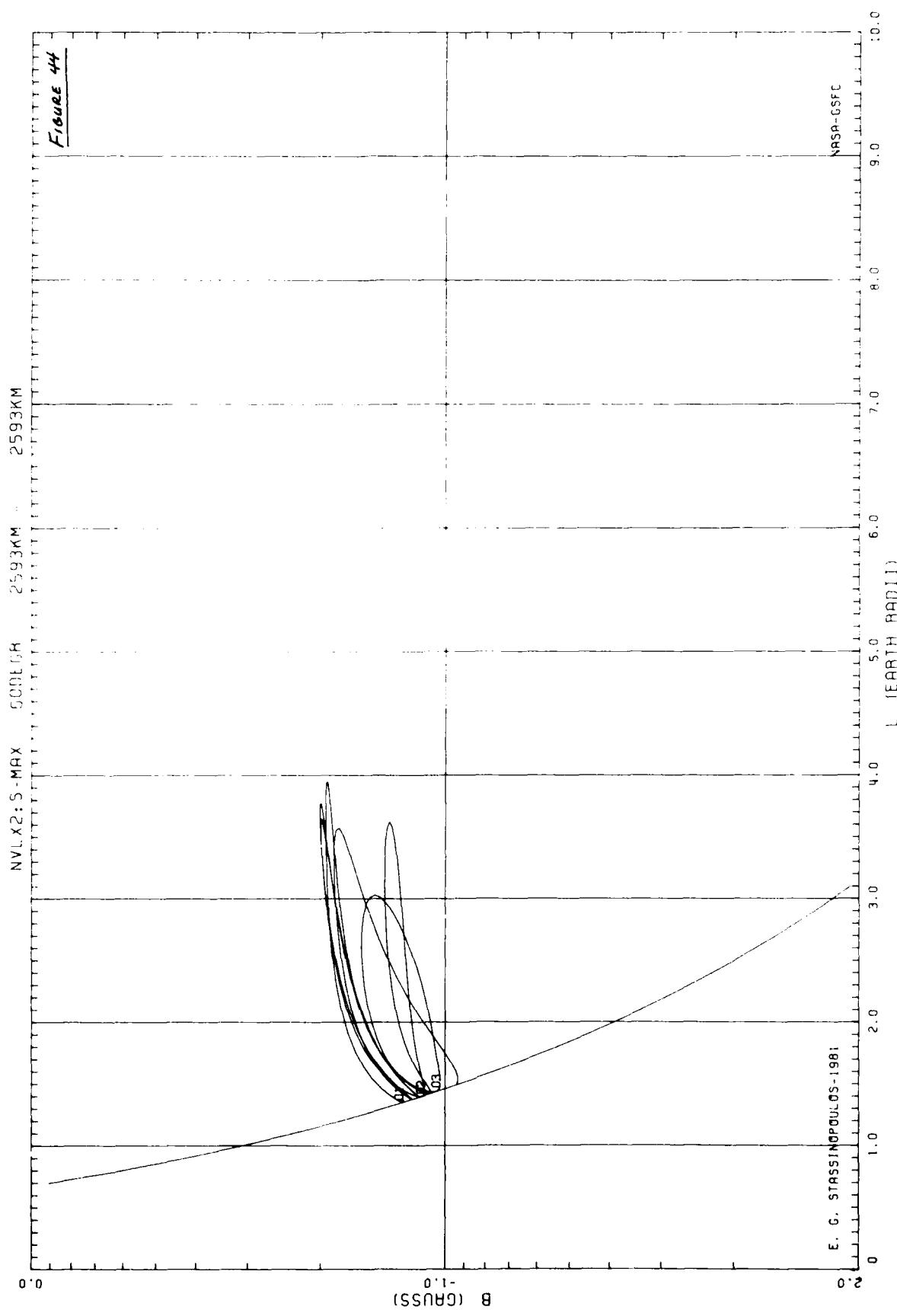


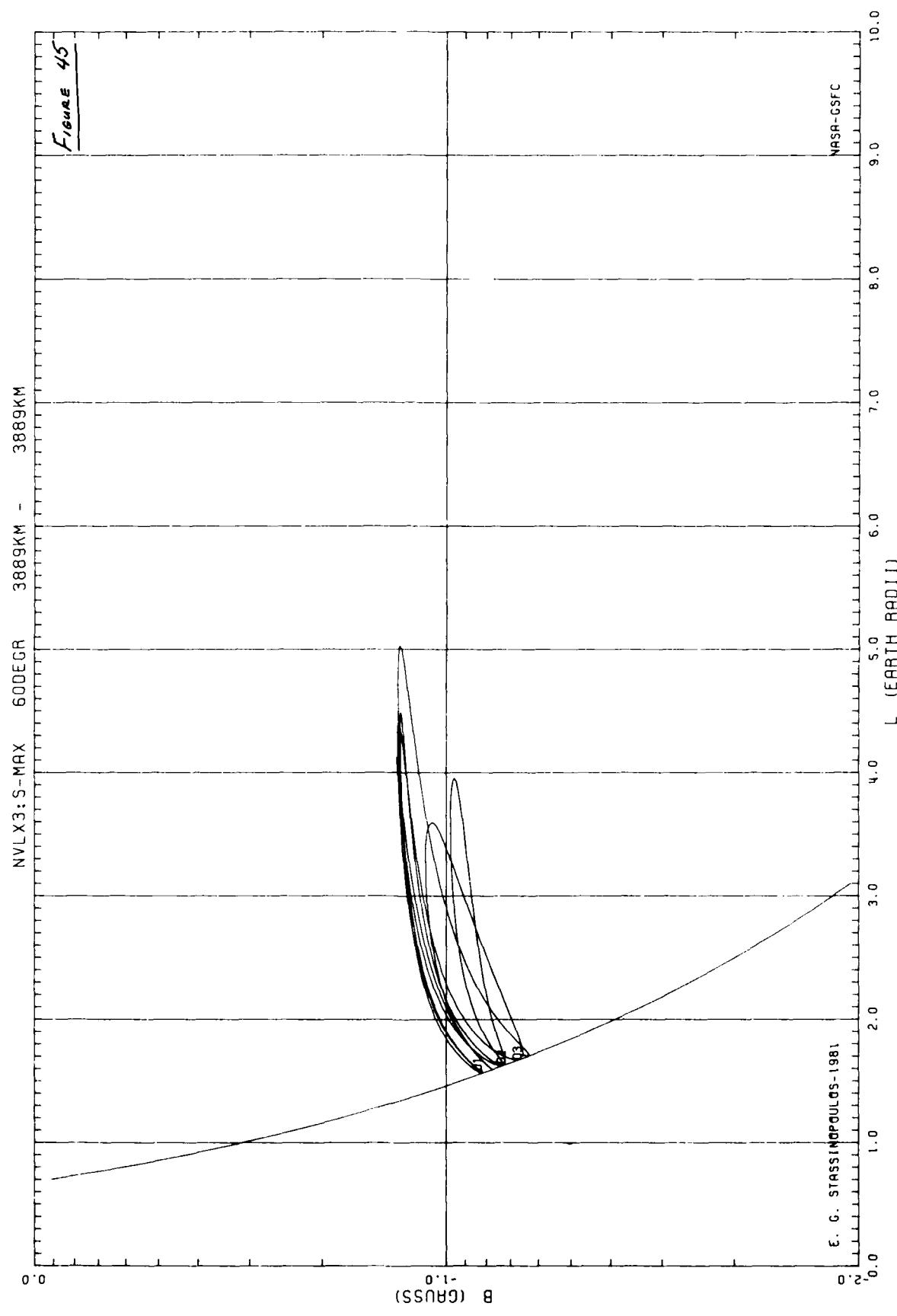


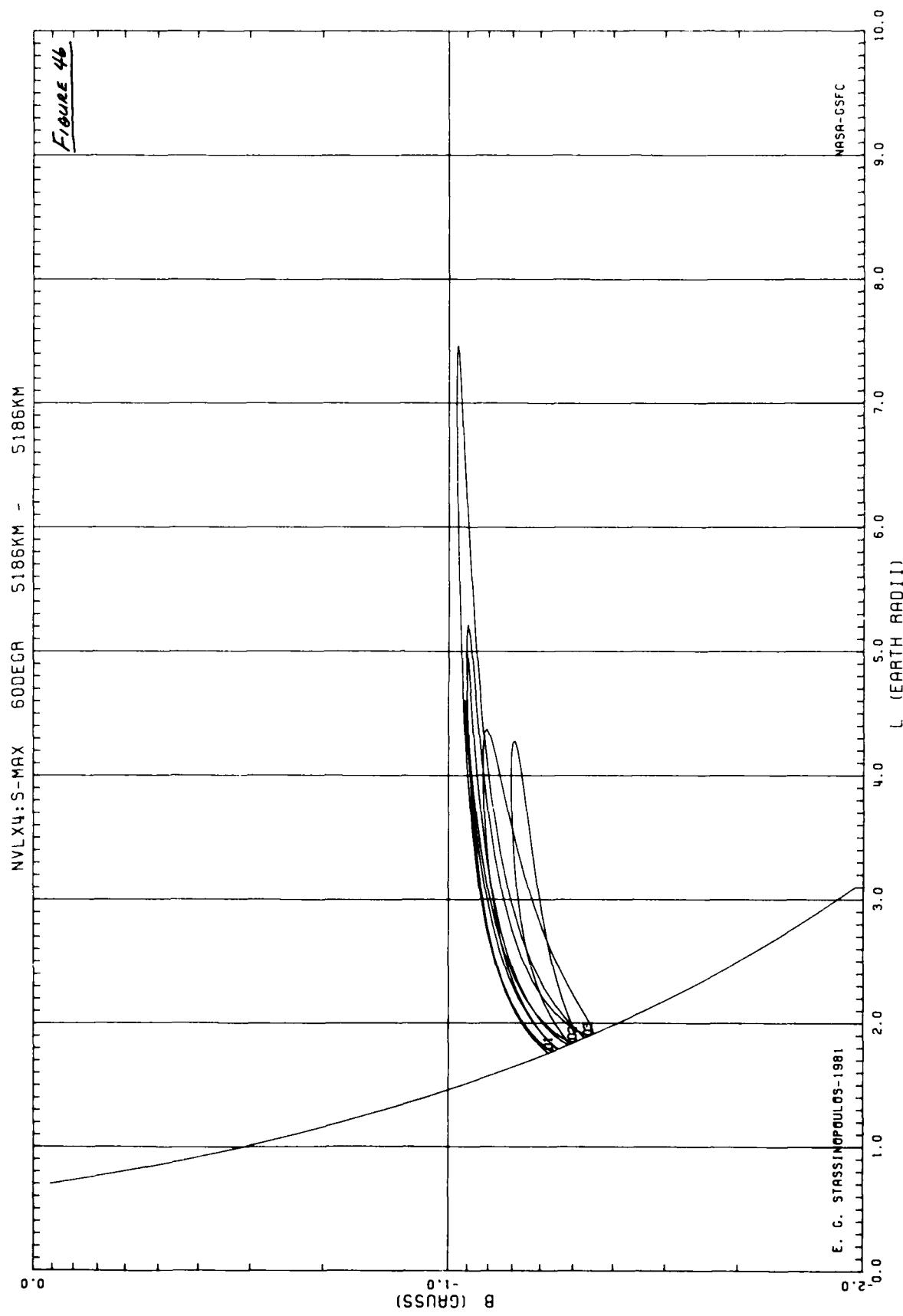


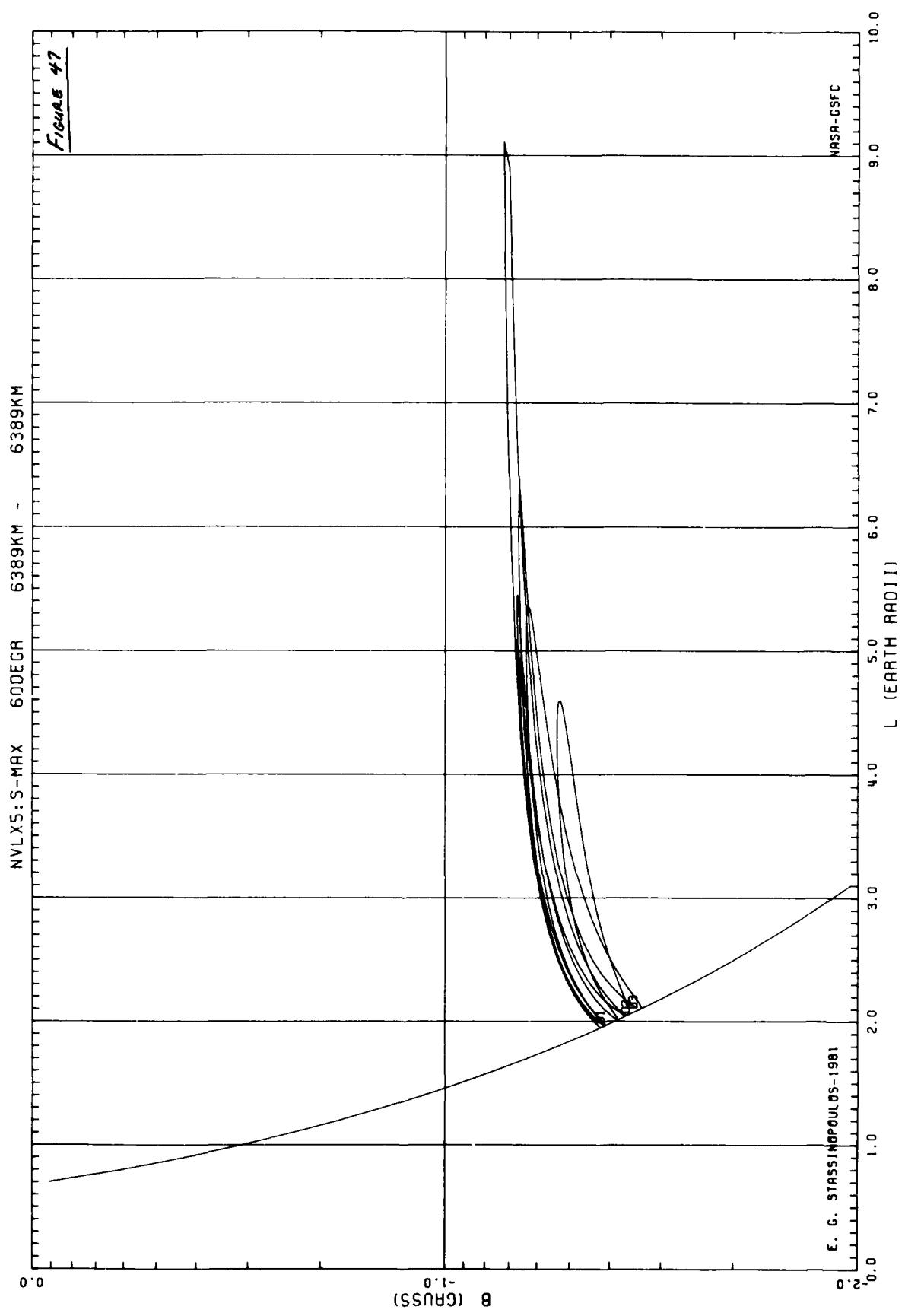












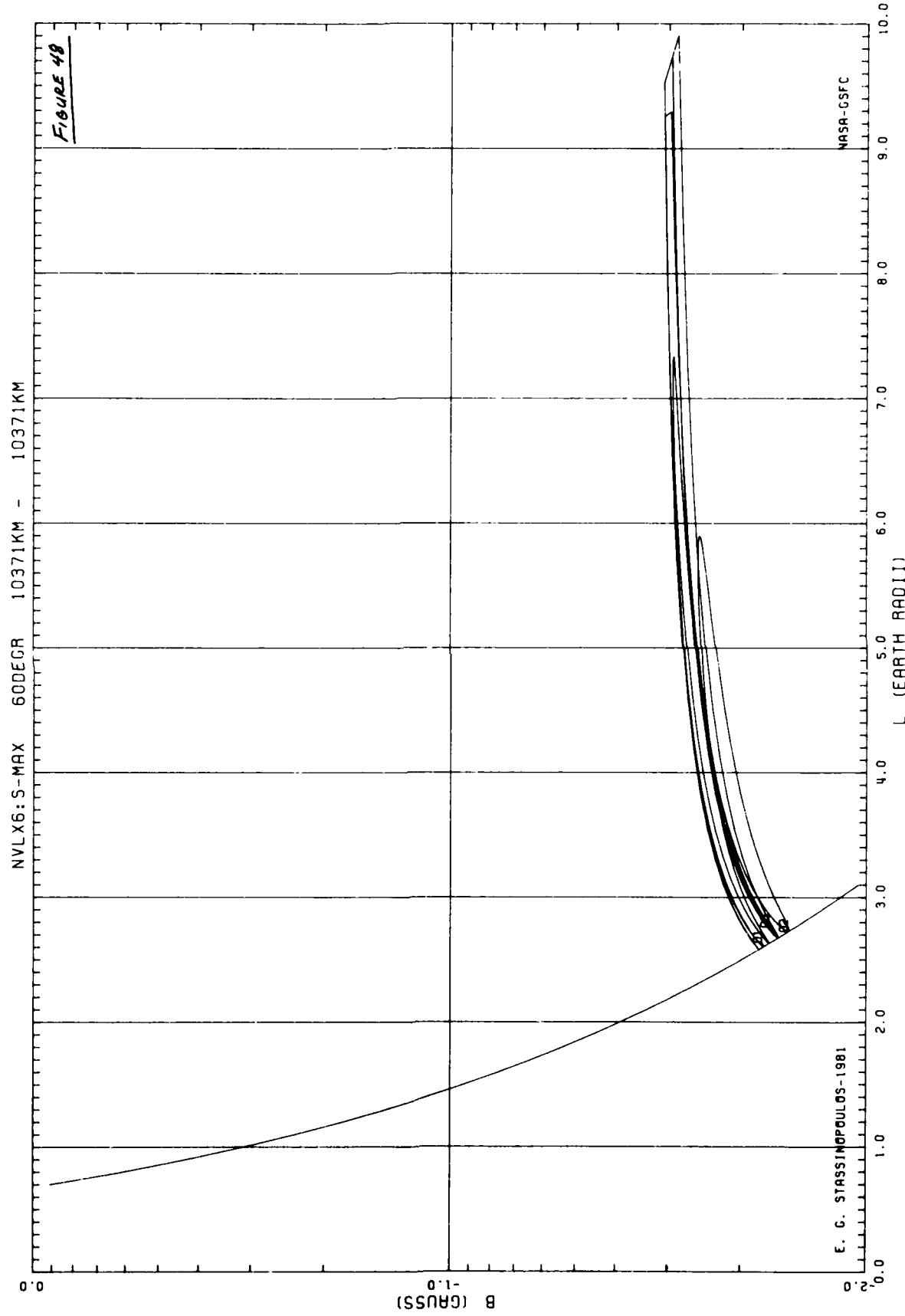


Figure 49

DOSE AT TRANSMISSION SURFACE OF FINITE ALUMINUM SLAB SHIELDS ** NVLX1: S-MAX

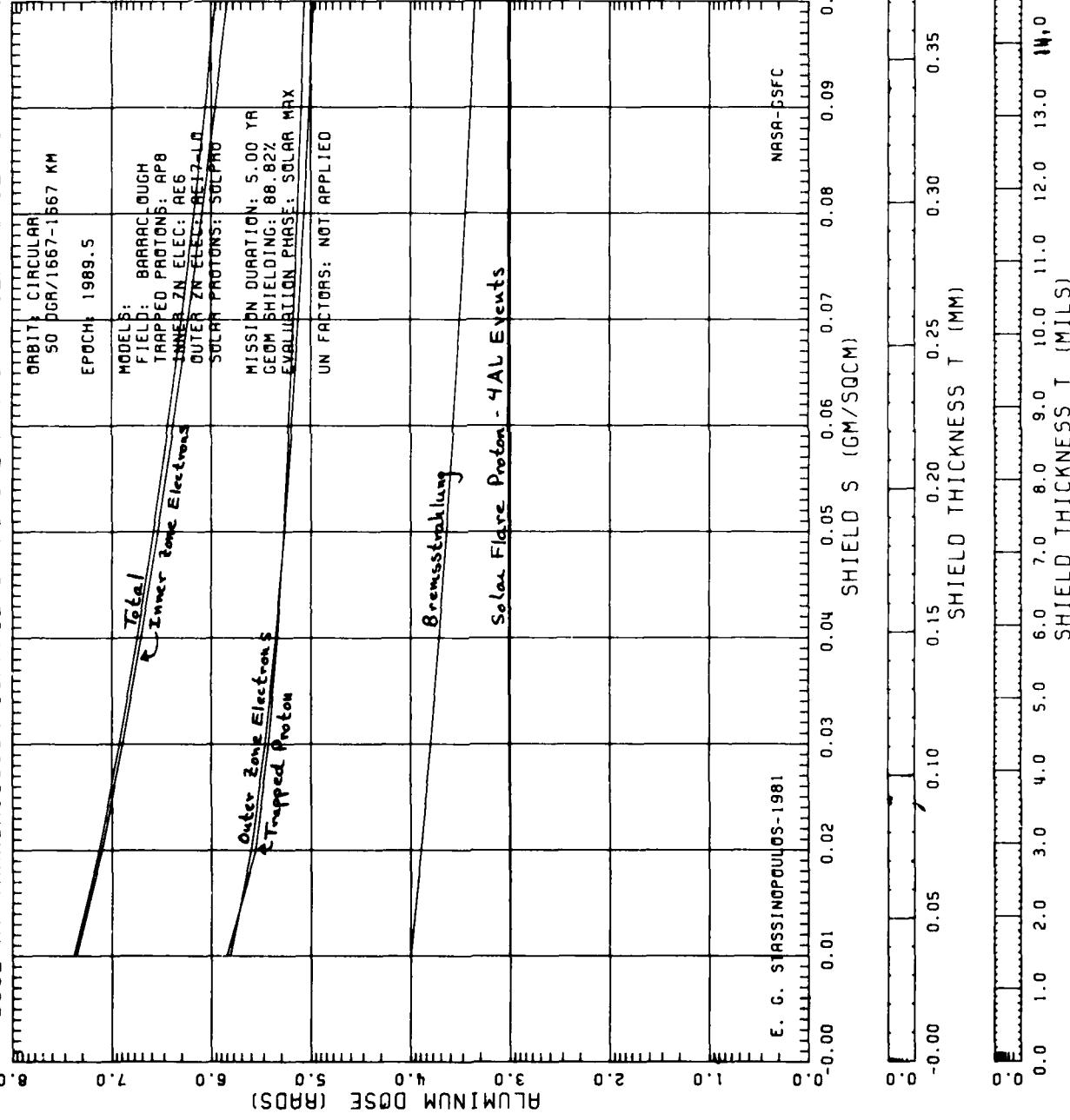


Figure 50

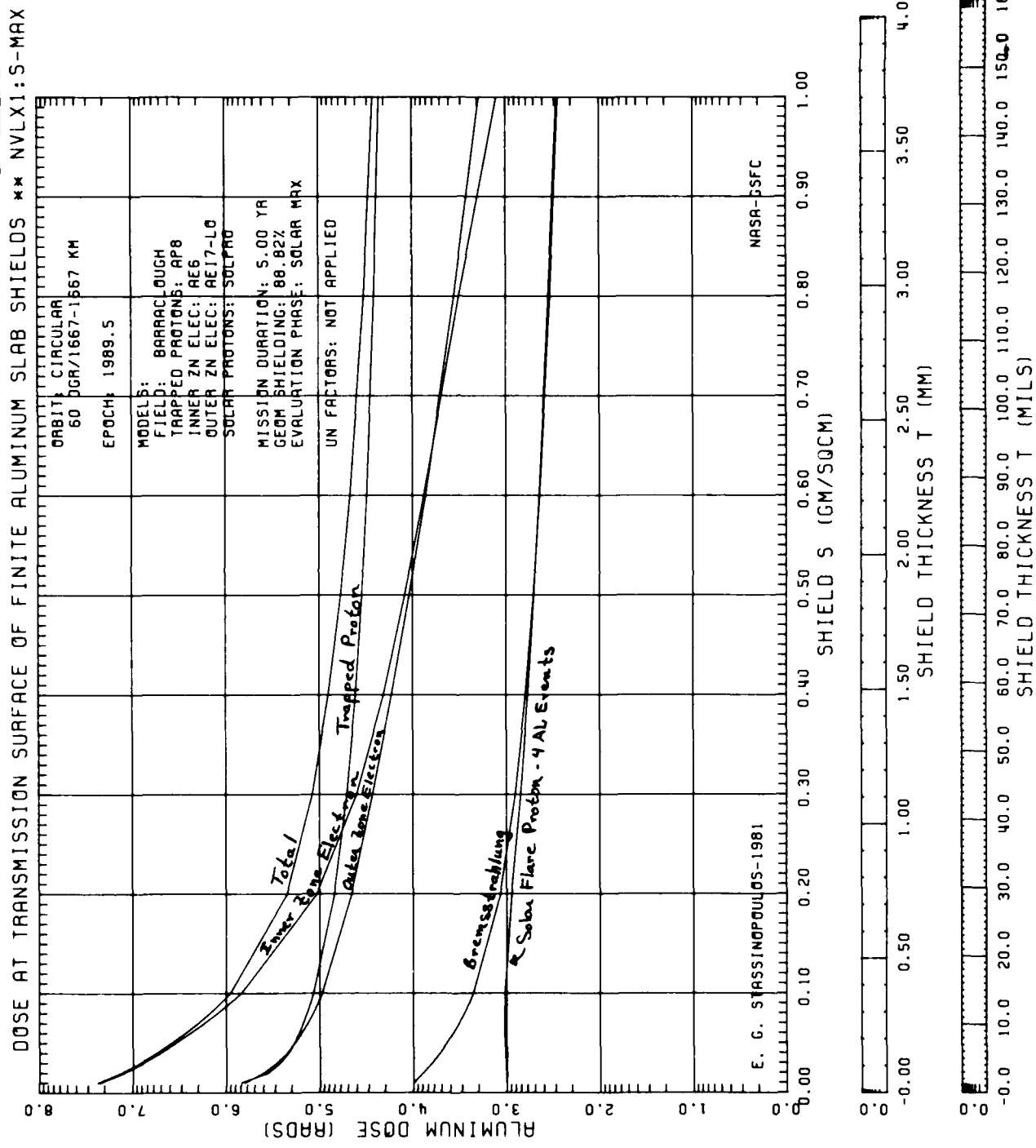


Figure 51

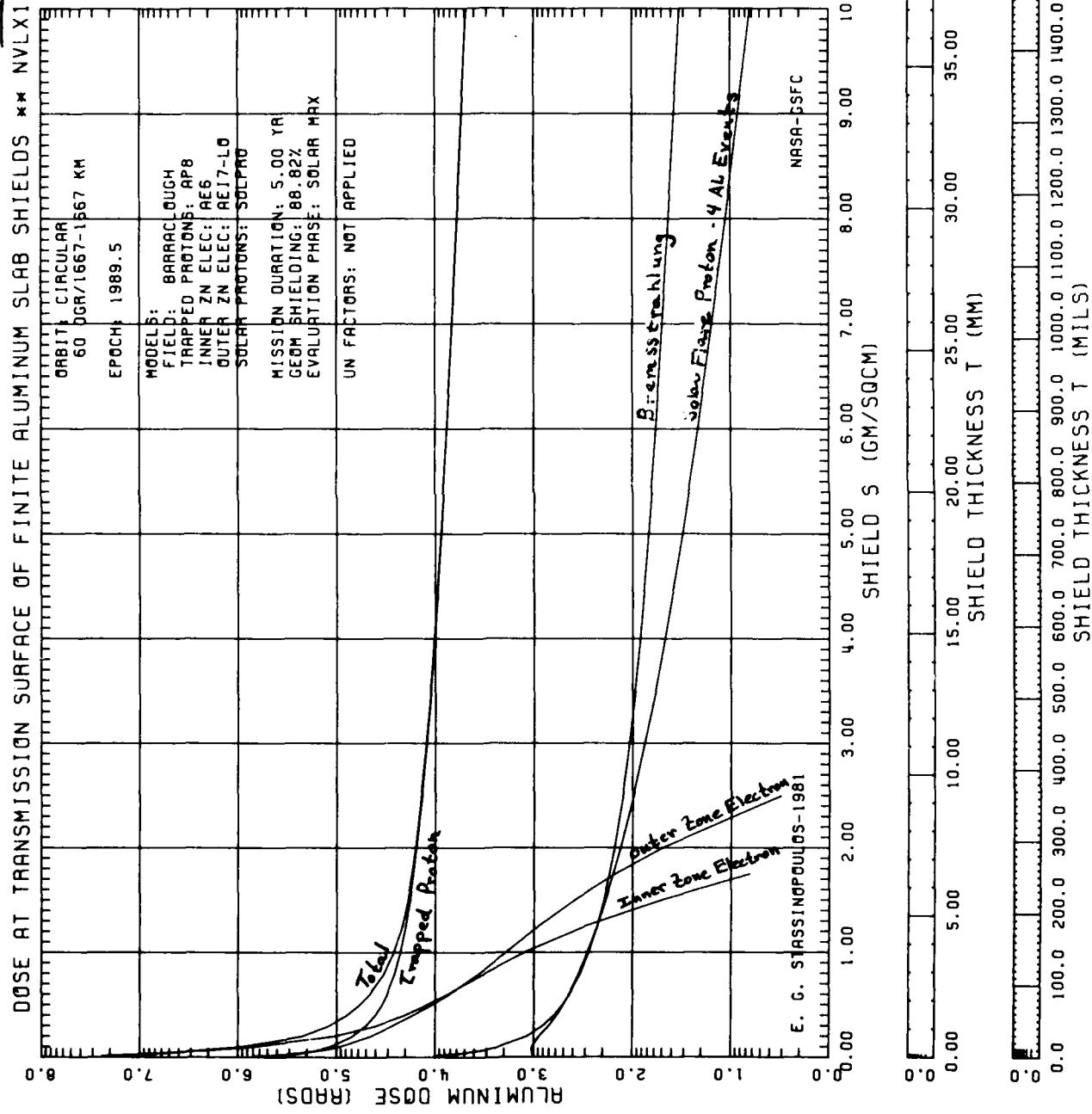


Figure 52

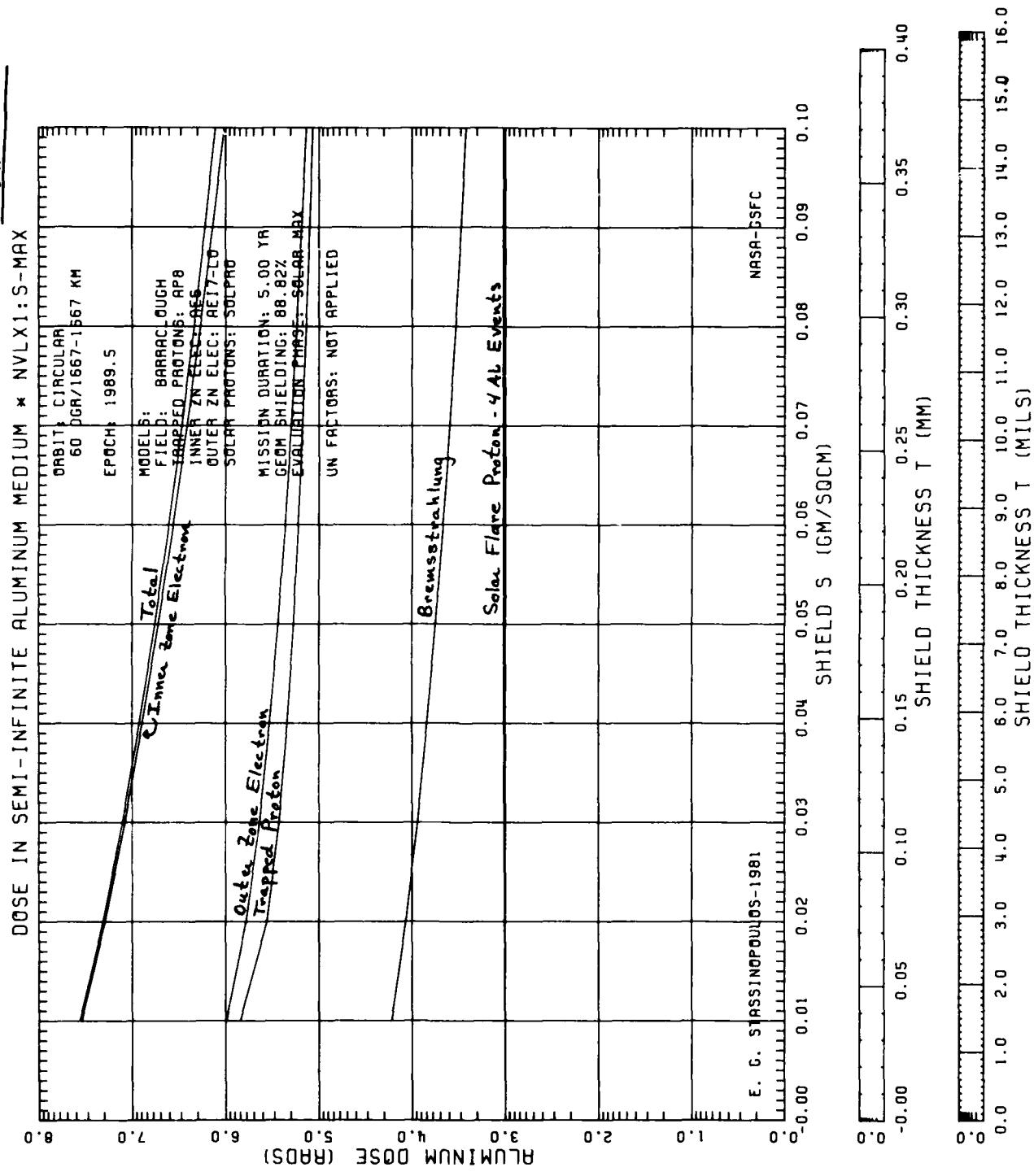


Figure 5.3

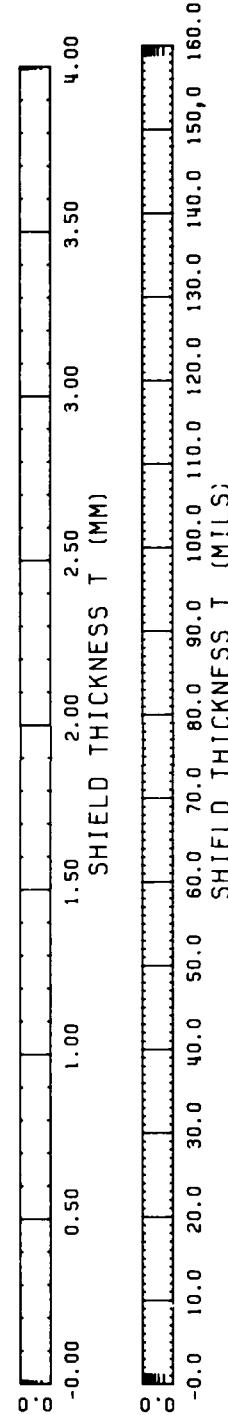
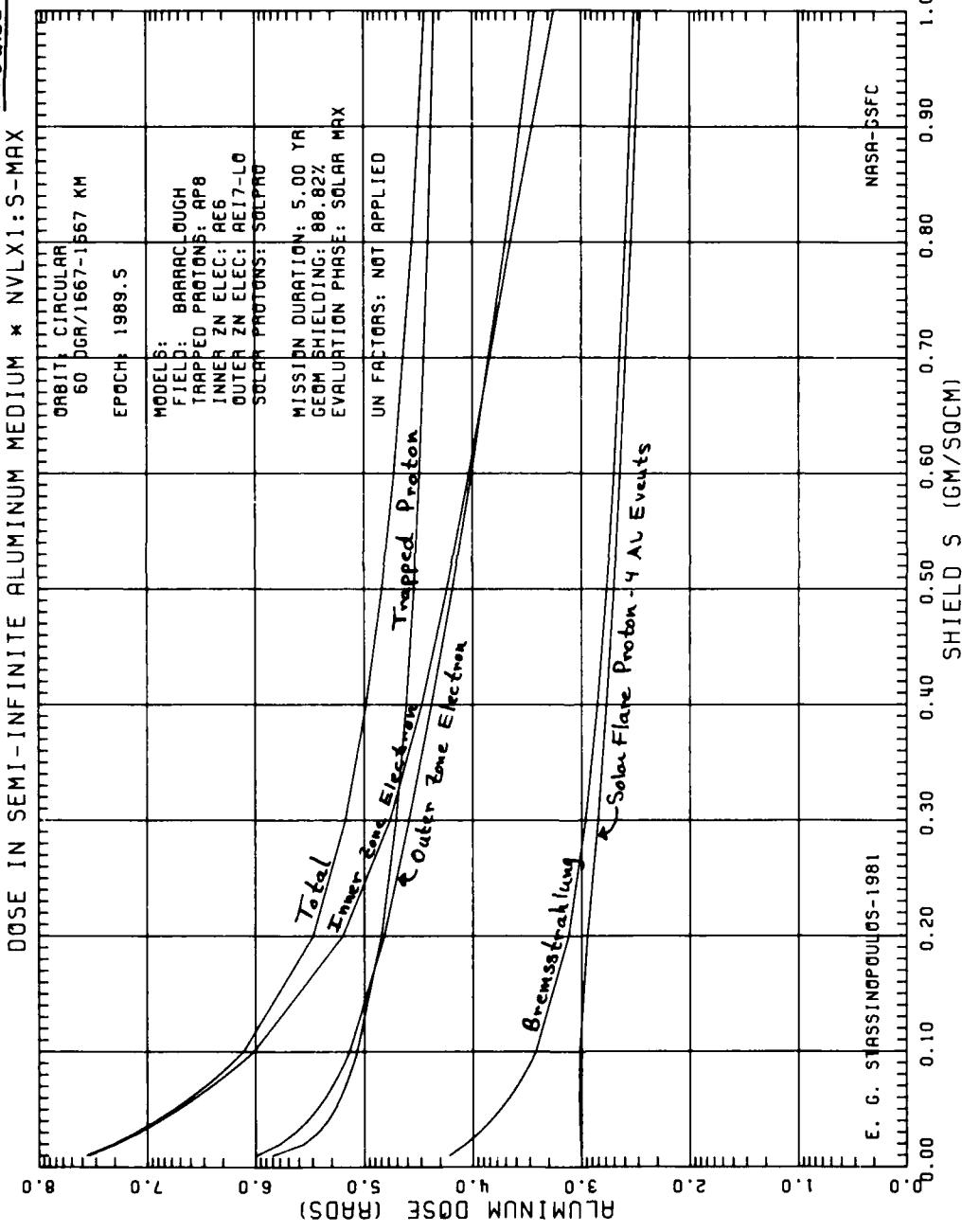


Figure 54

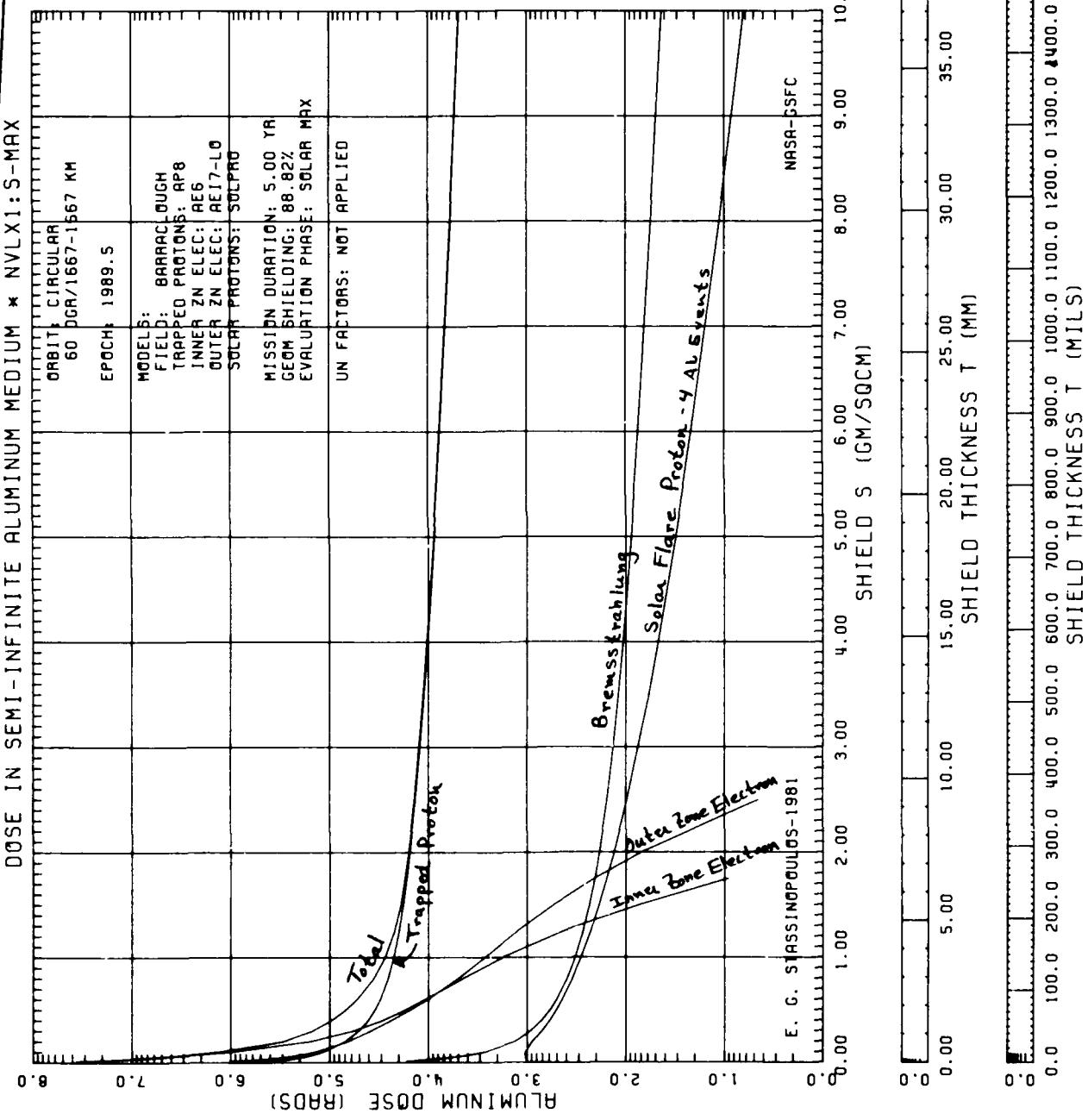
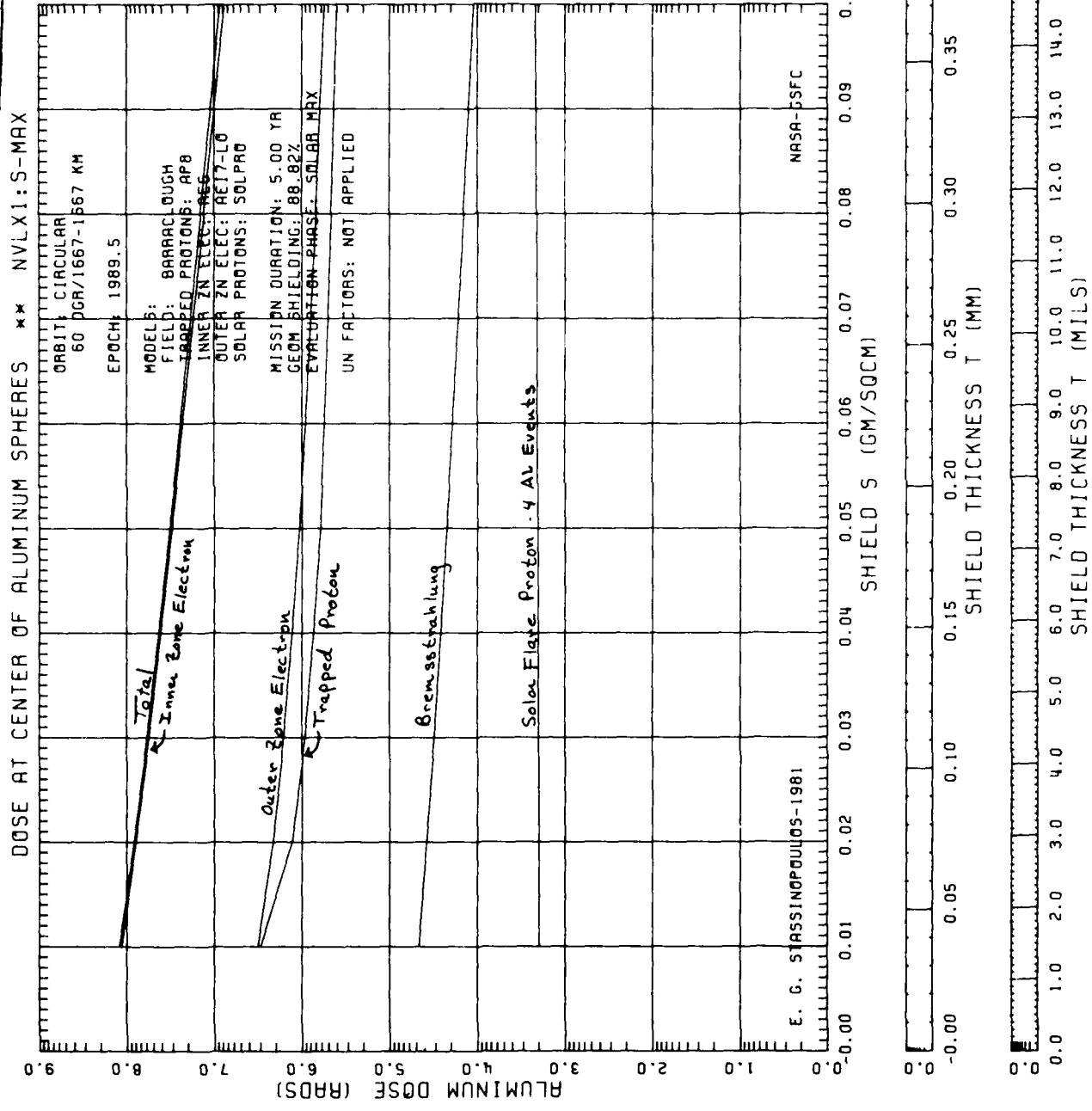


Figure 55



DOSE AT CENTER OF ALUMINUM SPHERES ** NVLX1: S-MAX

Figure 56

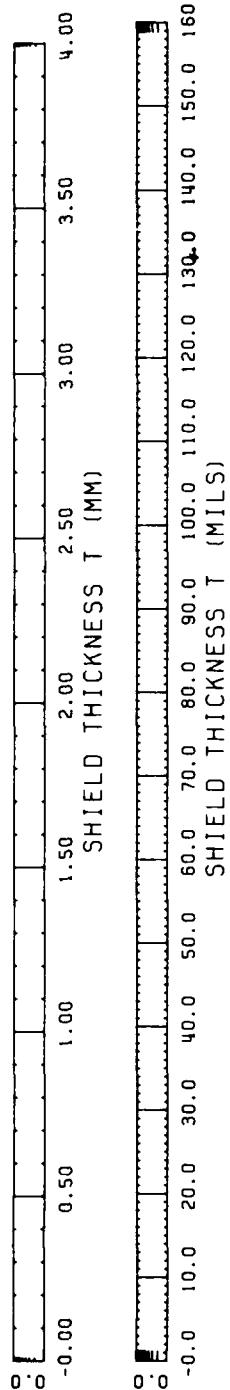
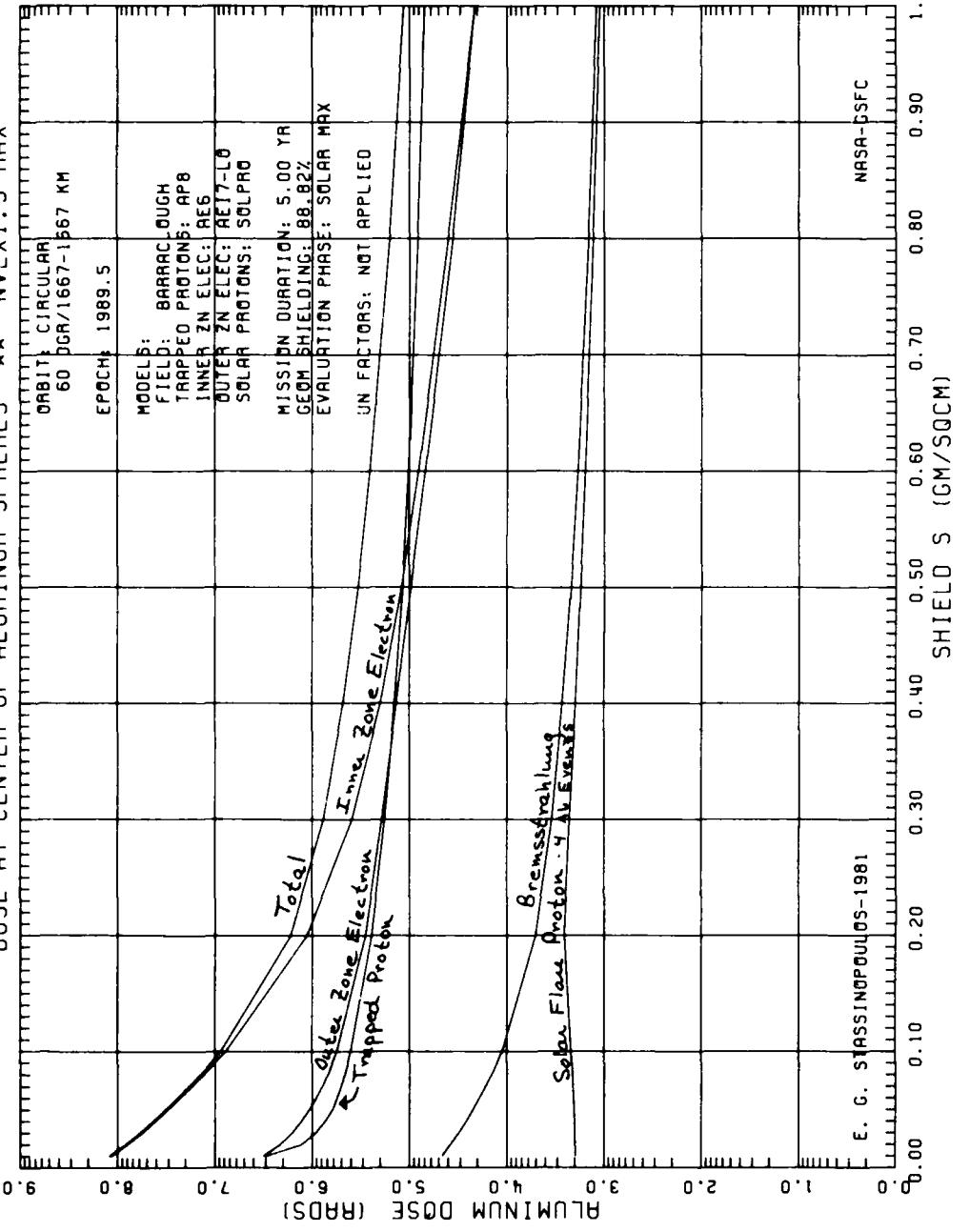


Figure 57

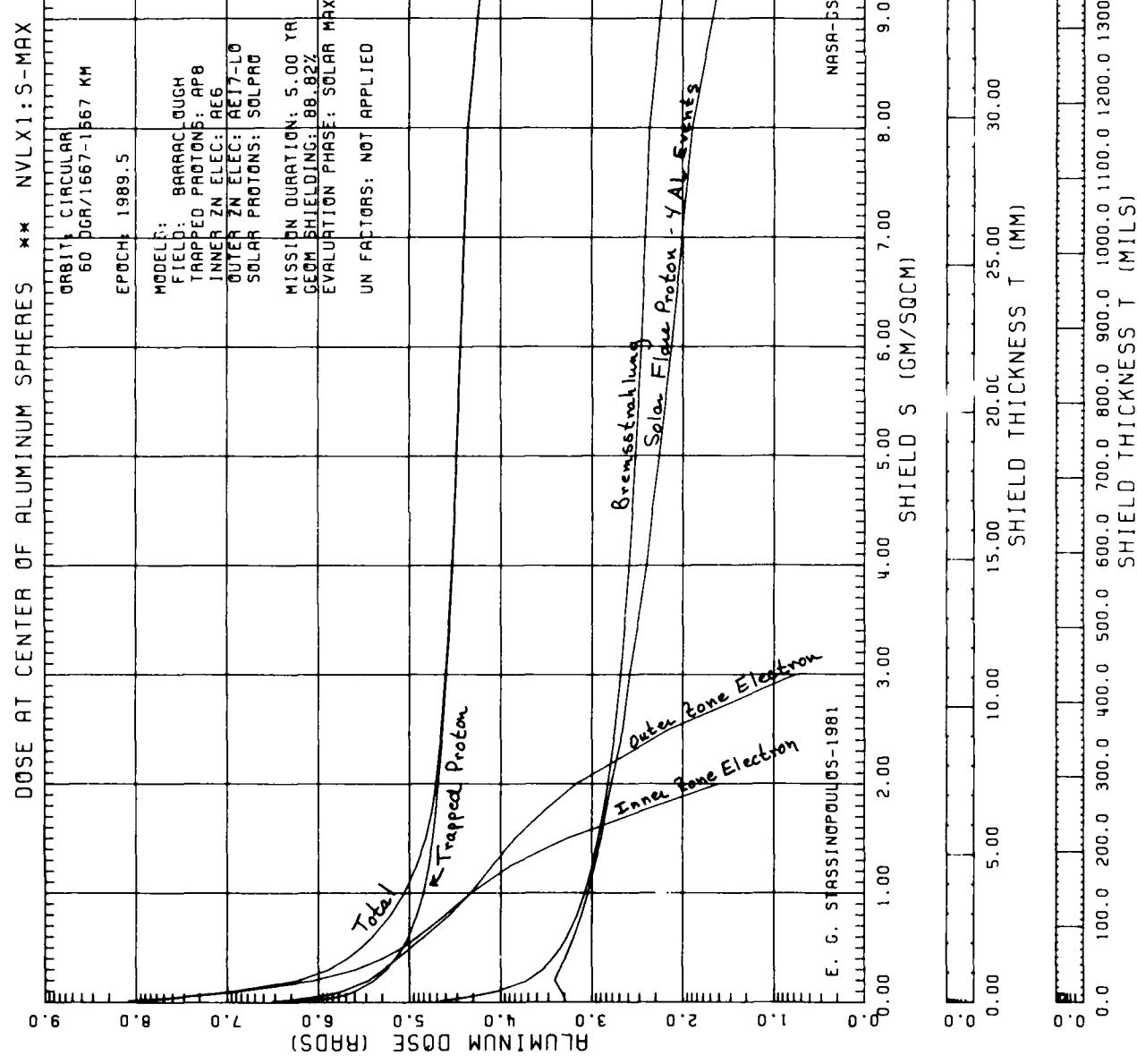
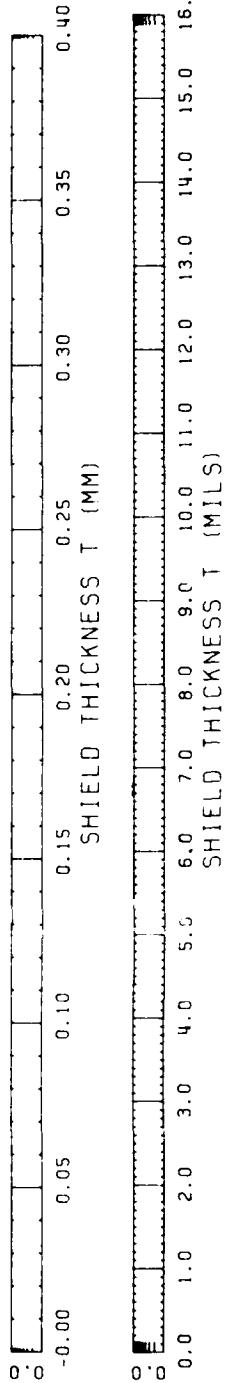
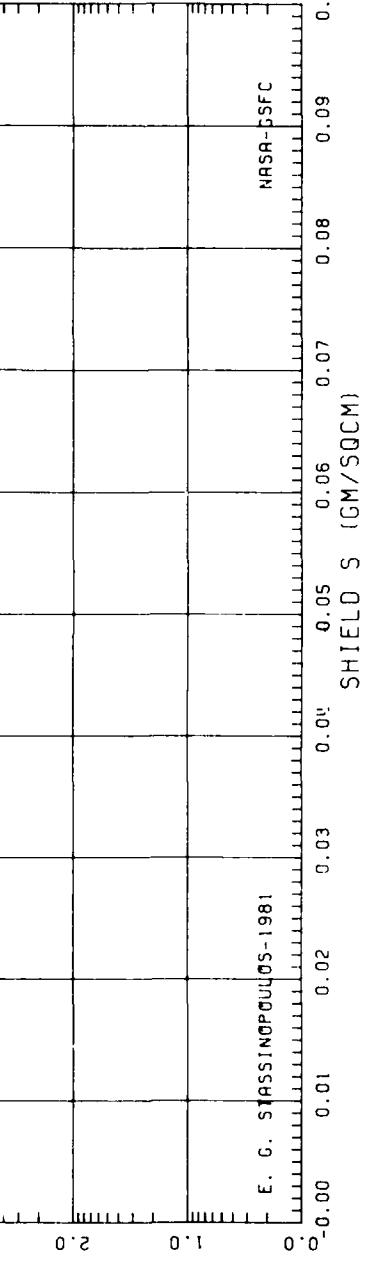
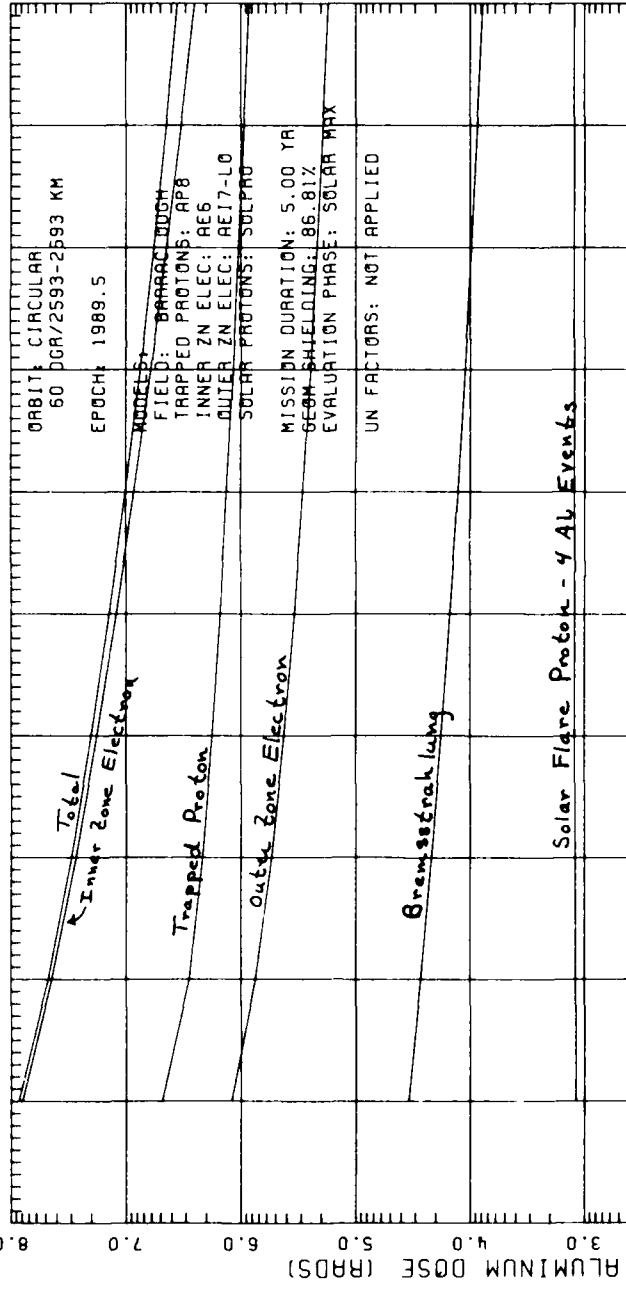


Figure 58

DOSE AT TRANSMISSION SURFACE OF FINITE ALUMINUM SLAB SHIELDS ** NVLX2: S-MAX



NASA-GSFC

MISSION DURATION: 5.00 YR

GEN SHIELDING: 86.81%

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Solar Flare Proton - 4 Al Events

Bremssstrahlung

AE6

AE17-LO

SOLPRO

AF8

AE6

AE17-LO

SOLPRO

AE6

AE6

AE17-LO

</div

Figure 59

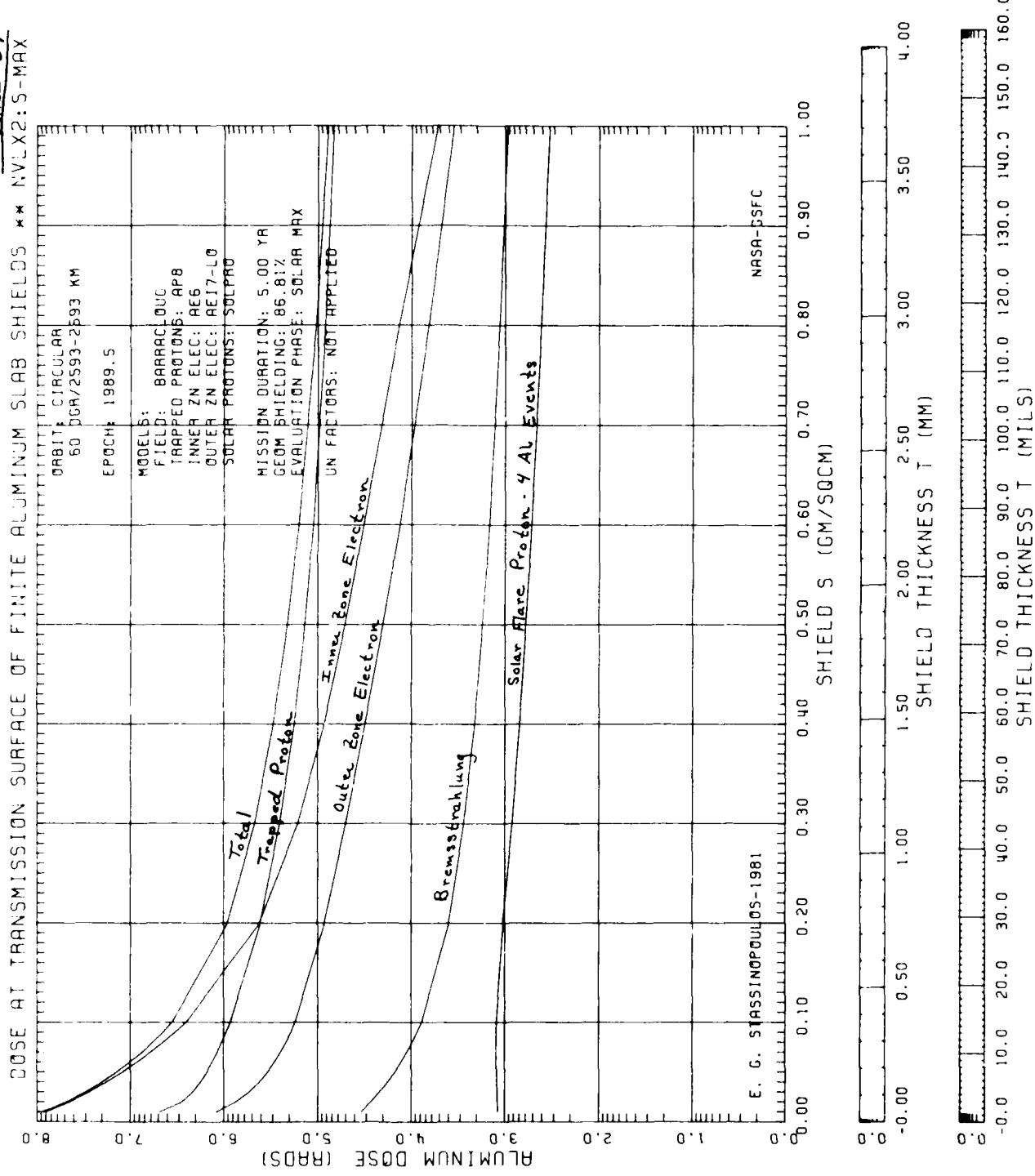


Figure 60

DOSE AT TRANSMISSION SURFACE OF FINITE ALUMINUM SLAB SHIELDS ** NVLX2: S-MAX

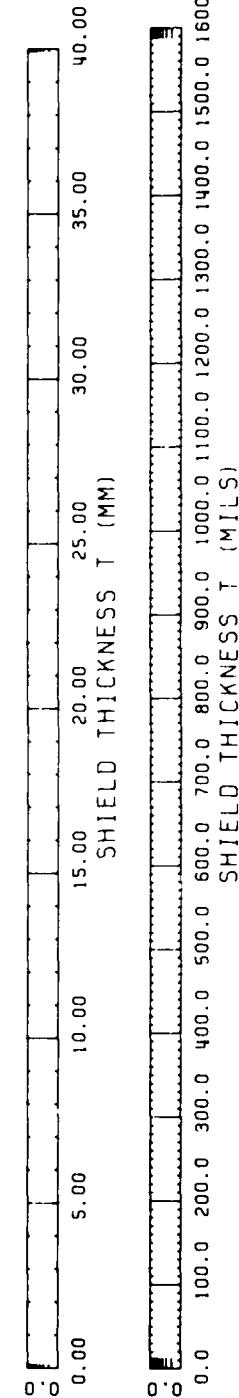
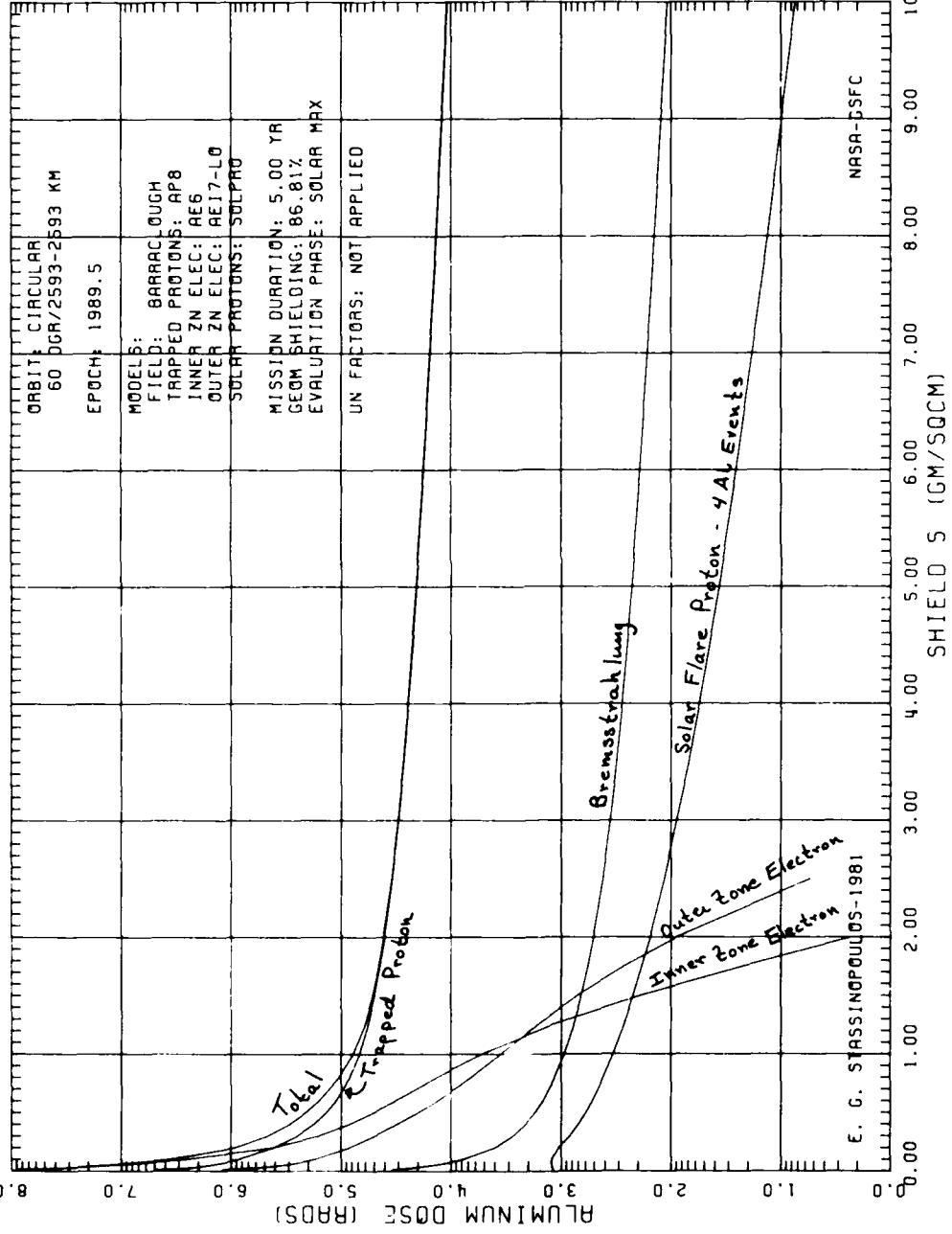


Figure 61

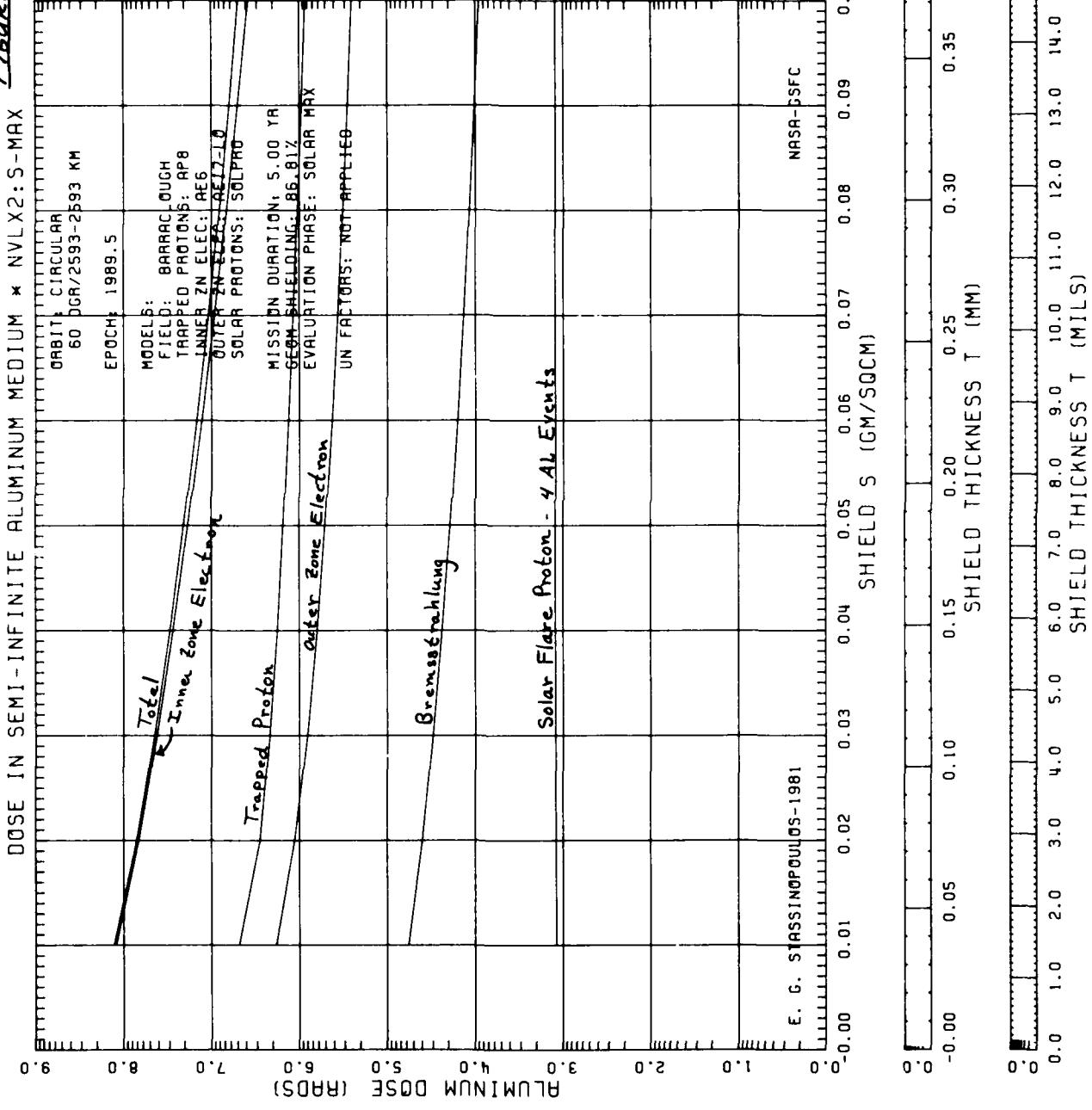


FIGURE 62

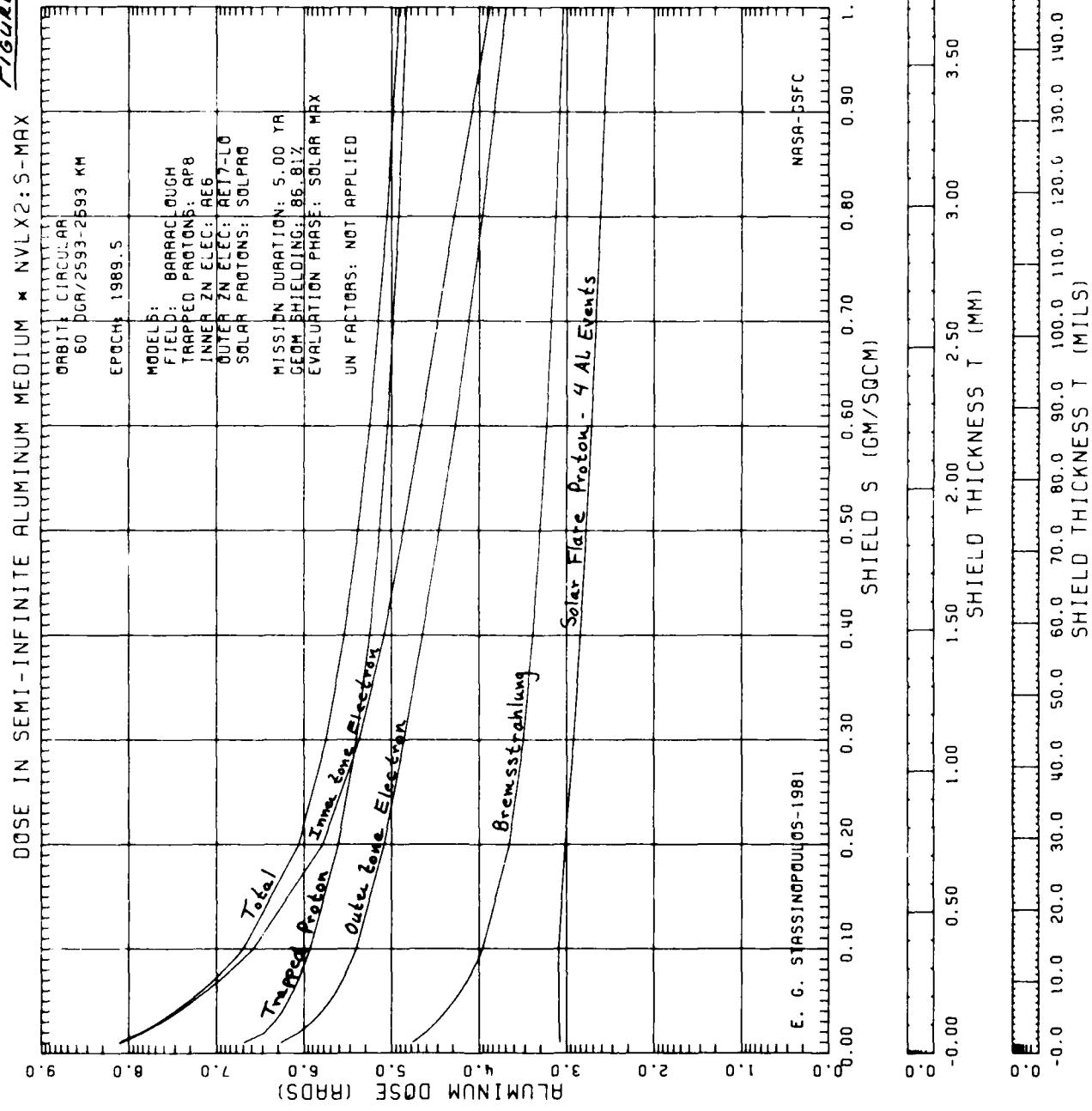


Figure E.3

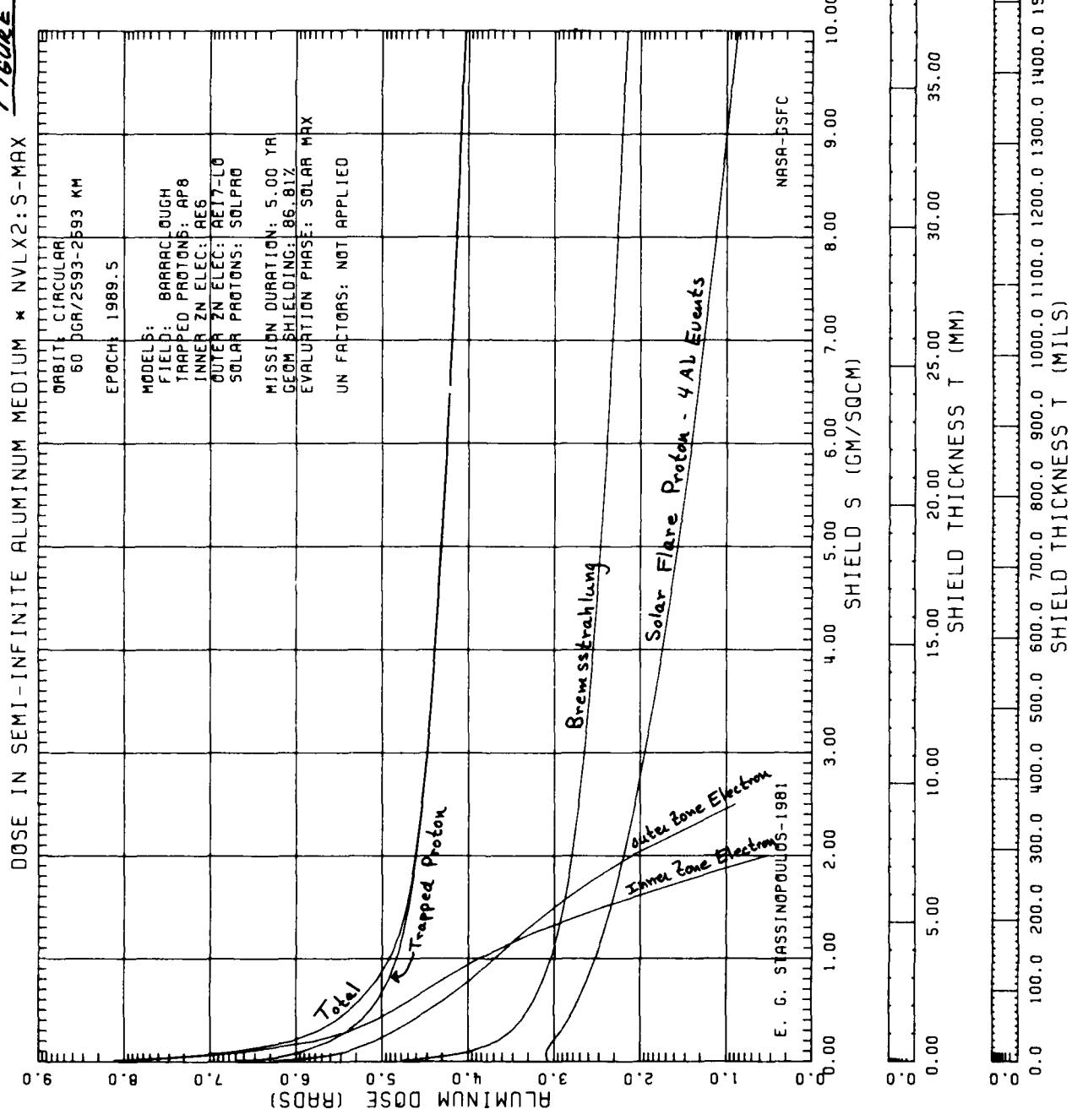


FIGURE 64

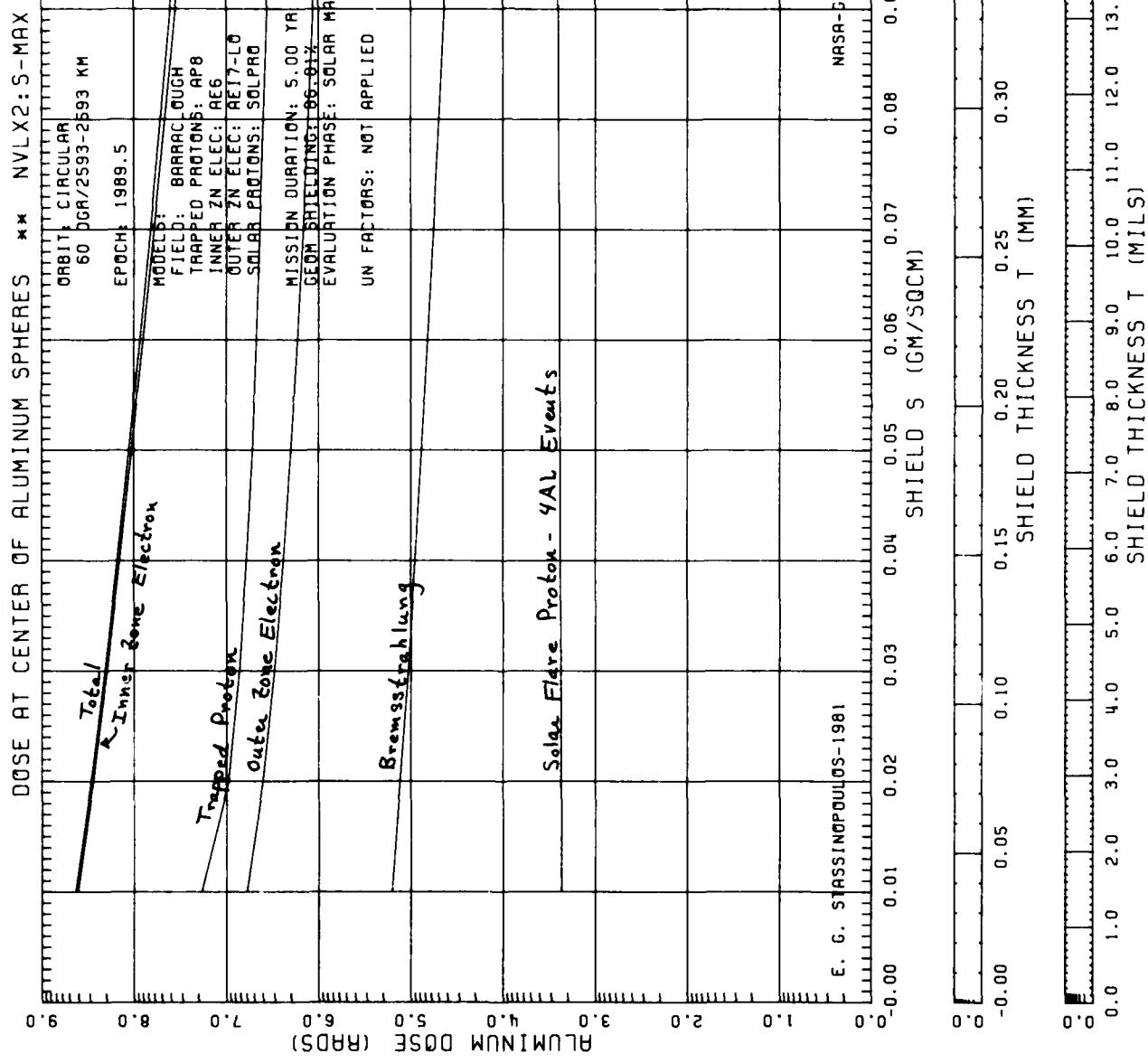


FIGURE 65

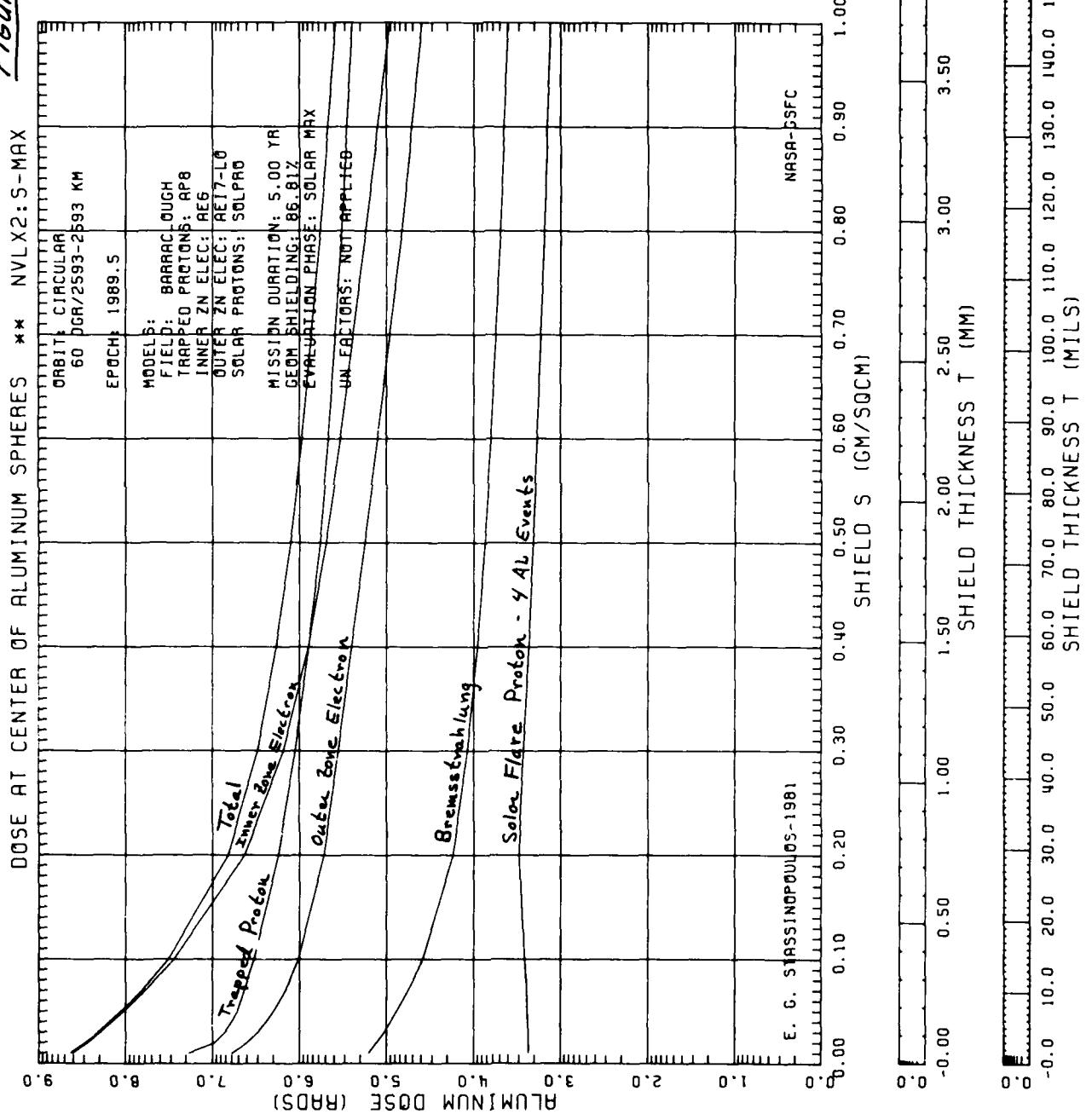


Figure 66

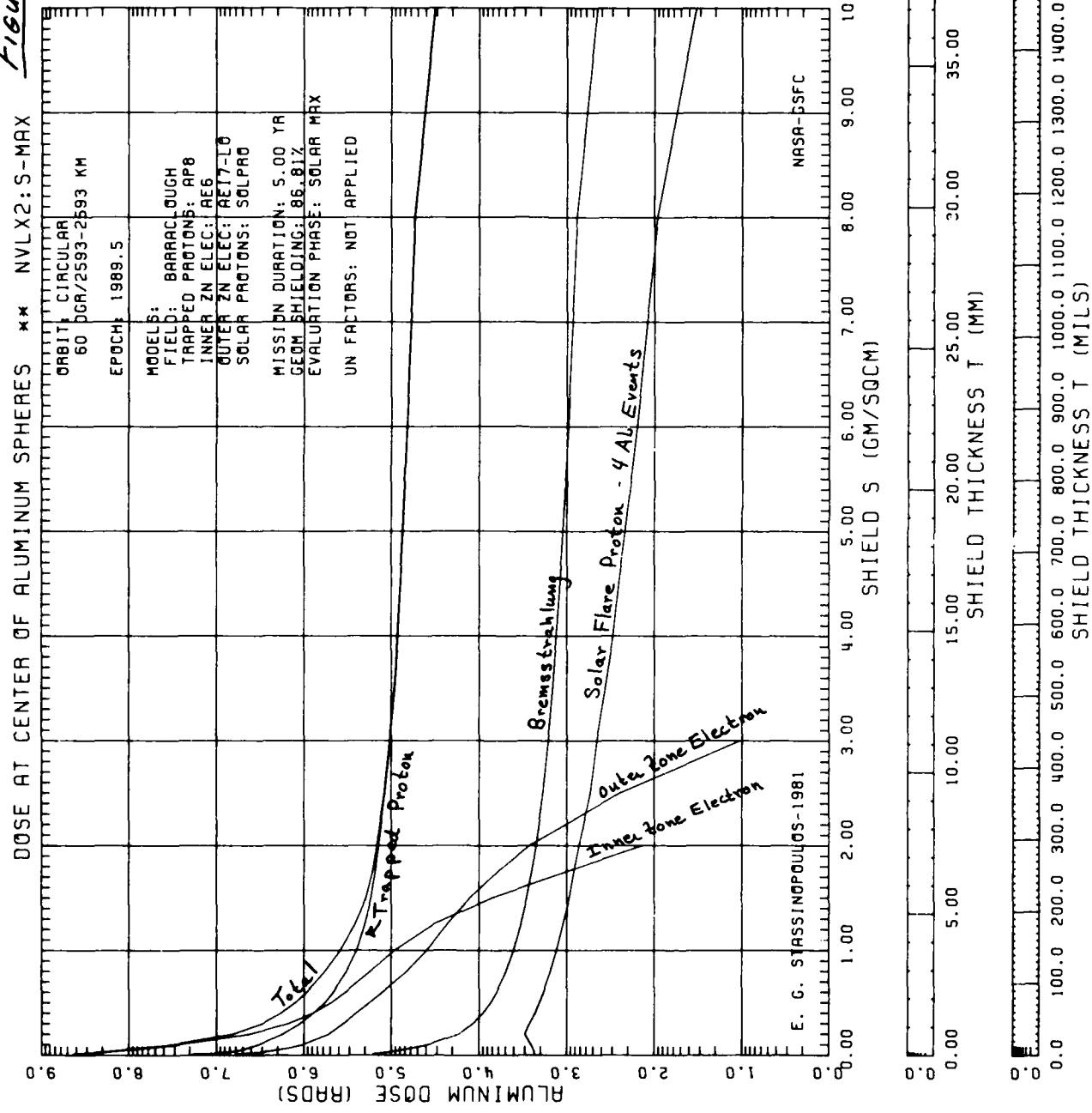


FIGURE 67

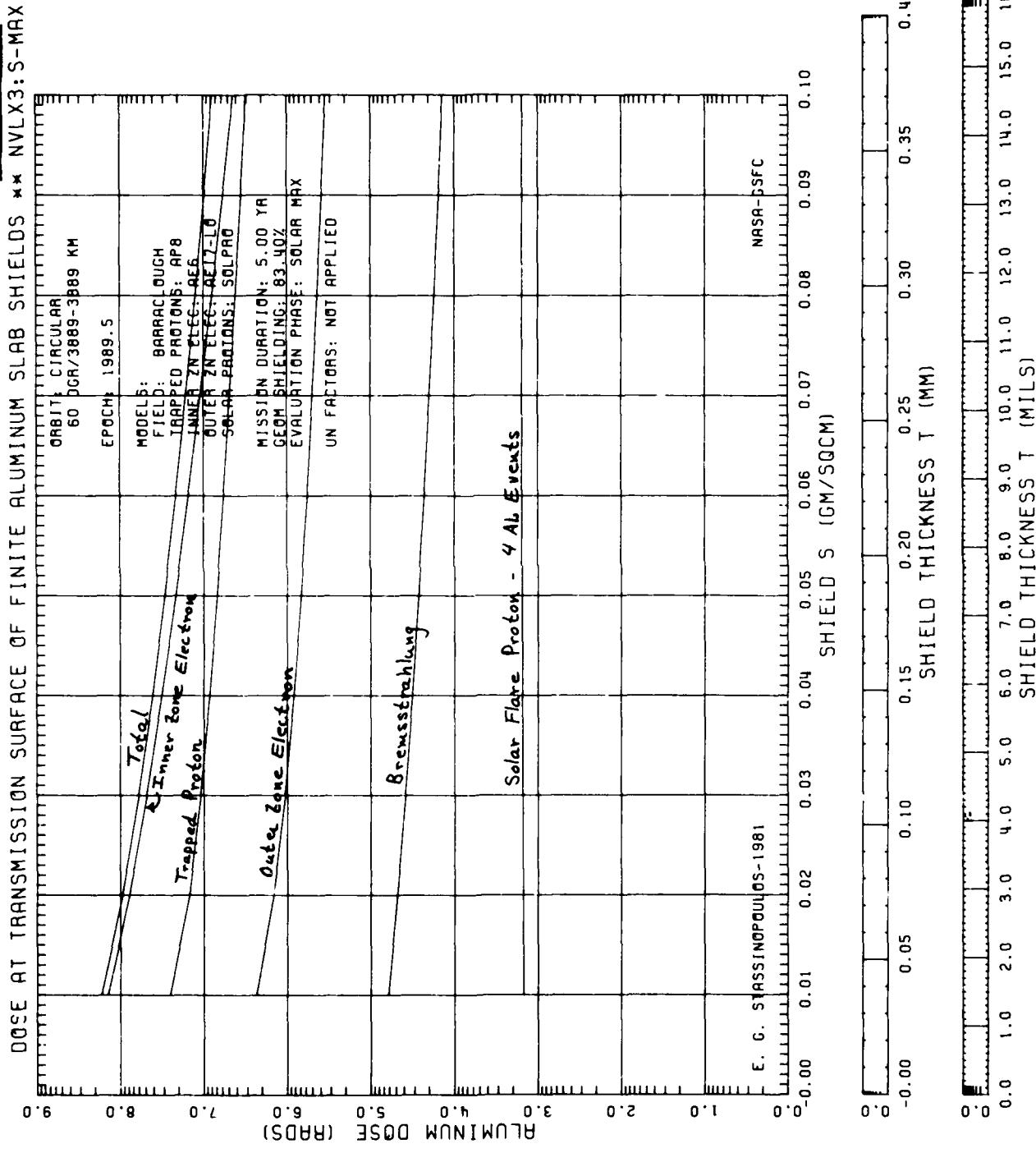


Figure 68

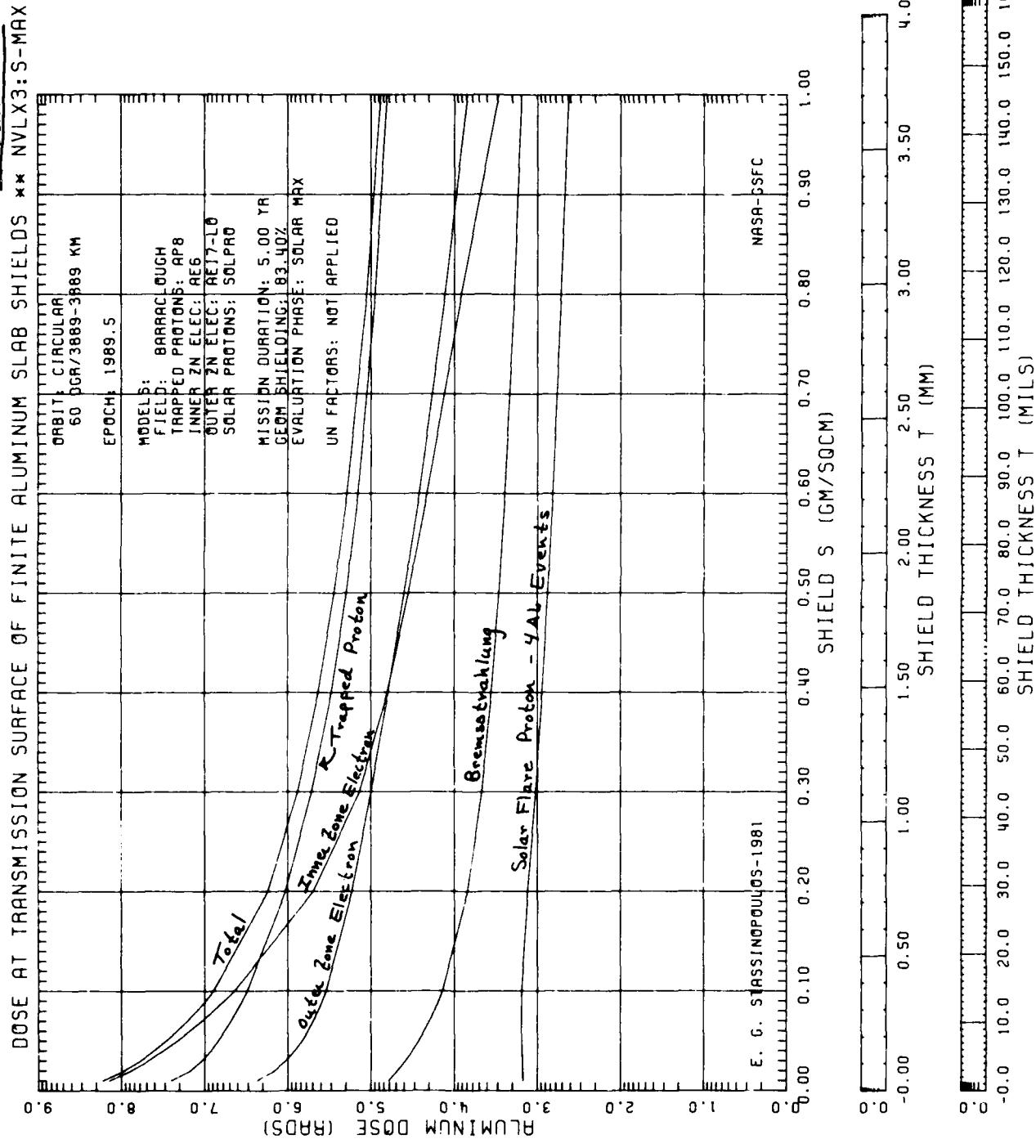


Figure 69

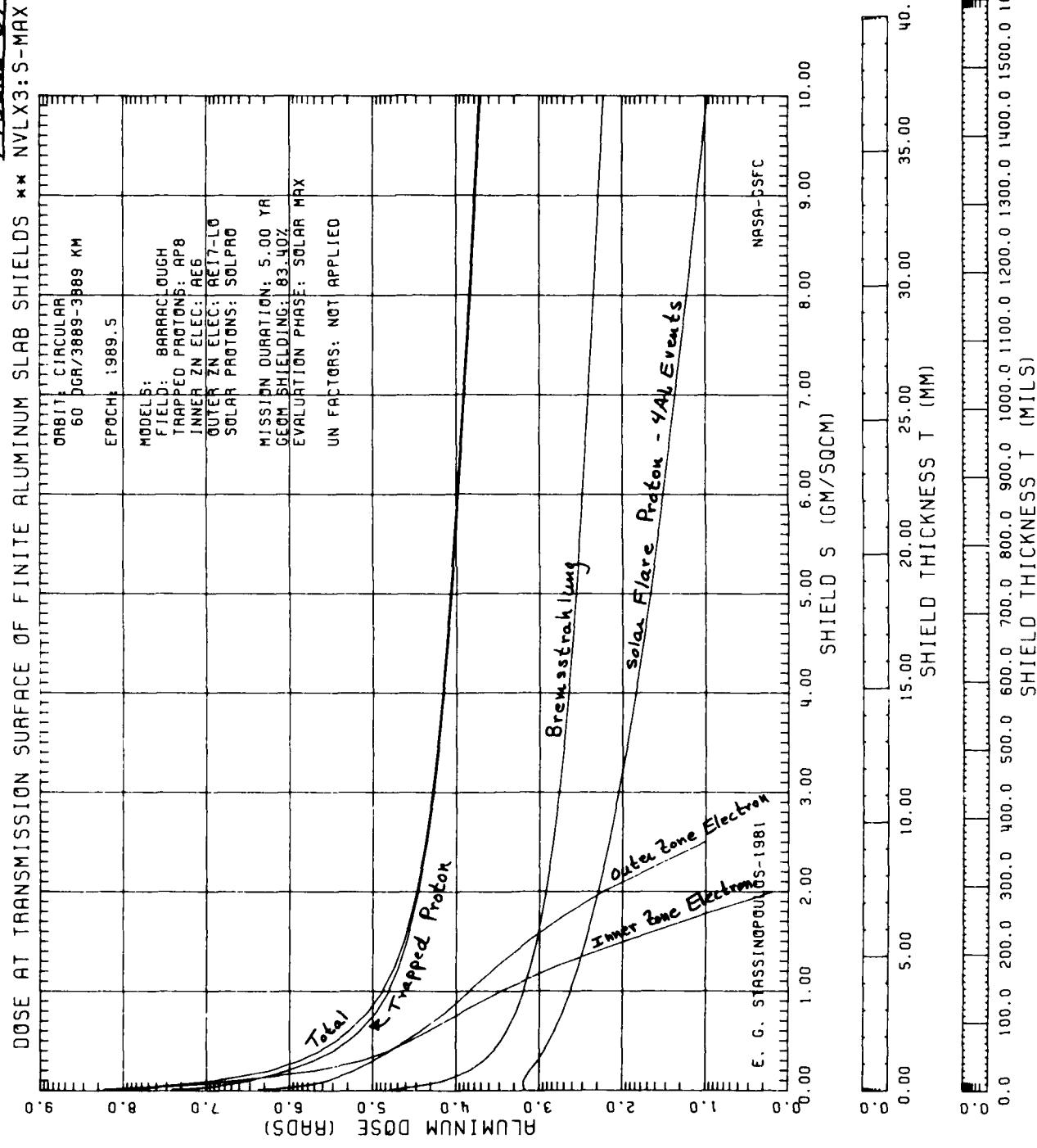


Figure 20

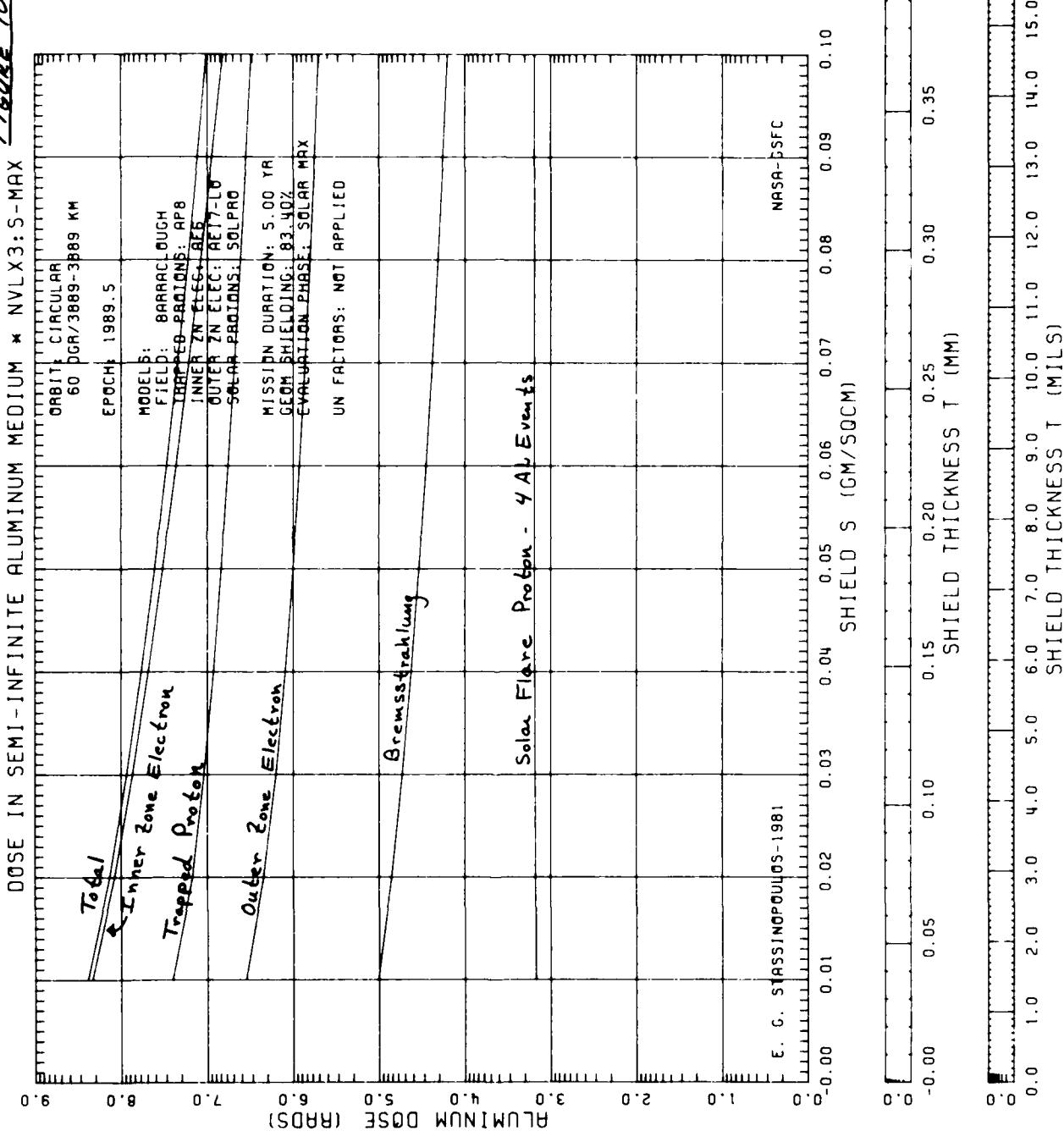


Figure 71

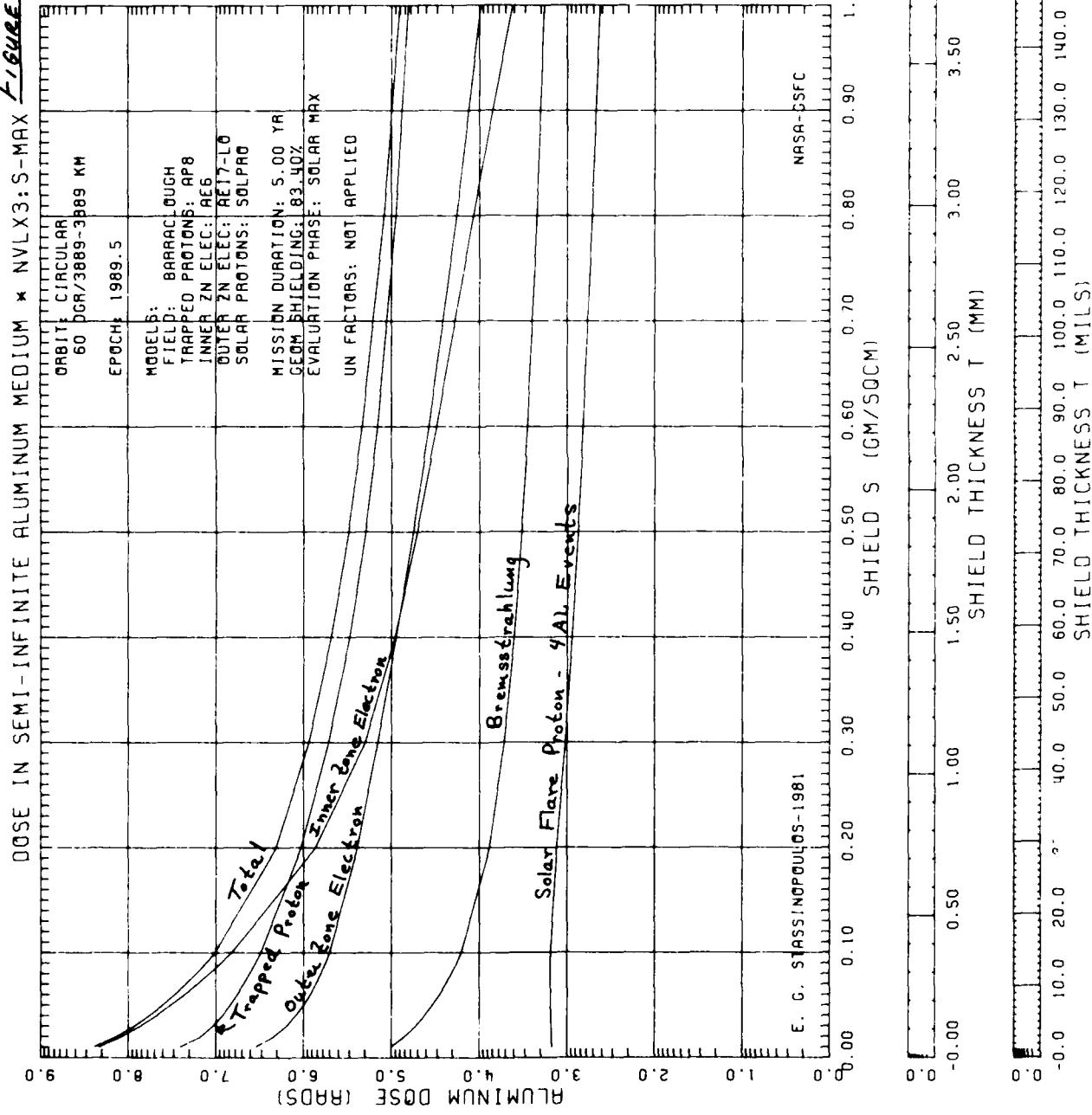
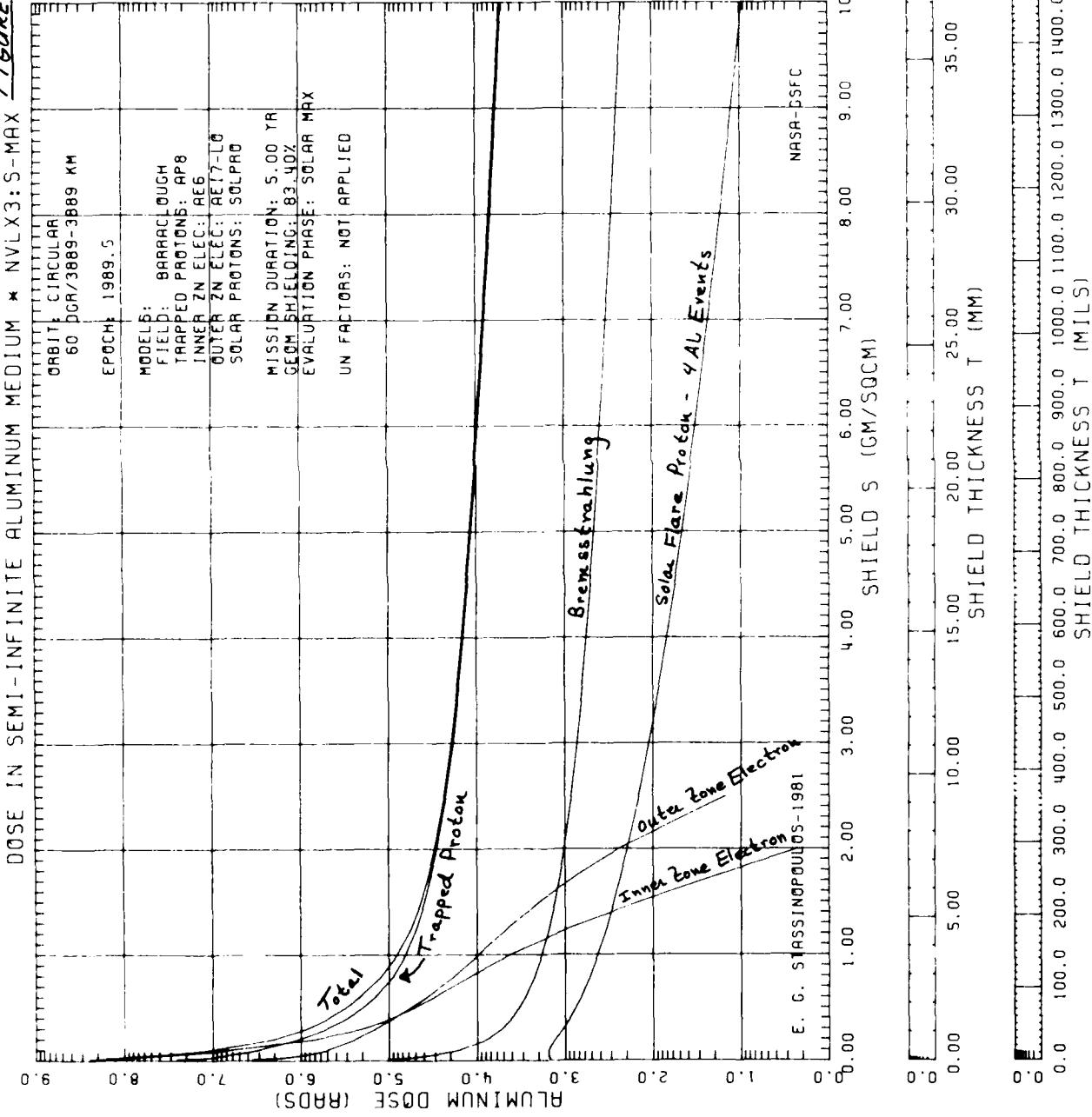


Figure 72



DOSAGE AT CENTER OF ALUMINUM SPHERES ** NVL X3: S-MAX

FIGURE 73

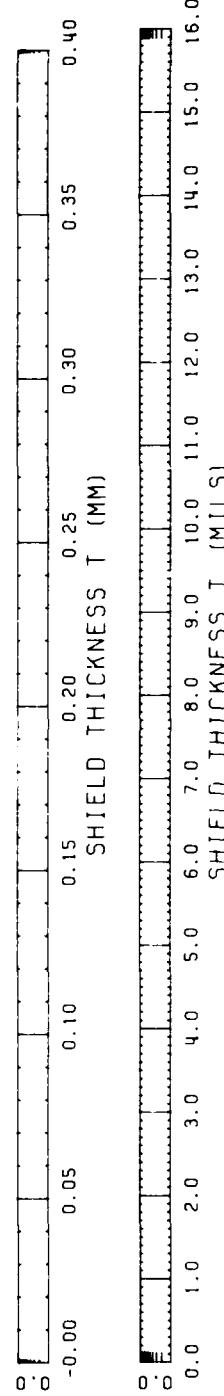
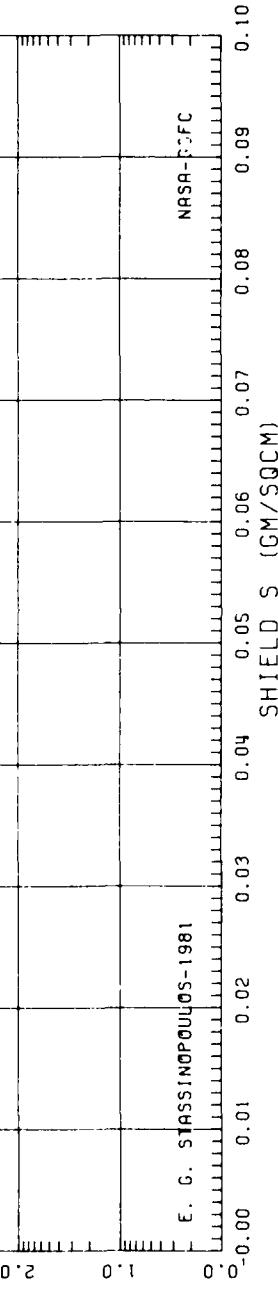
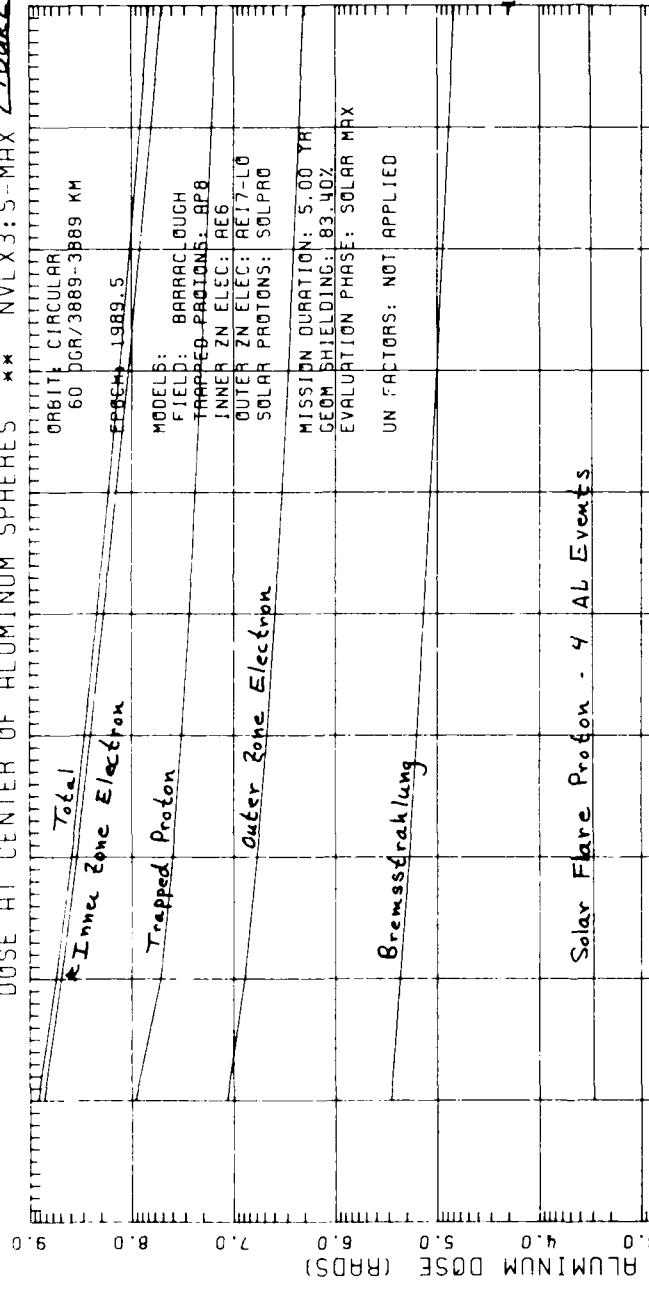


Figure 74

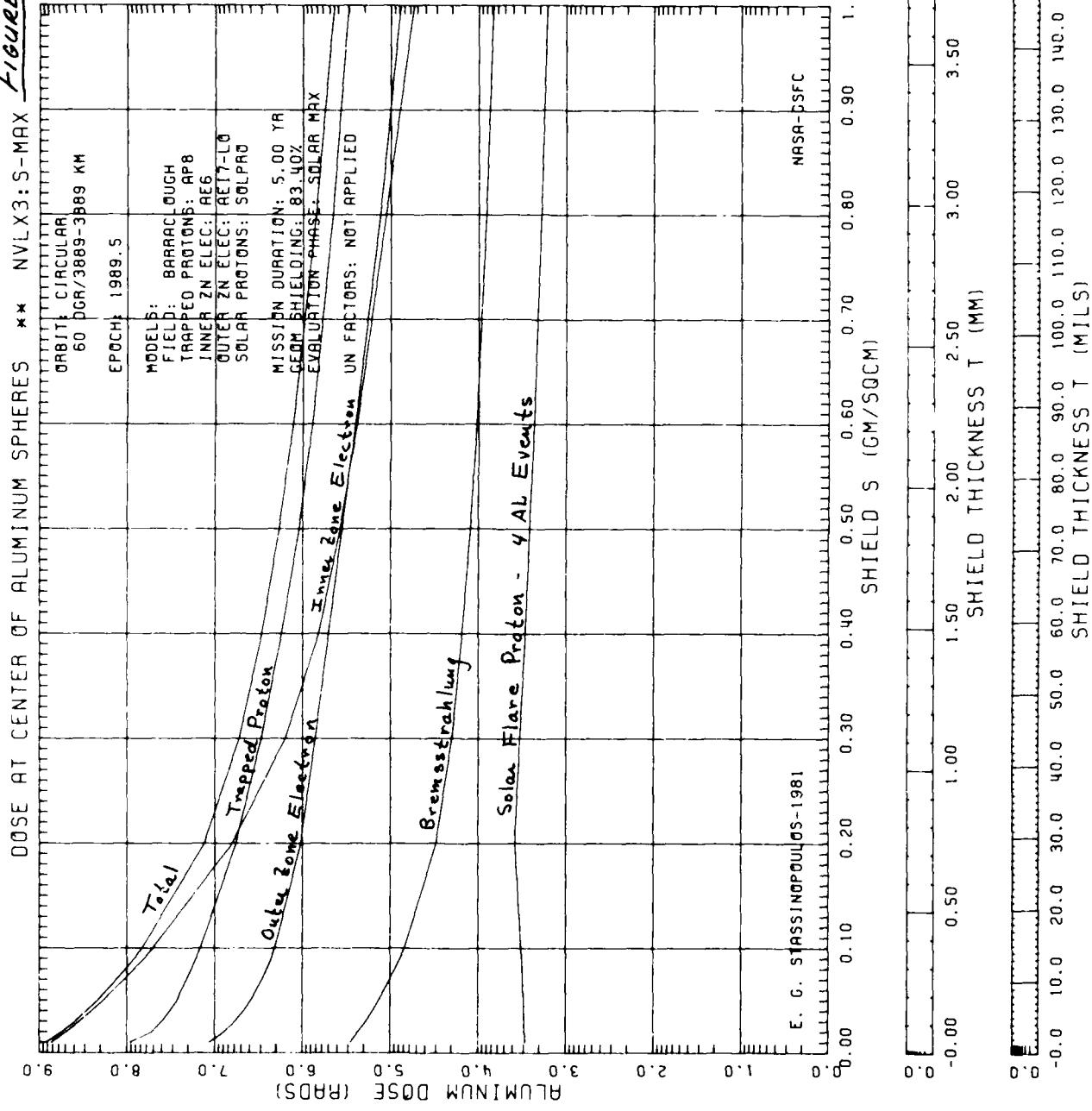


Figure 75

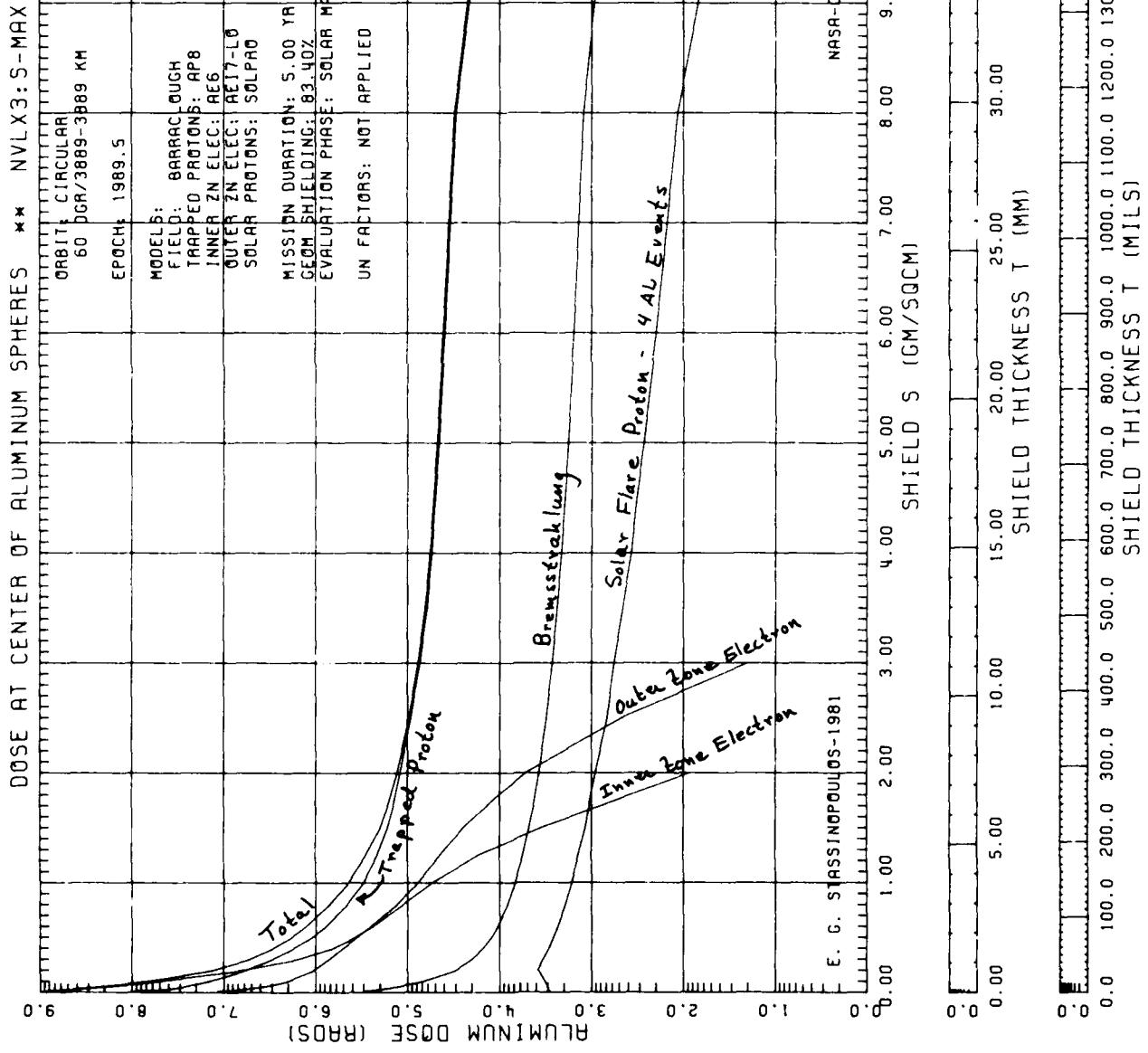


FIGURE 76

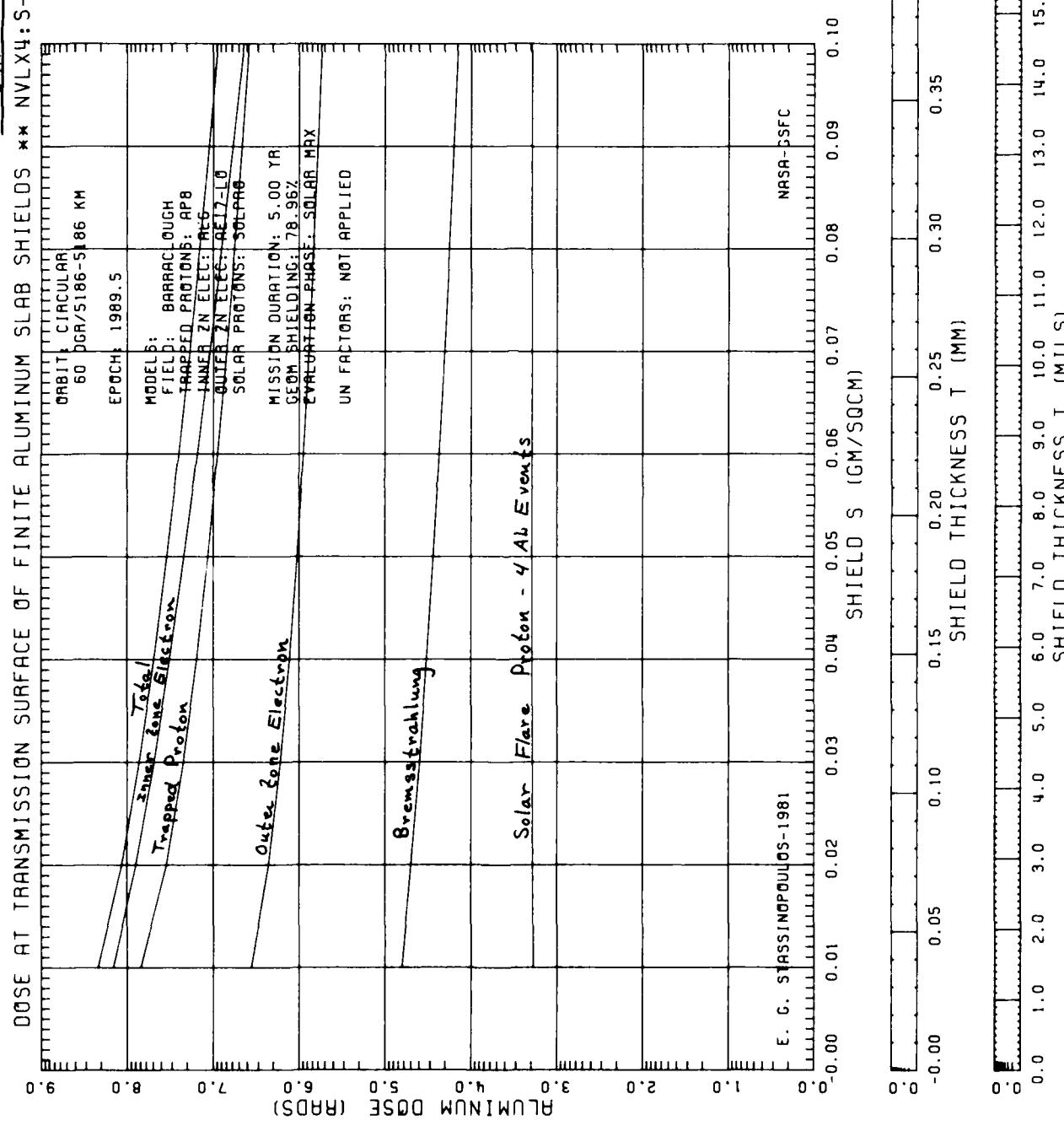


Figure 77

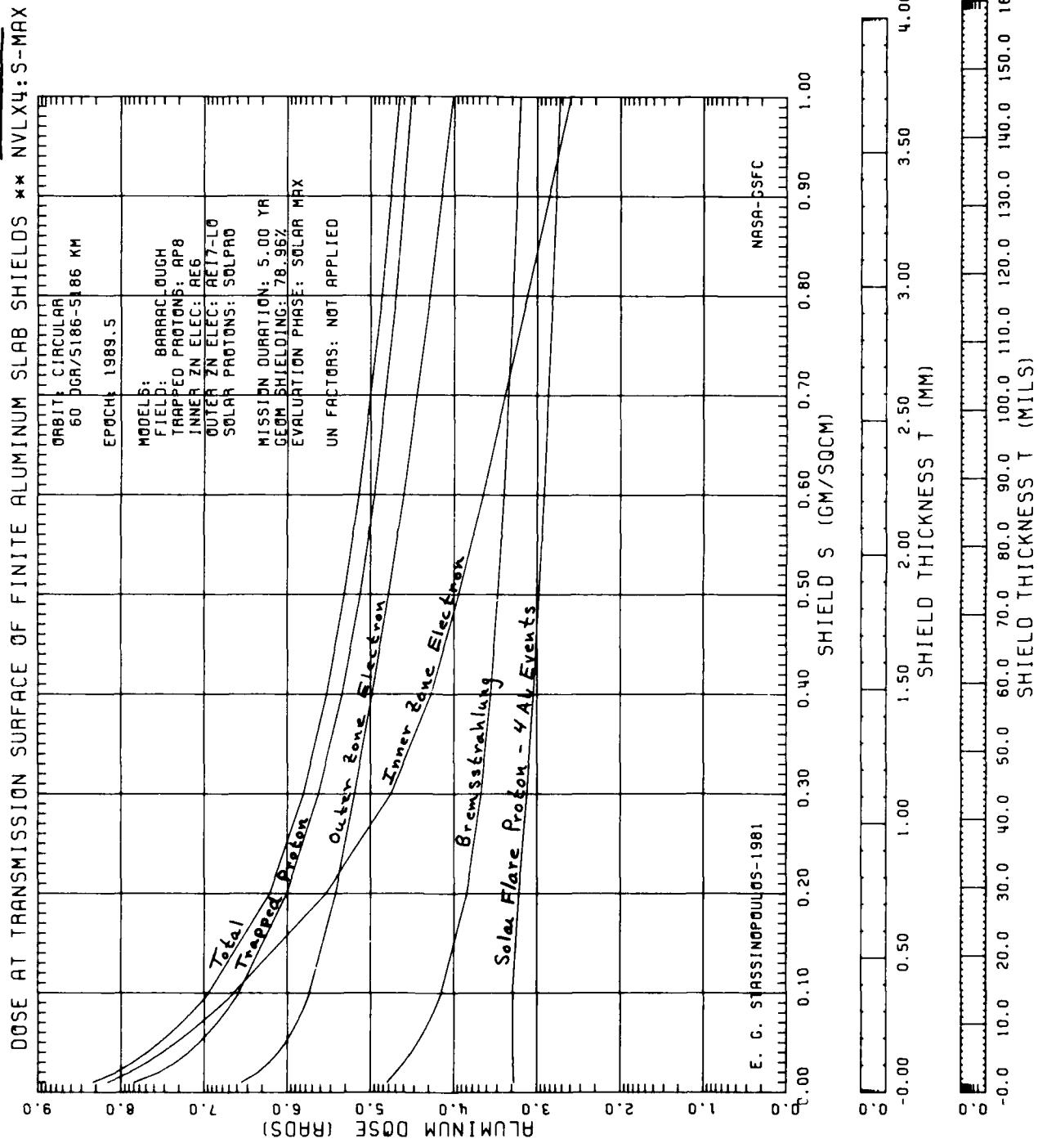


FIGURE 7B

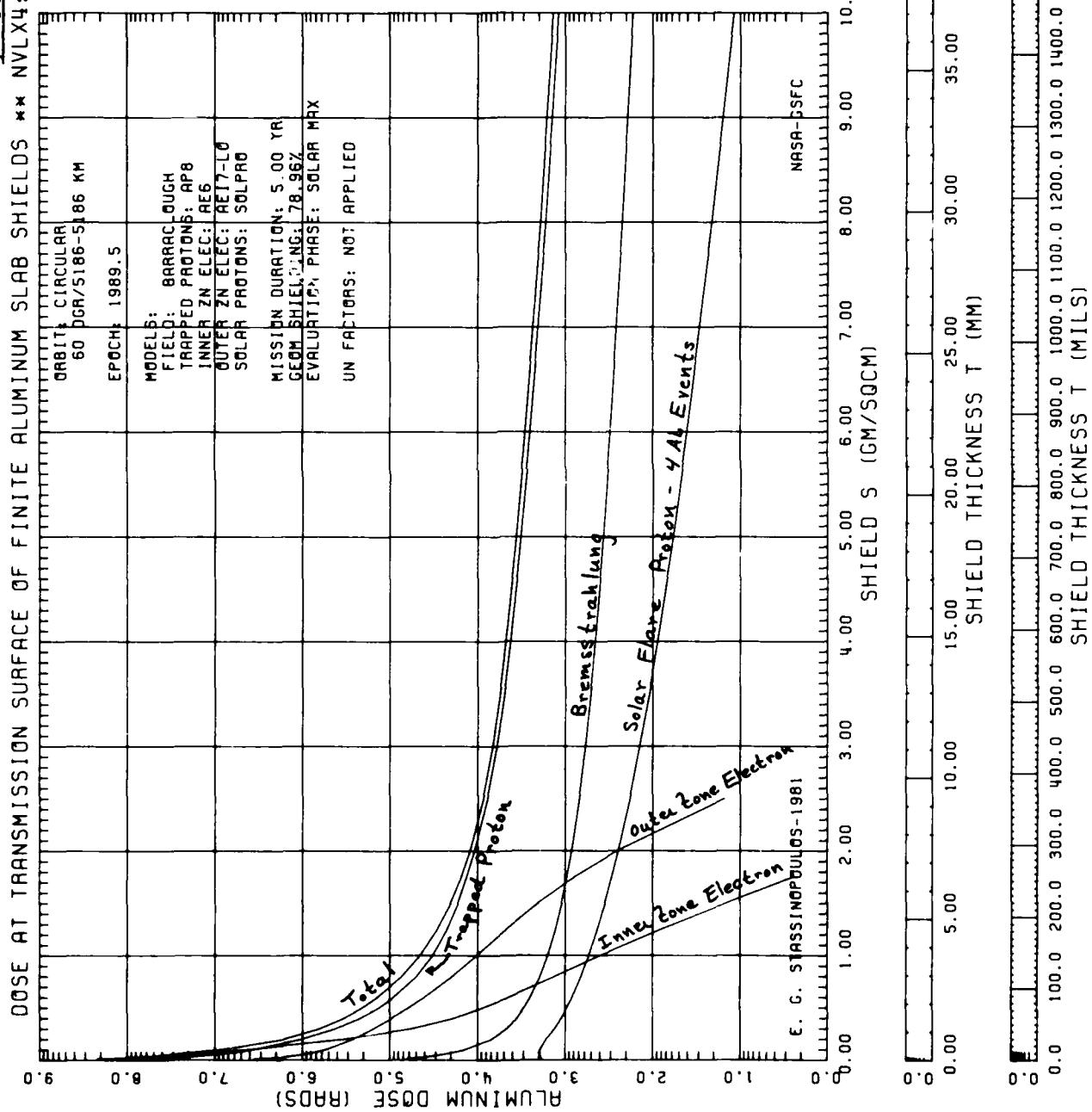


Figure 79

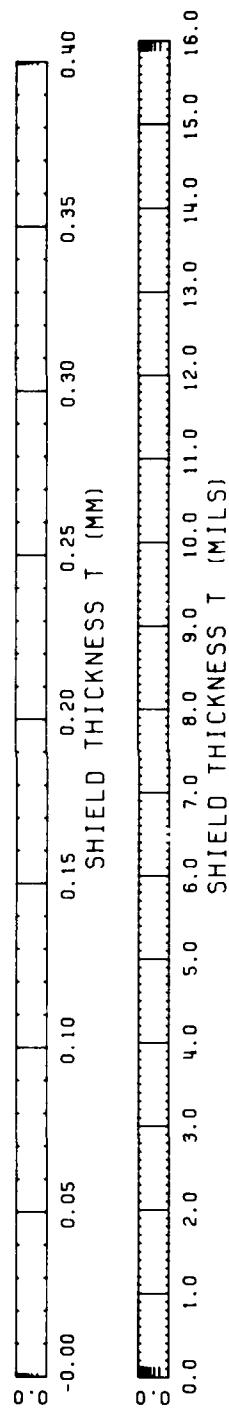
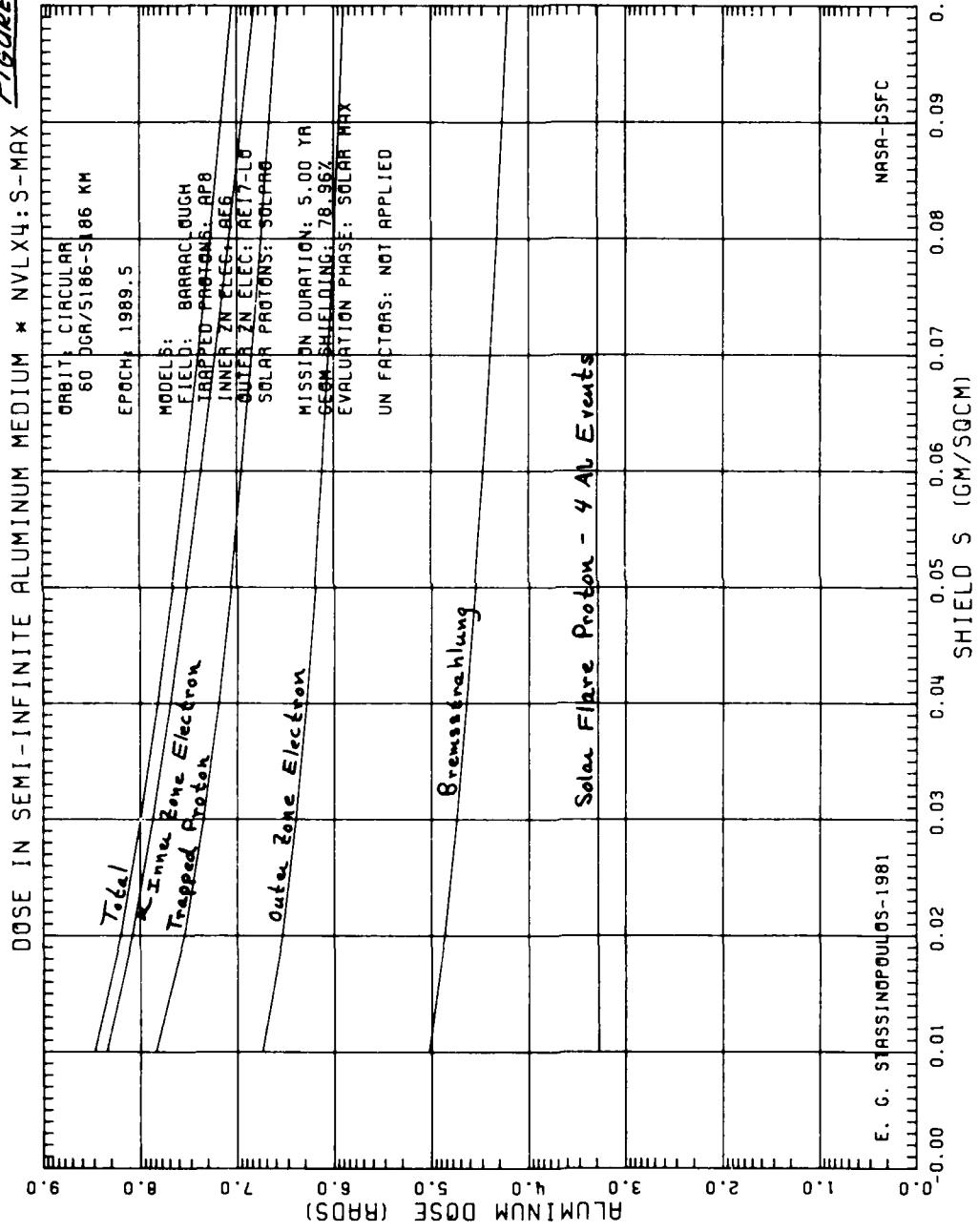


Figure 80

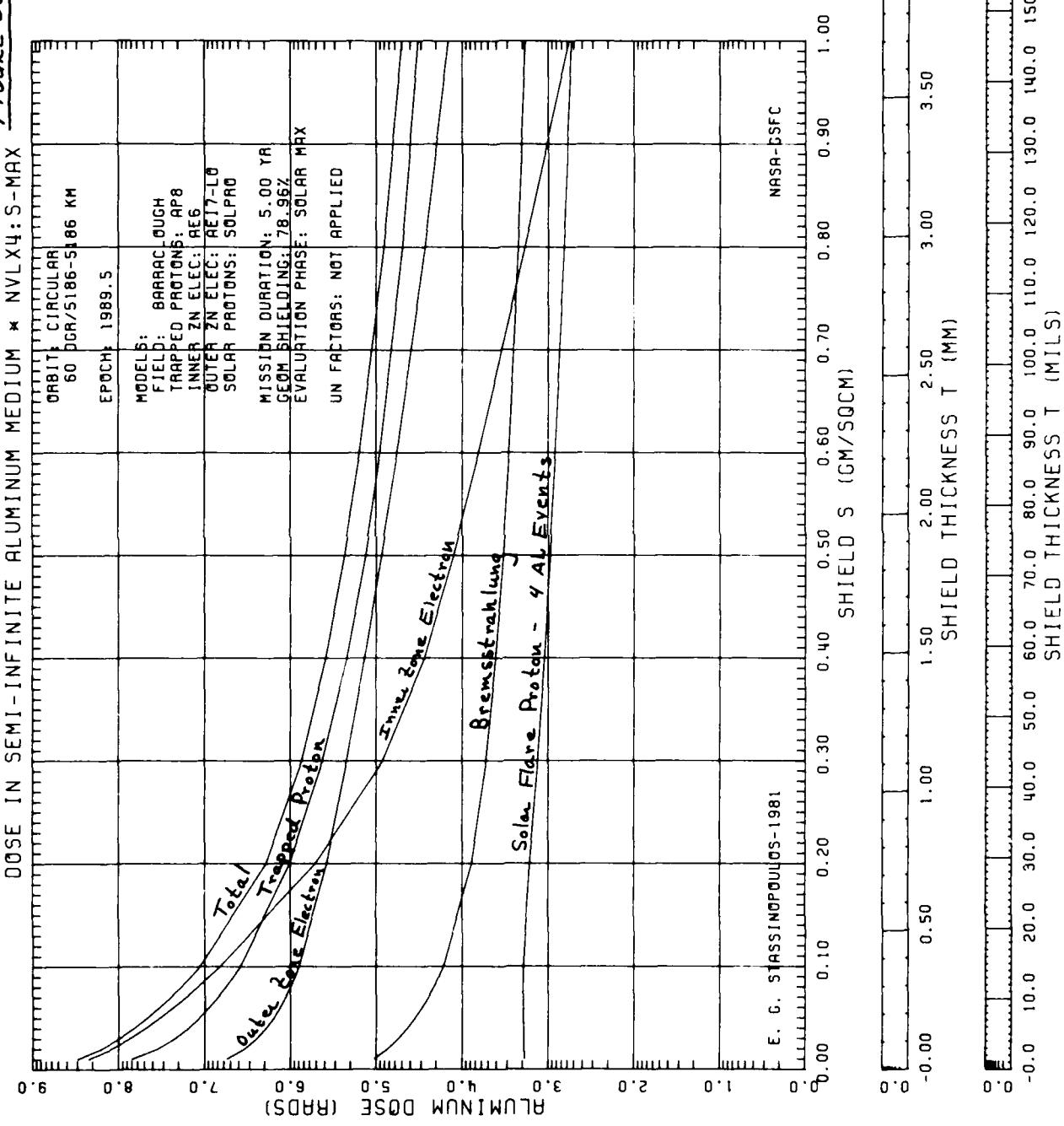


Figure 8/

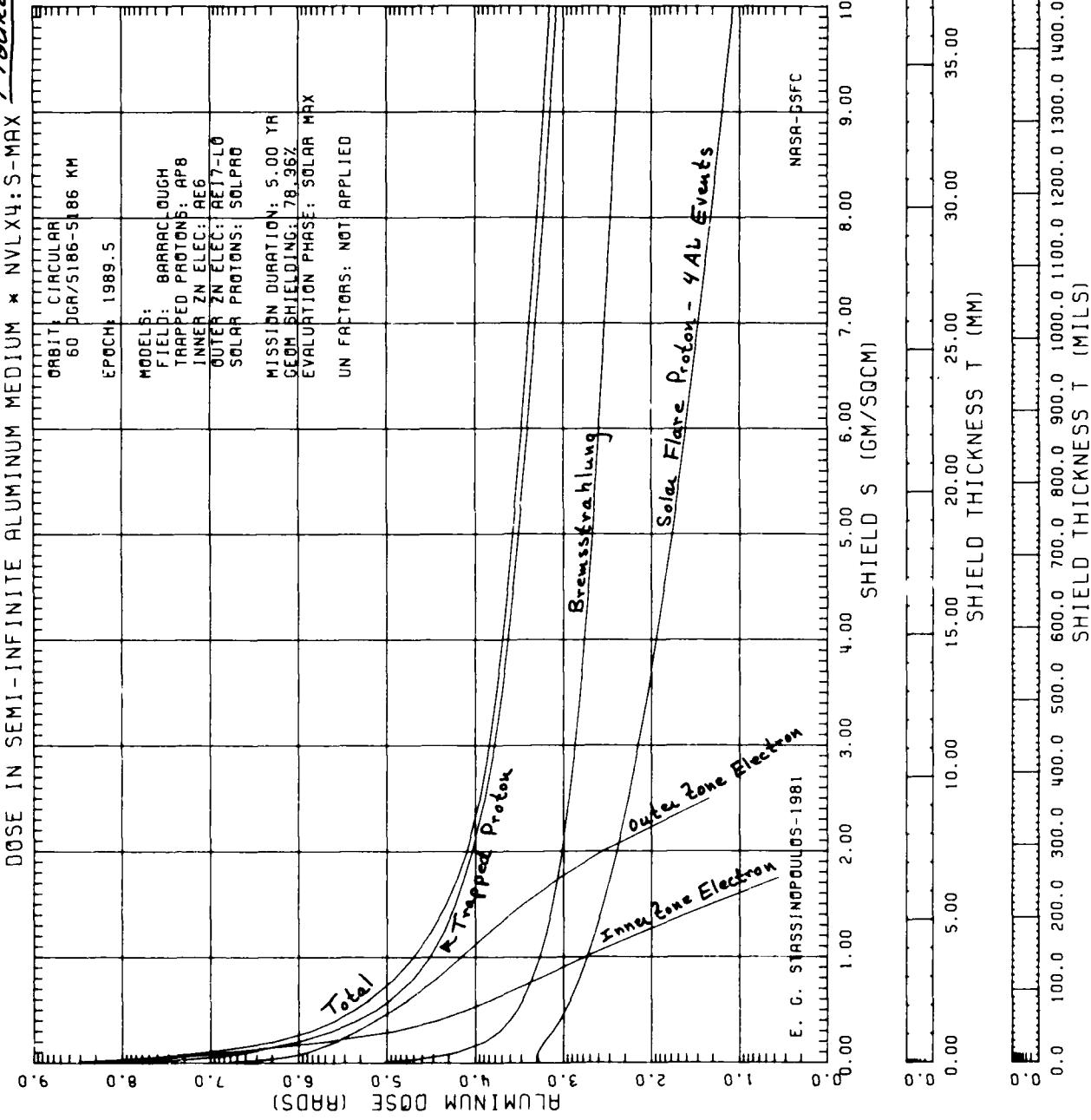


Figure 82

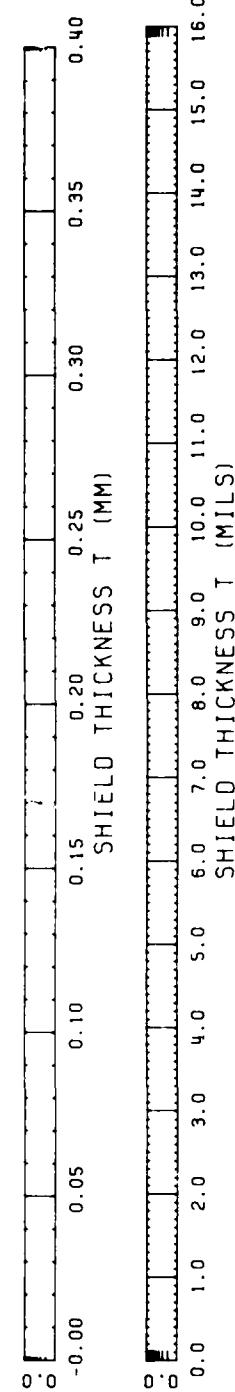
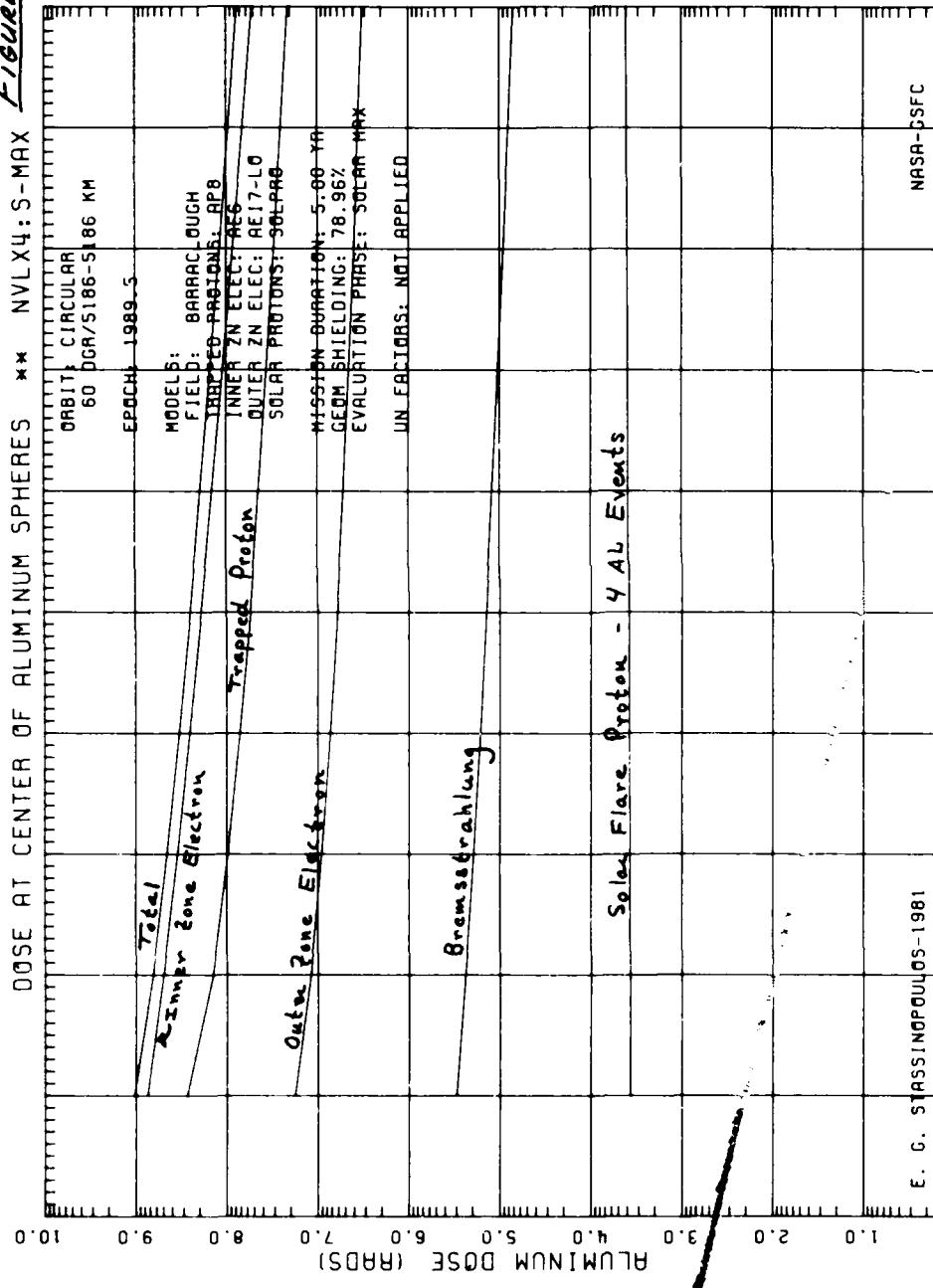


FIGURE 83

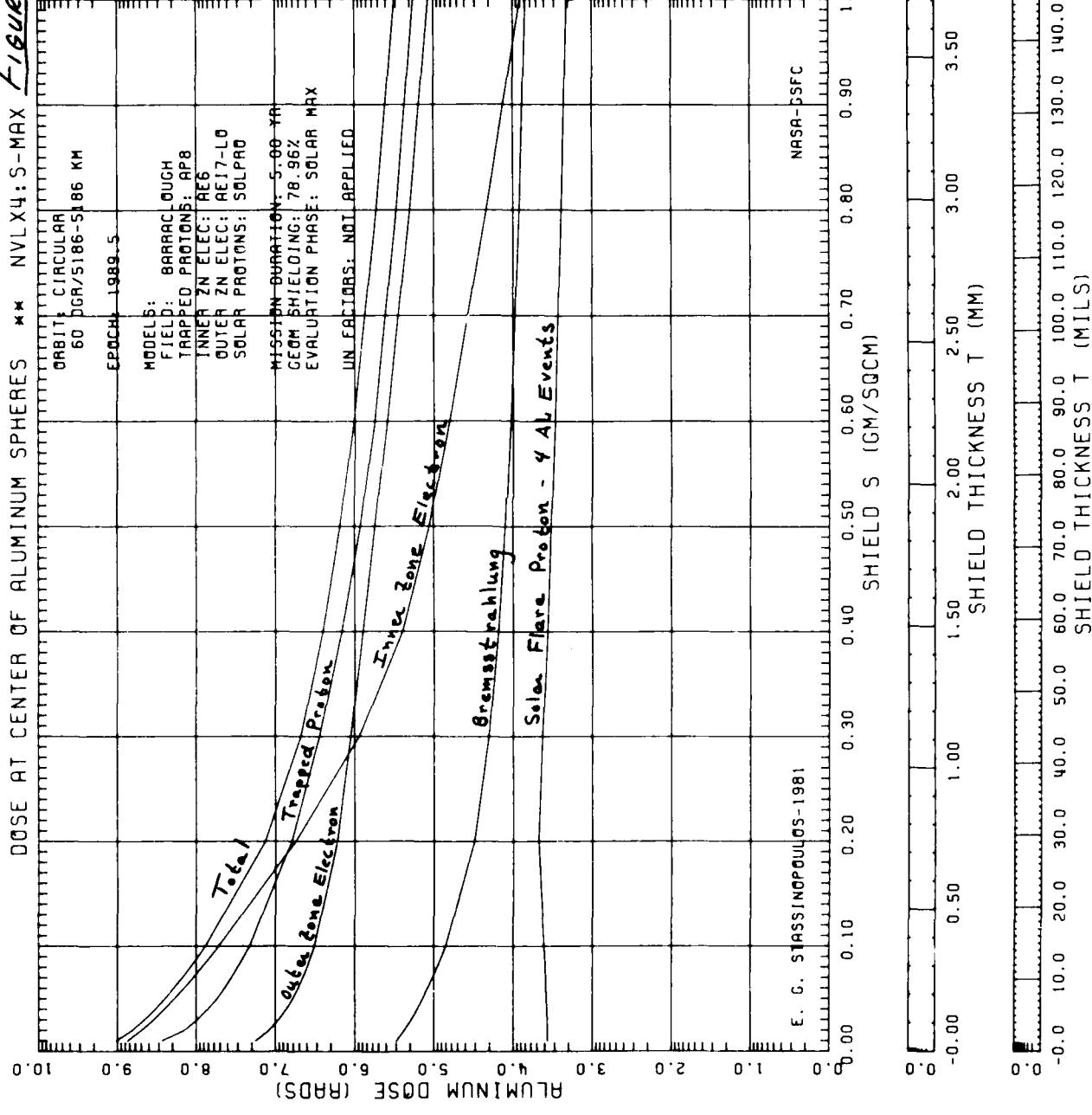


FIGURE 84

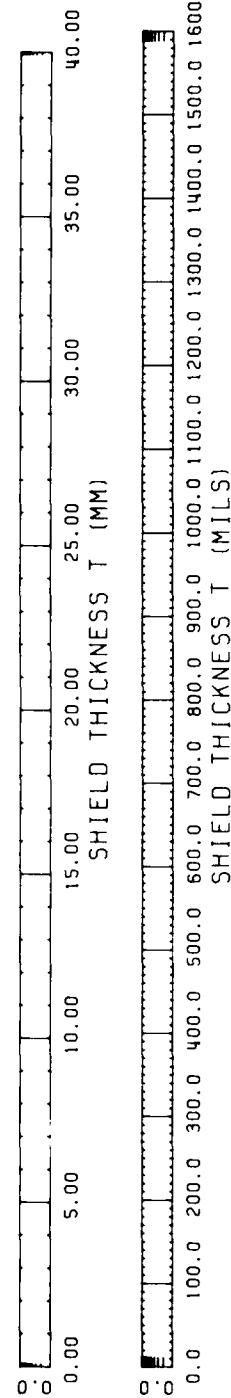
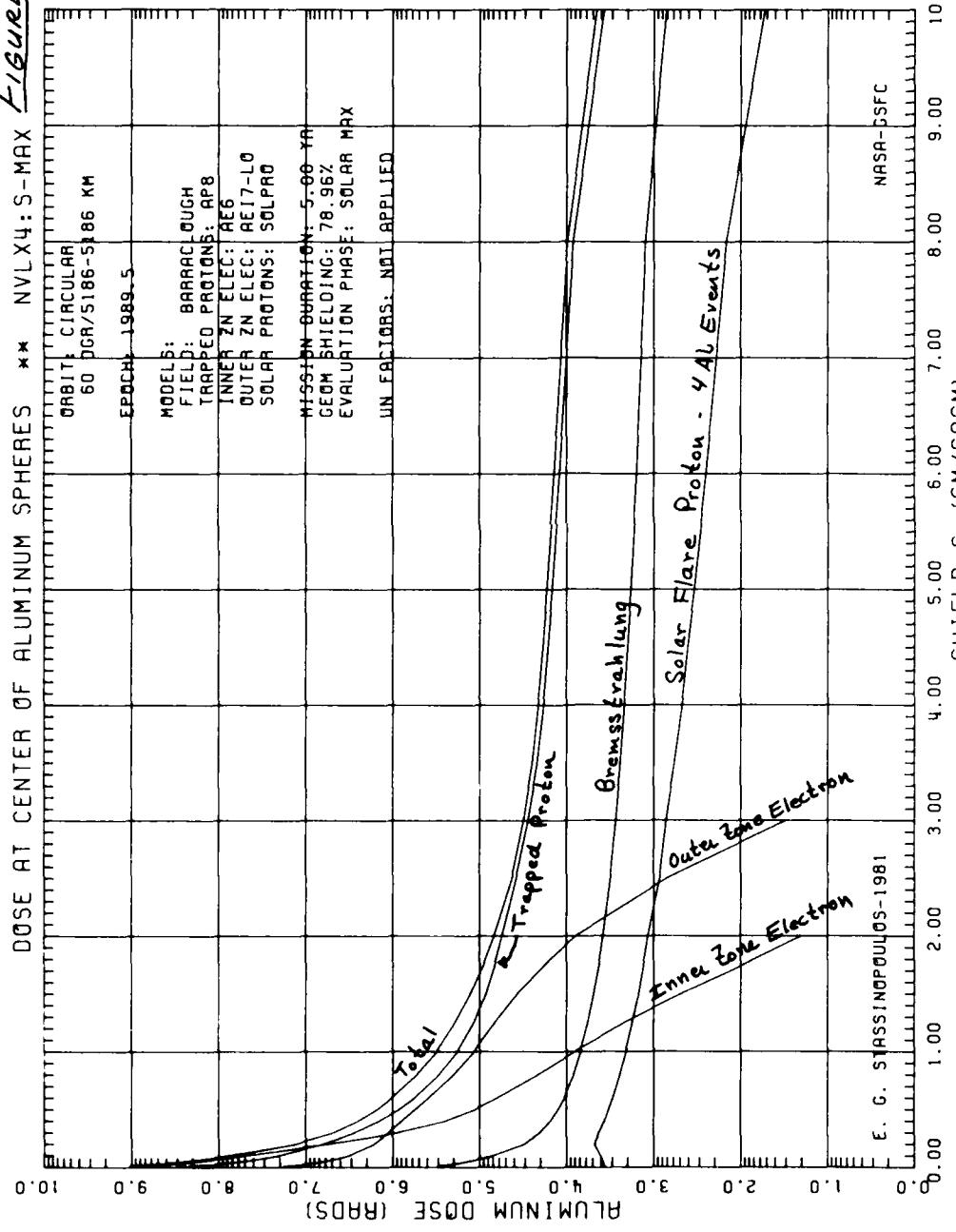


Figure 25

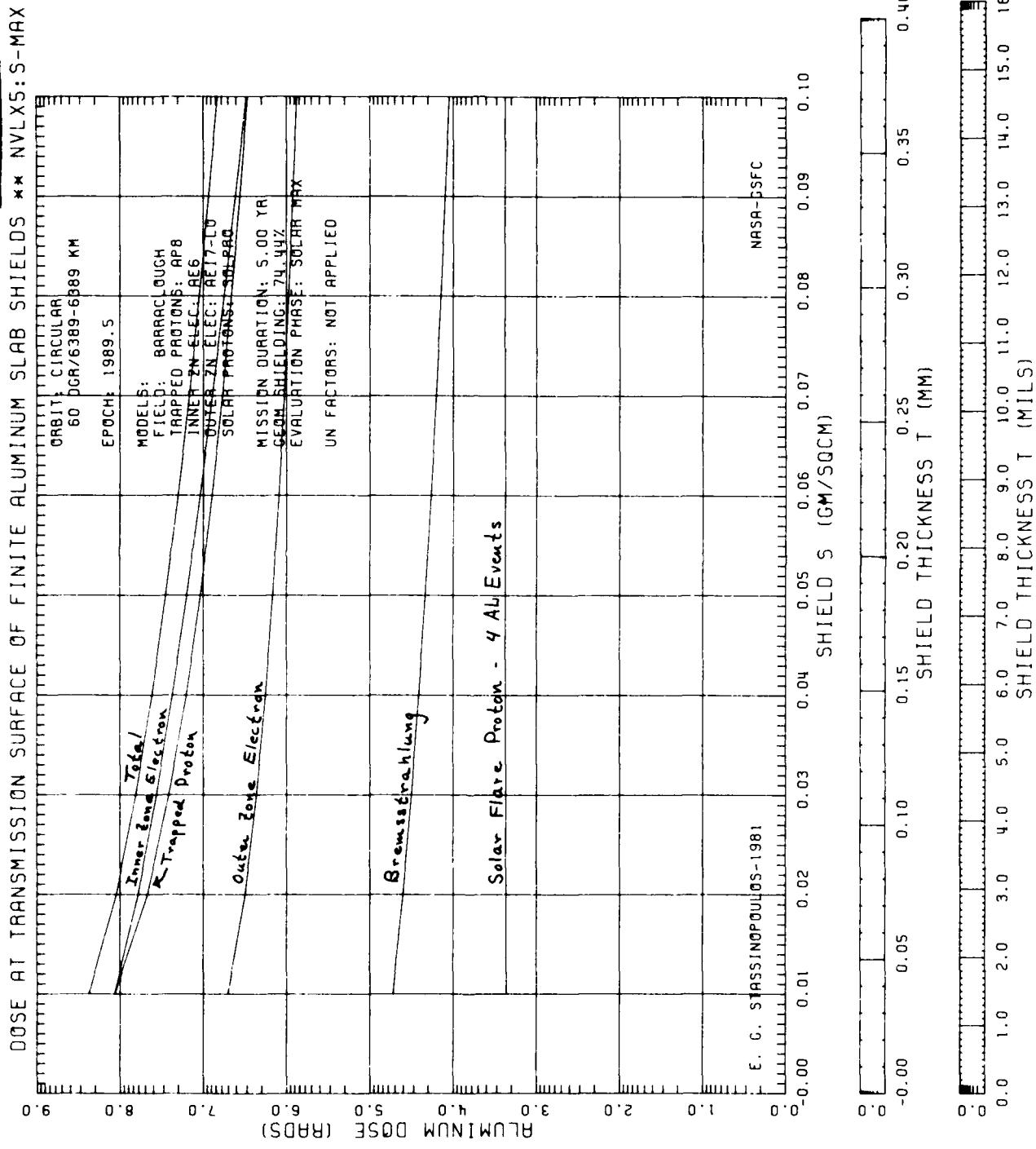


Figure 86

DOSE AT TRANSMISSION SURFACE OF FINITE ALUMINUM SLAB SHIELDS ** NVLX5: S-MAX

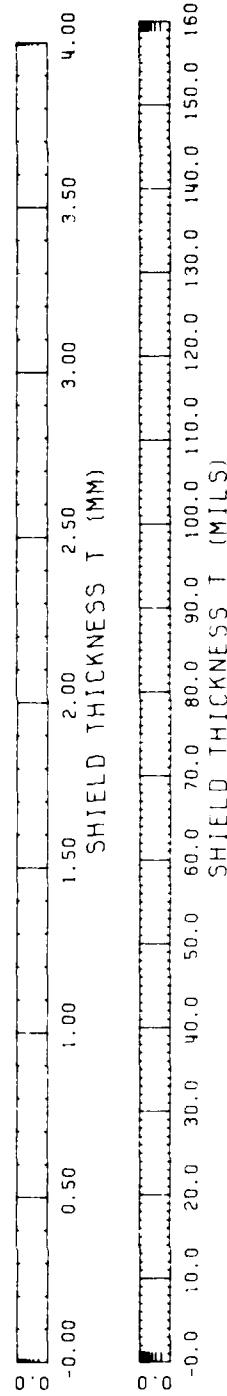
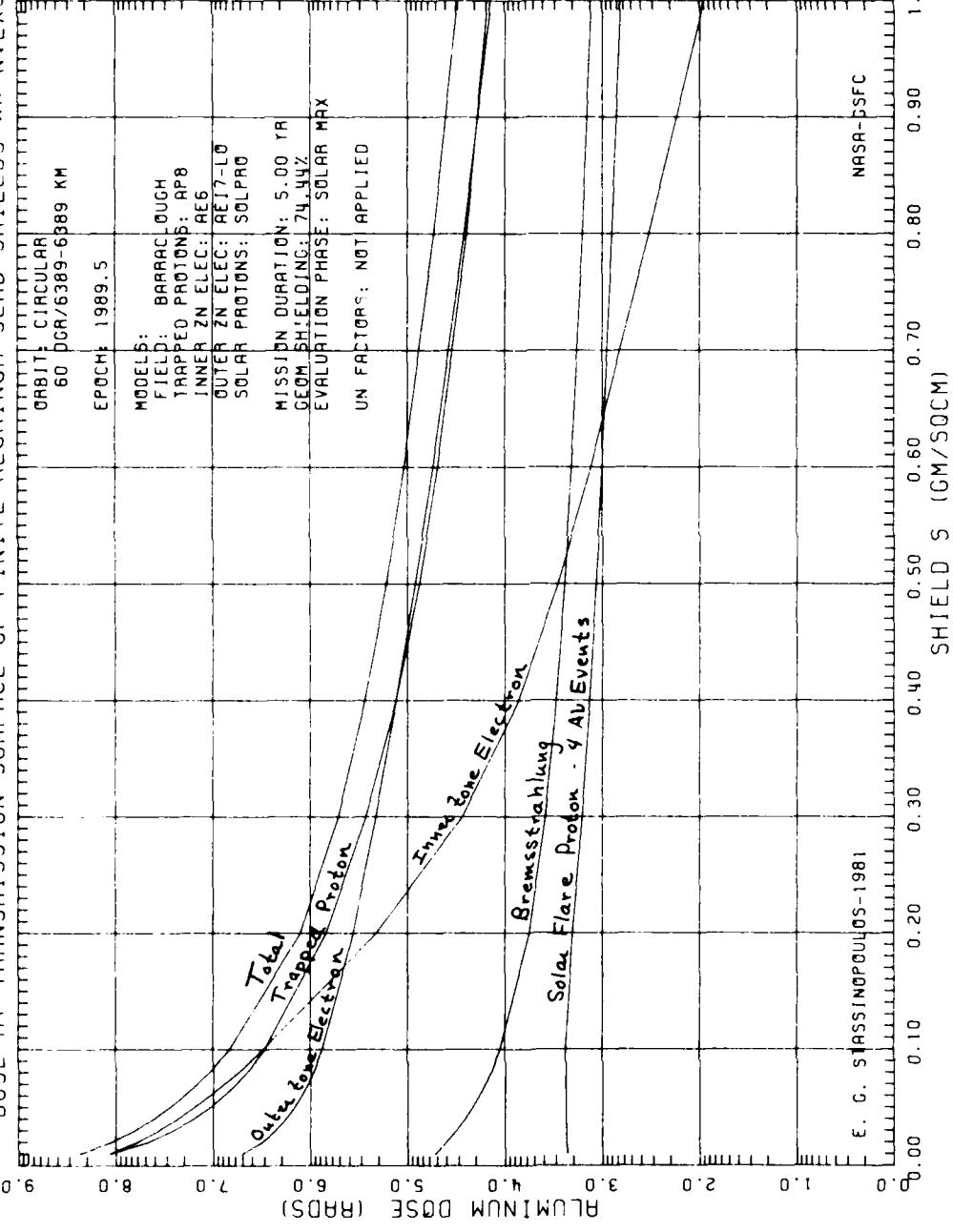


FIGURE 87

DOSAGE AT TRANSMISSION SURFACE OF FINITE ALUMINUM SLAB SHIELDS ** NVLX5: S..MAX

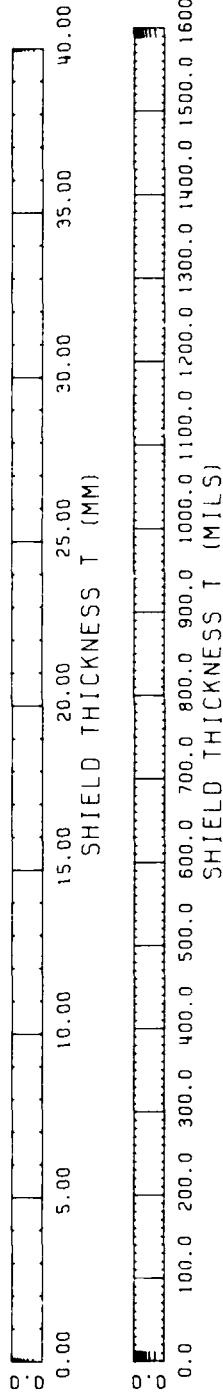
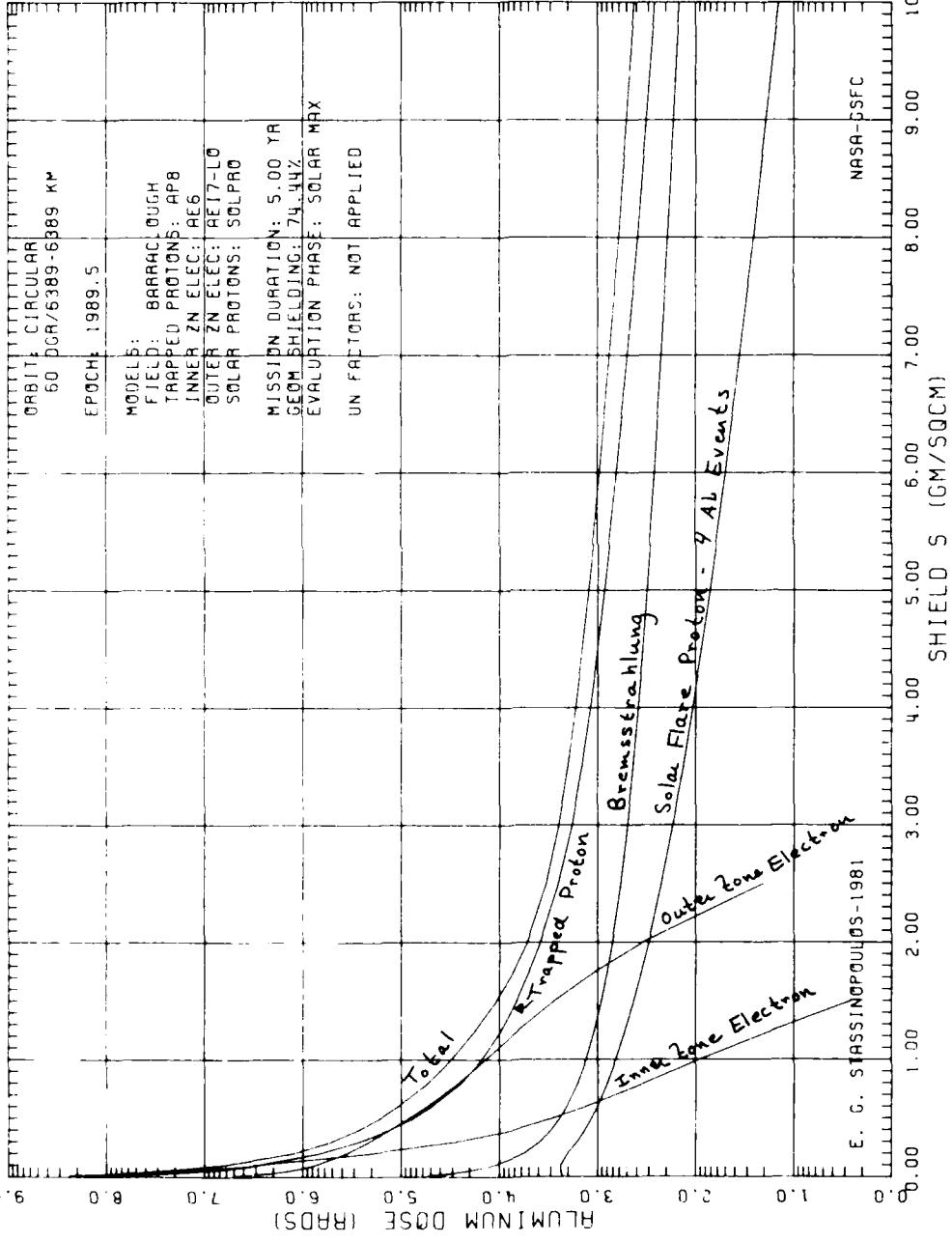
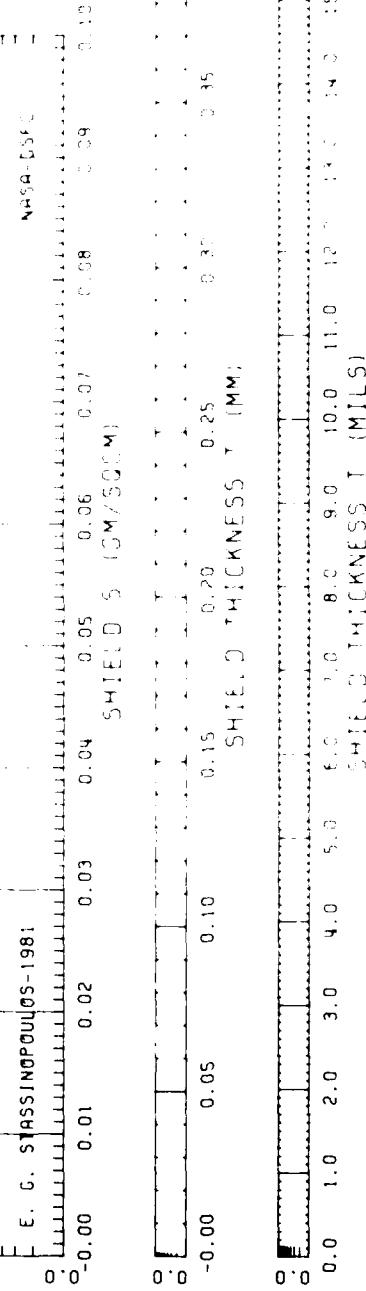
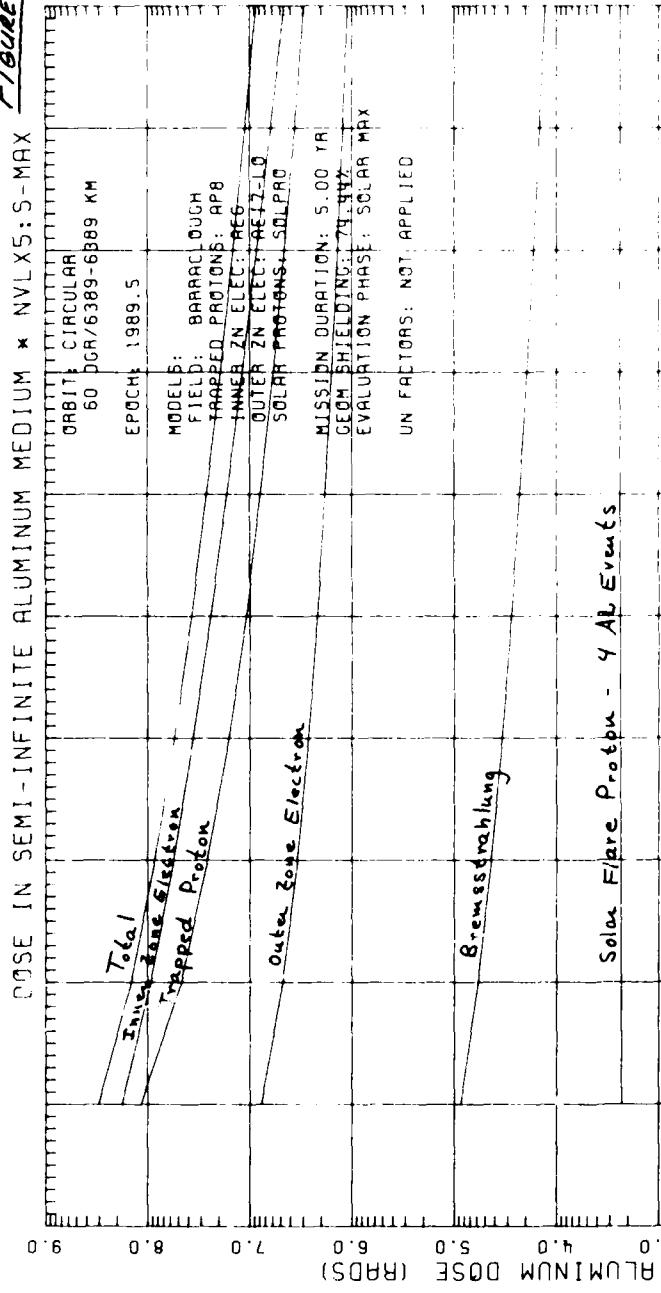


Figure 88



DOSE IN SEMI-INFINITE ALUMINUM MEDIUM vs. NEXUS MAX

Figure 89

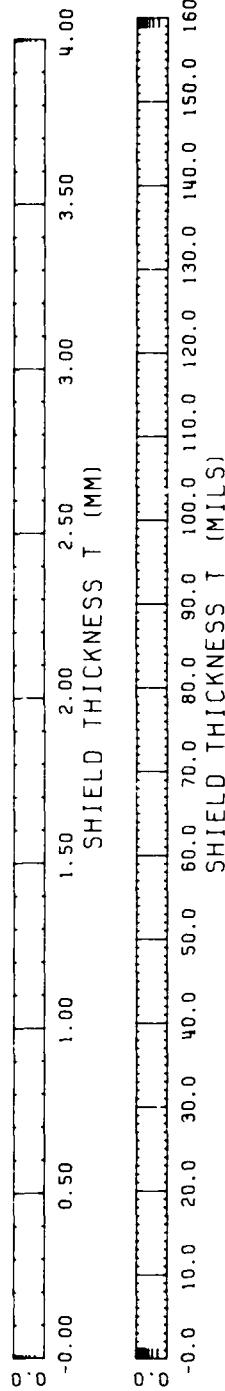
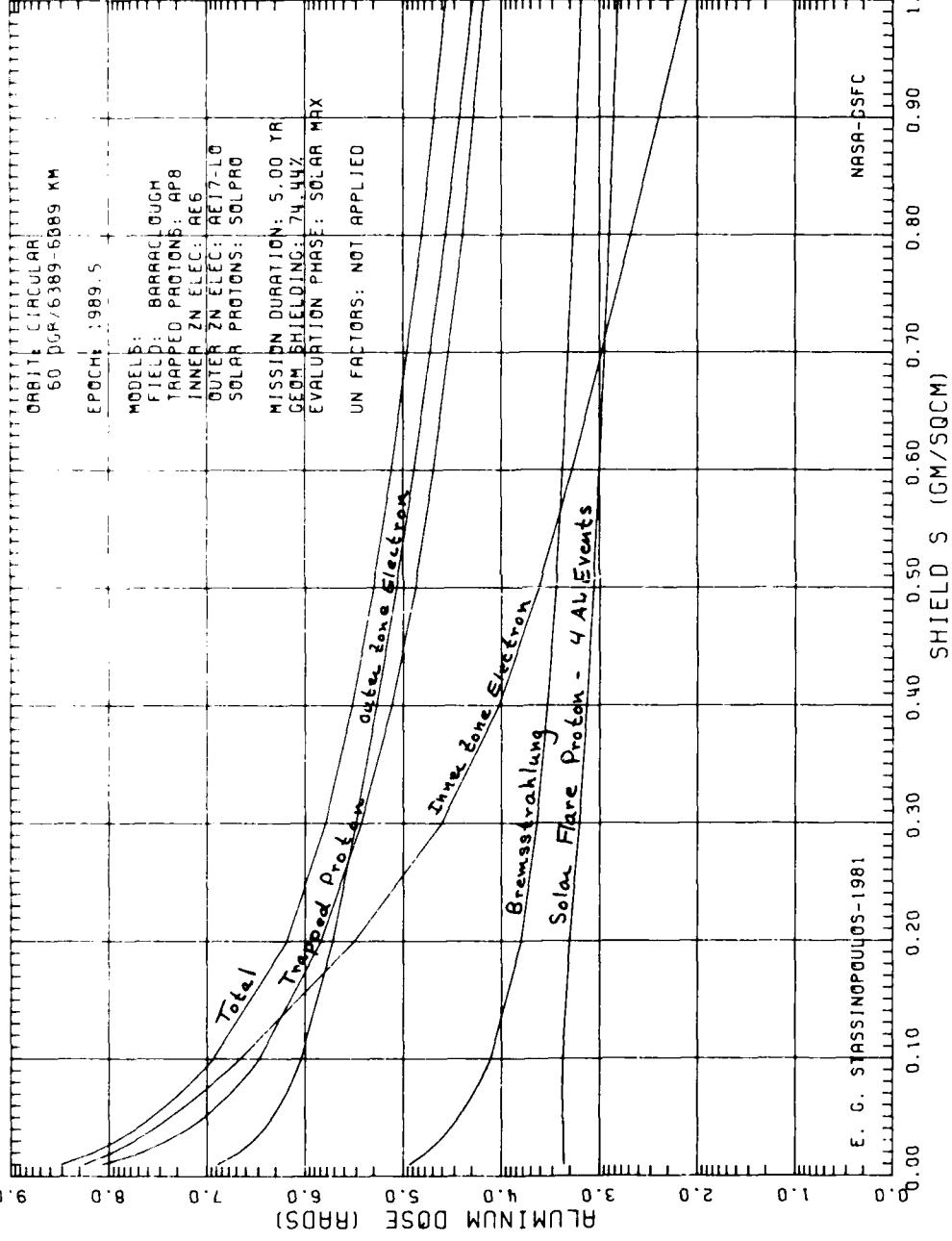


Figure 90

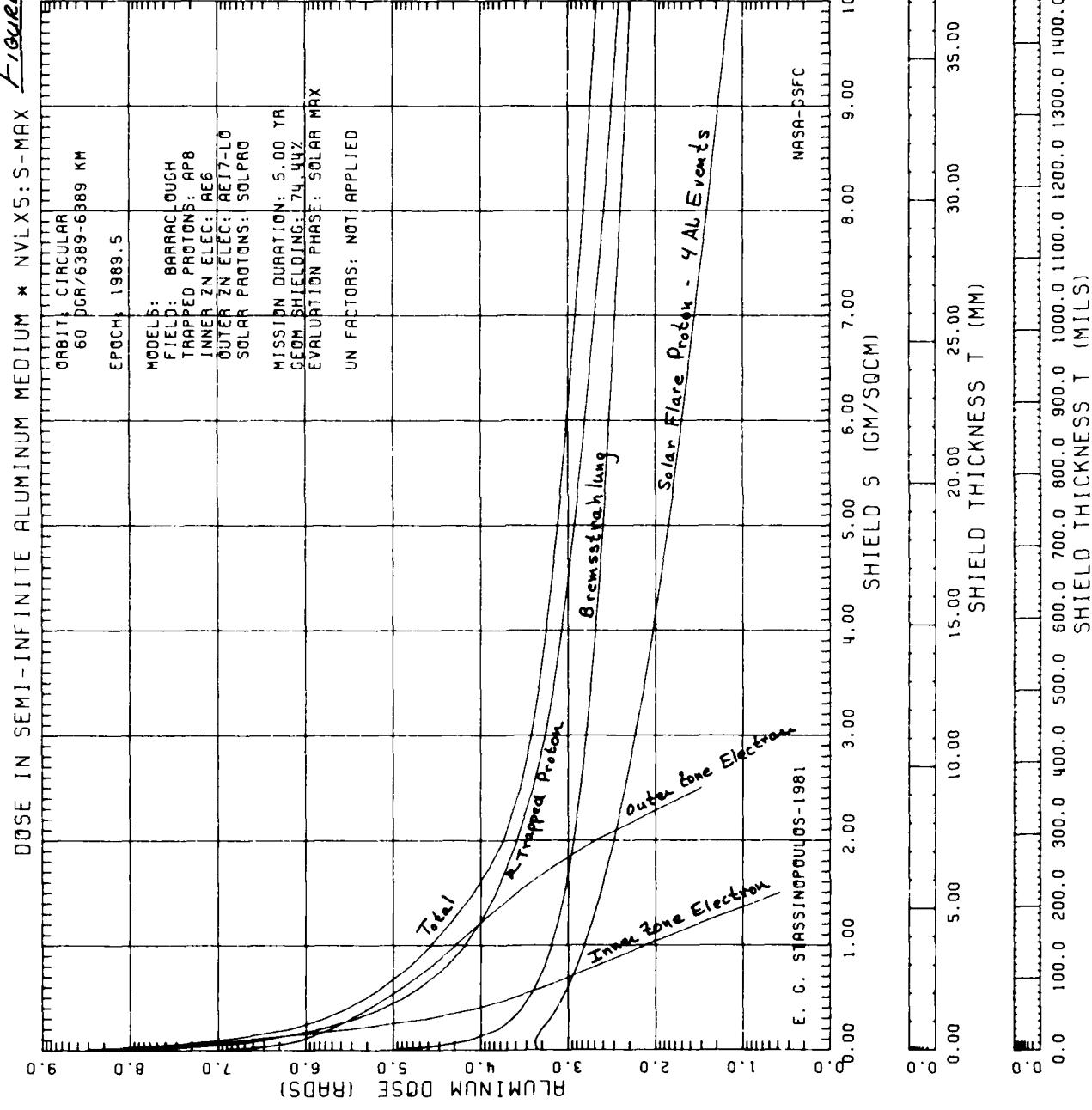


Figure 91

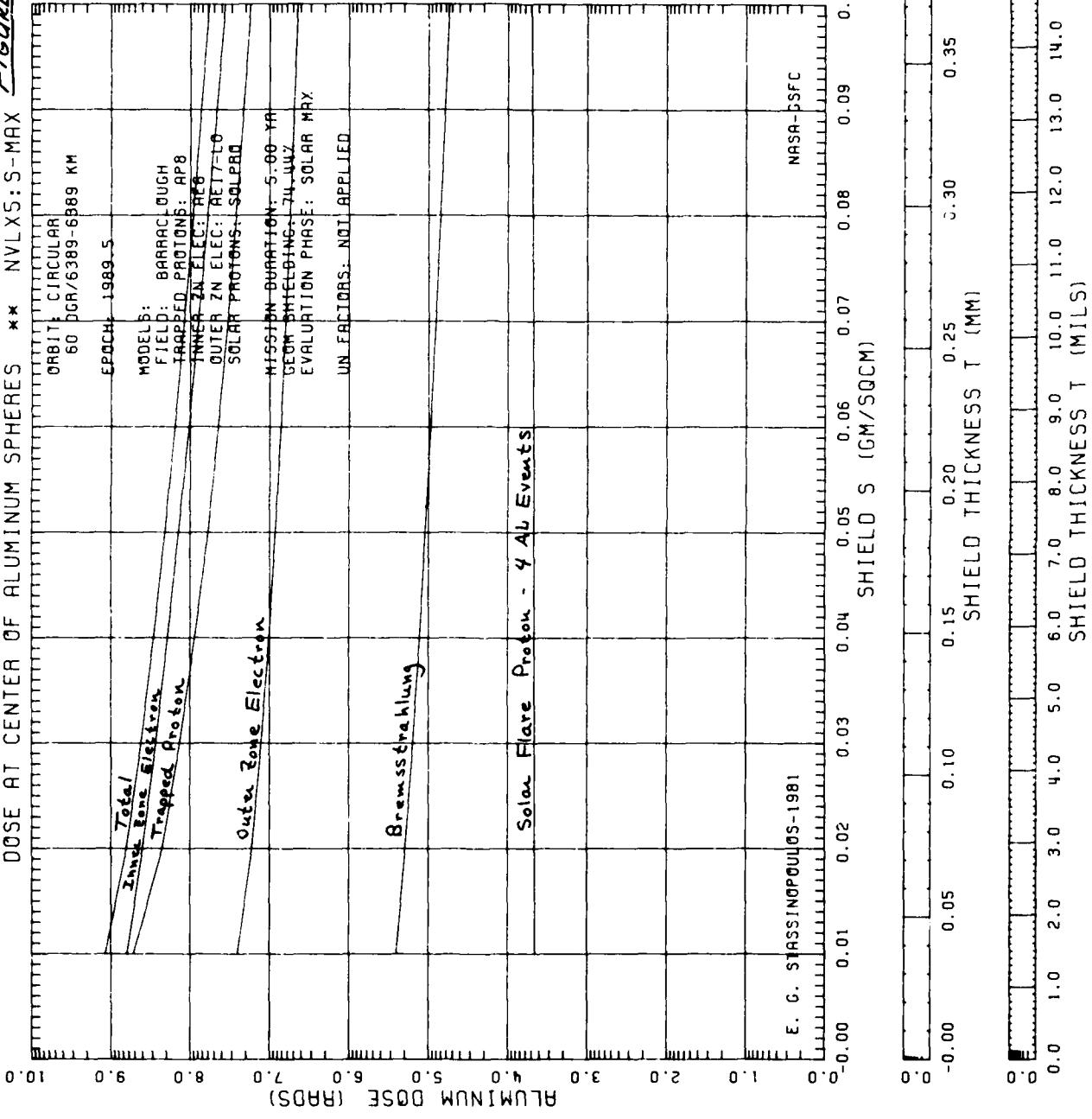


FIGURE 92

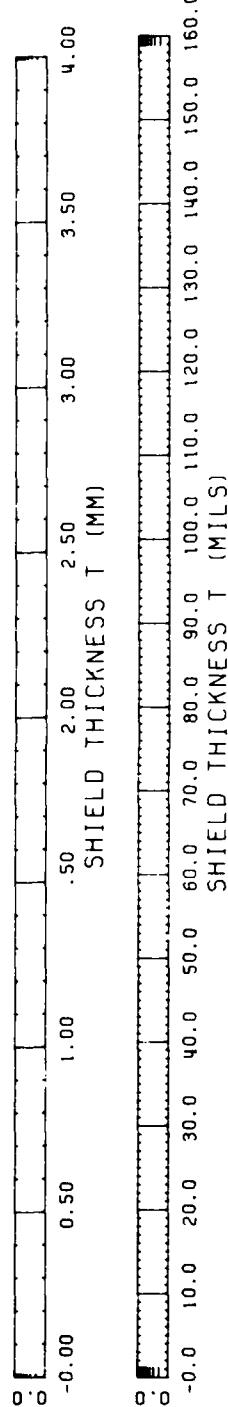
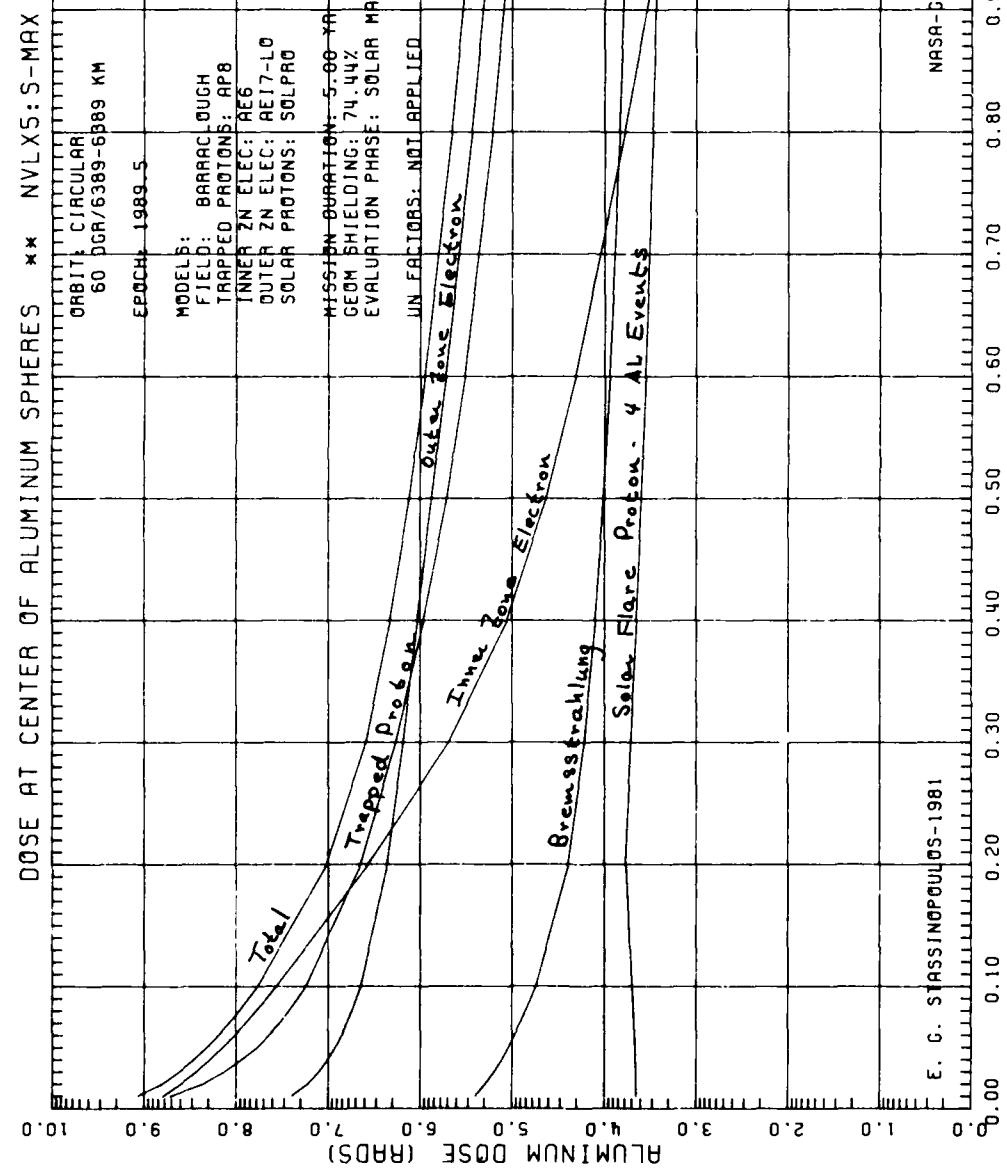


Figure 93

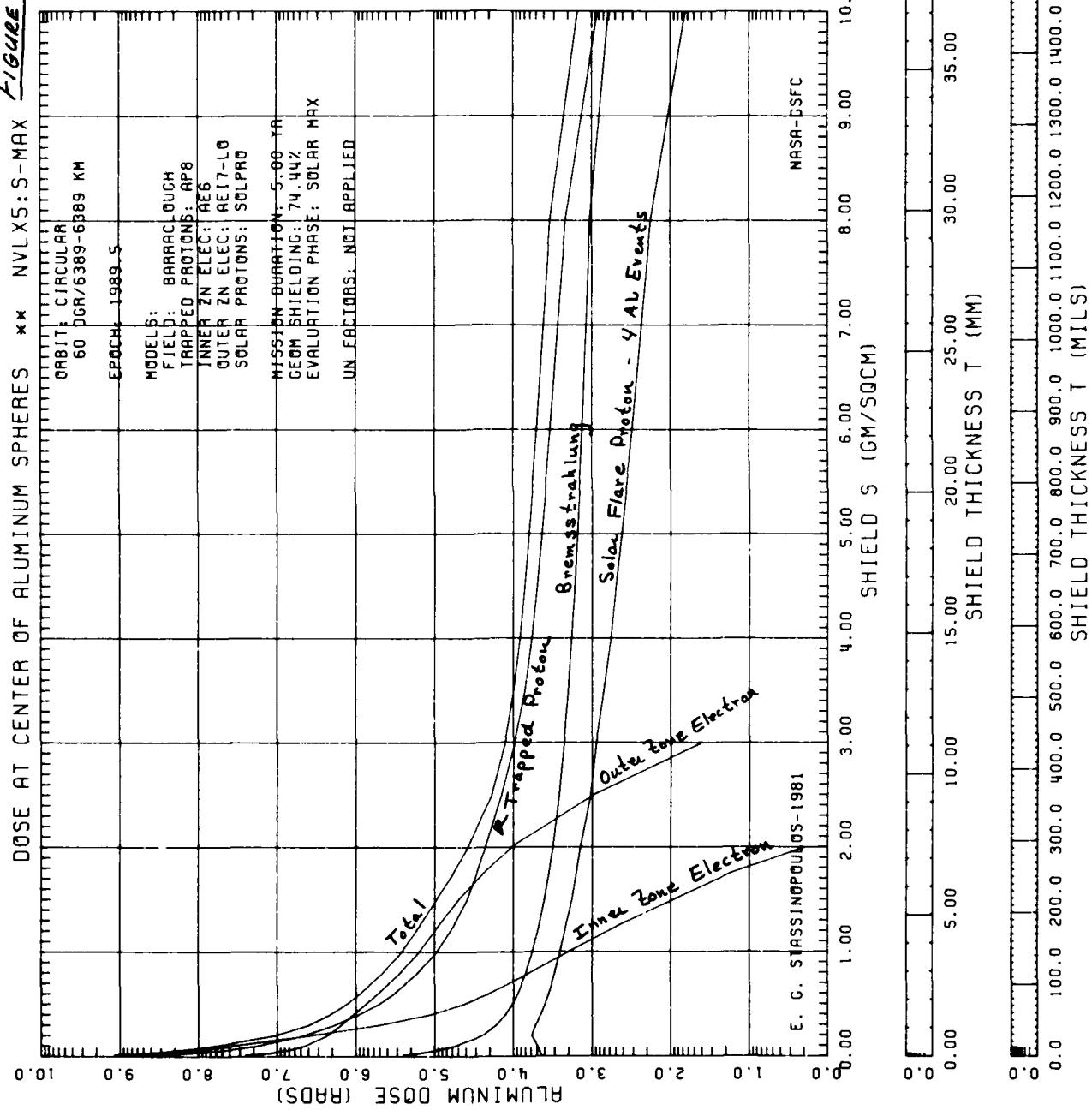


Figure 94

* NVLX6: S-MAX

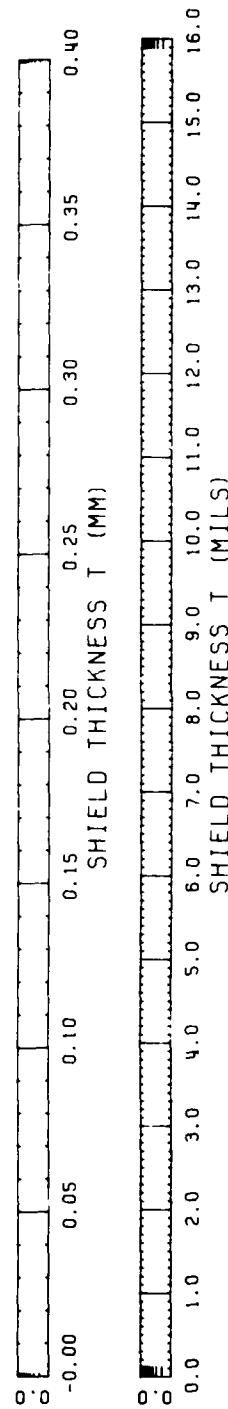
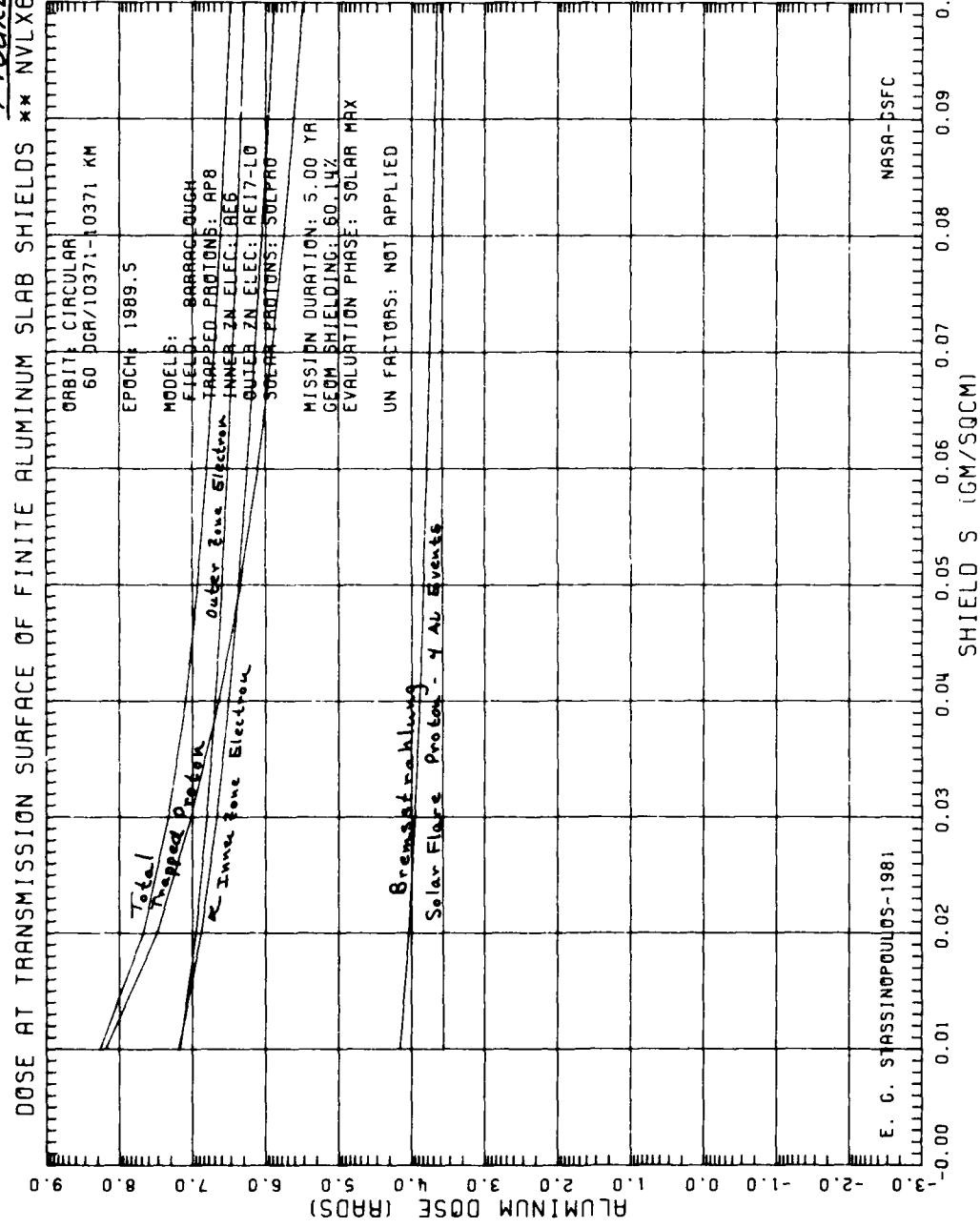


Figure 95

DOSE AT TRANSMISSION SURFACE OF FINITE ALUMINUM SLAB SHIELDS ** NVLX6: S-MAX

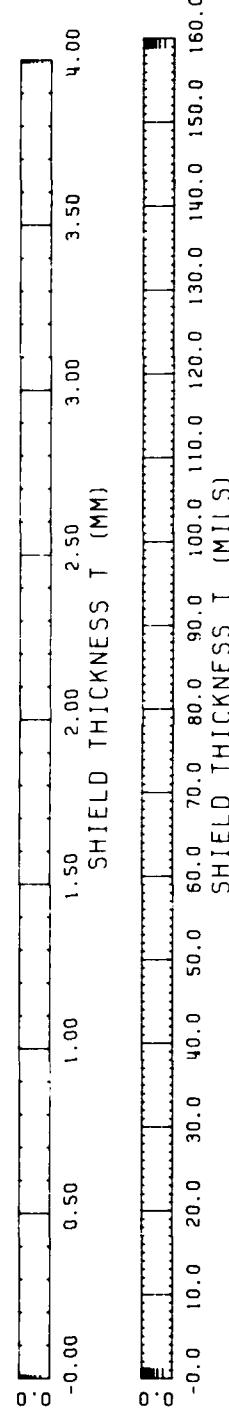
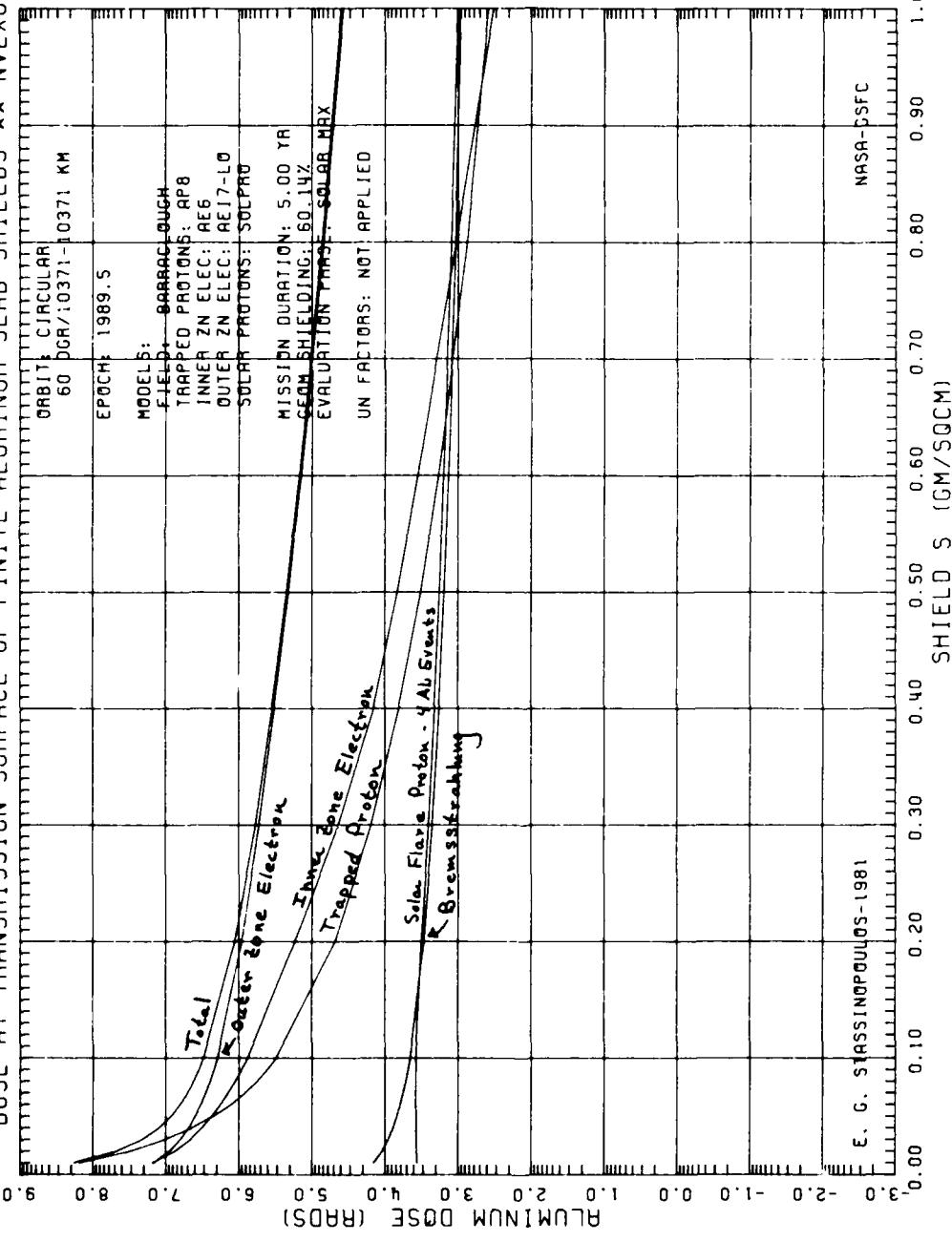


Figure 26

NVLX6:S-MAX

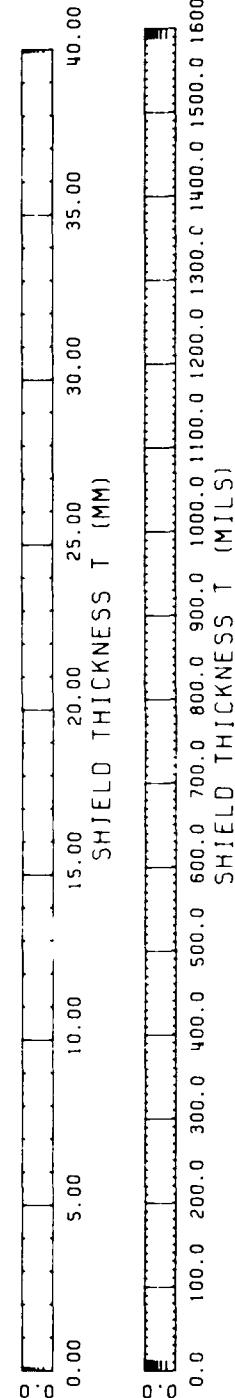
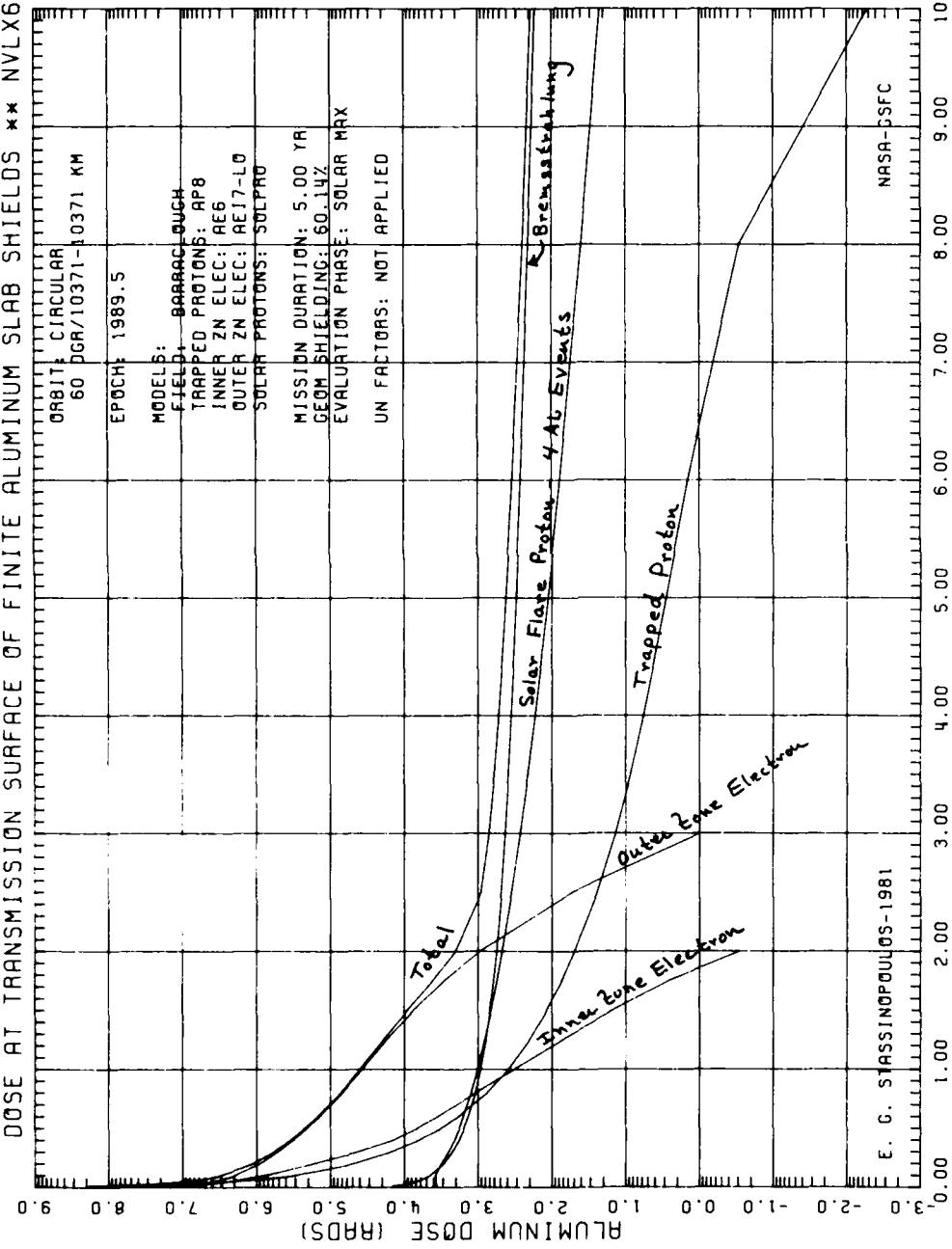
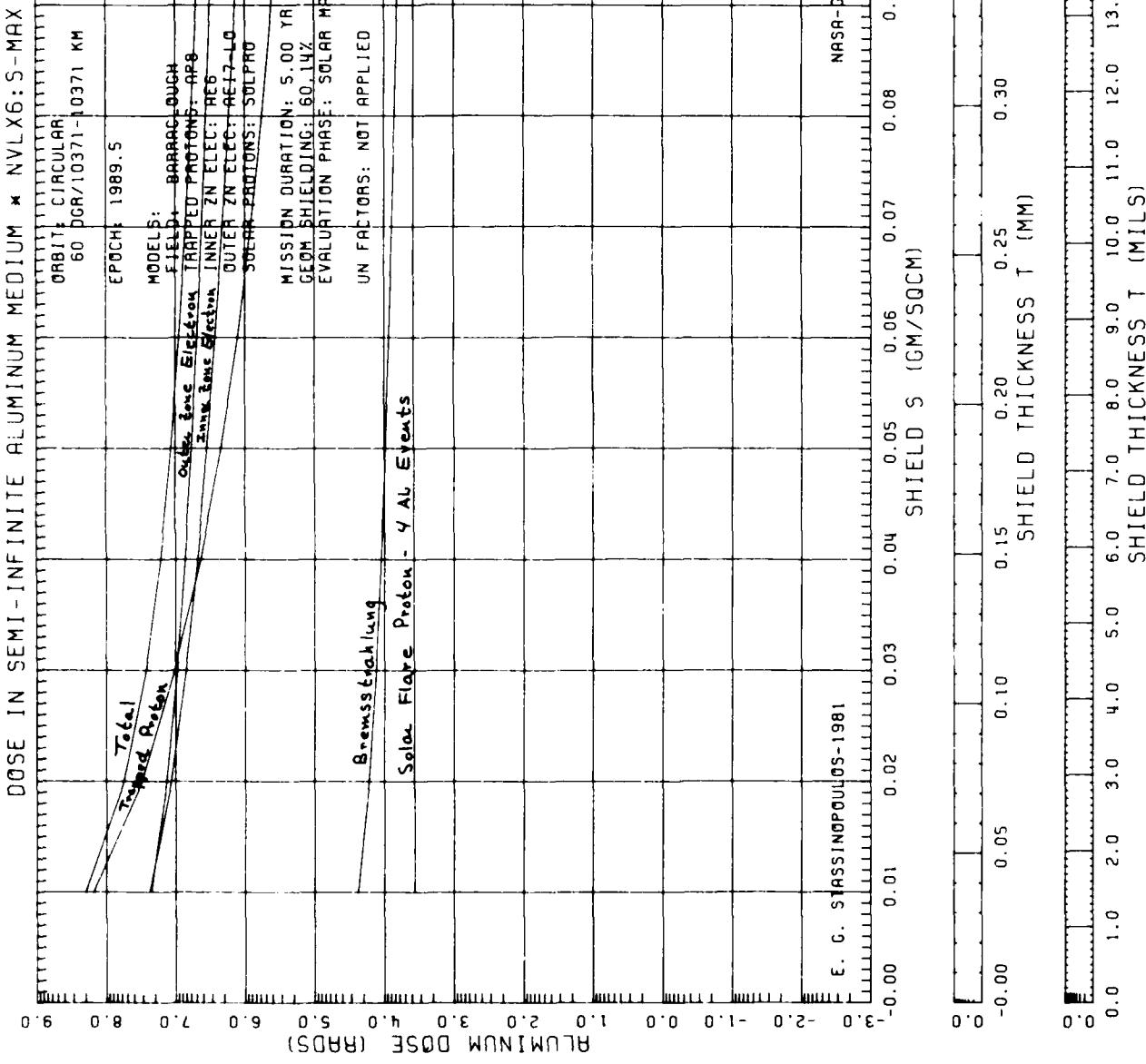
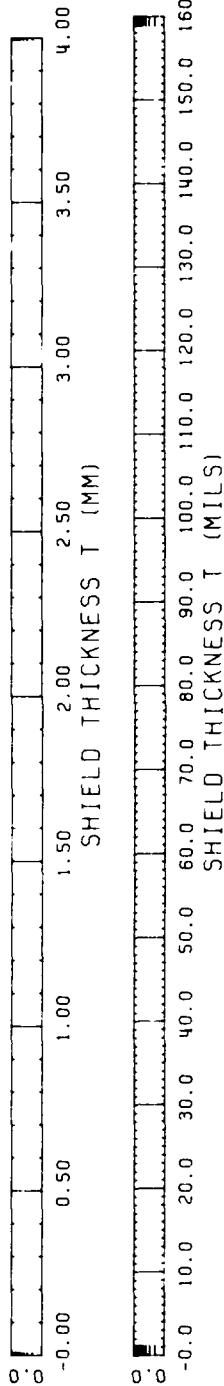
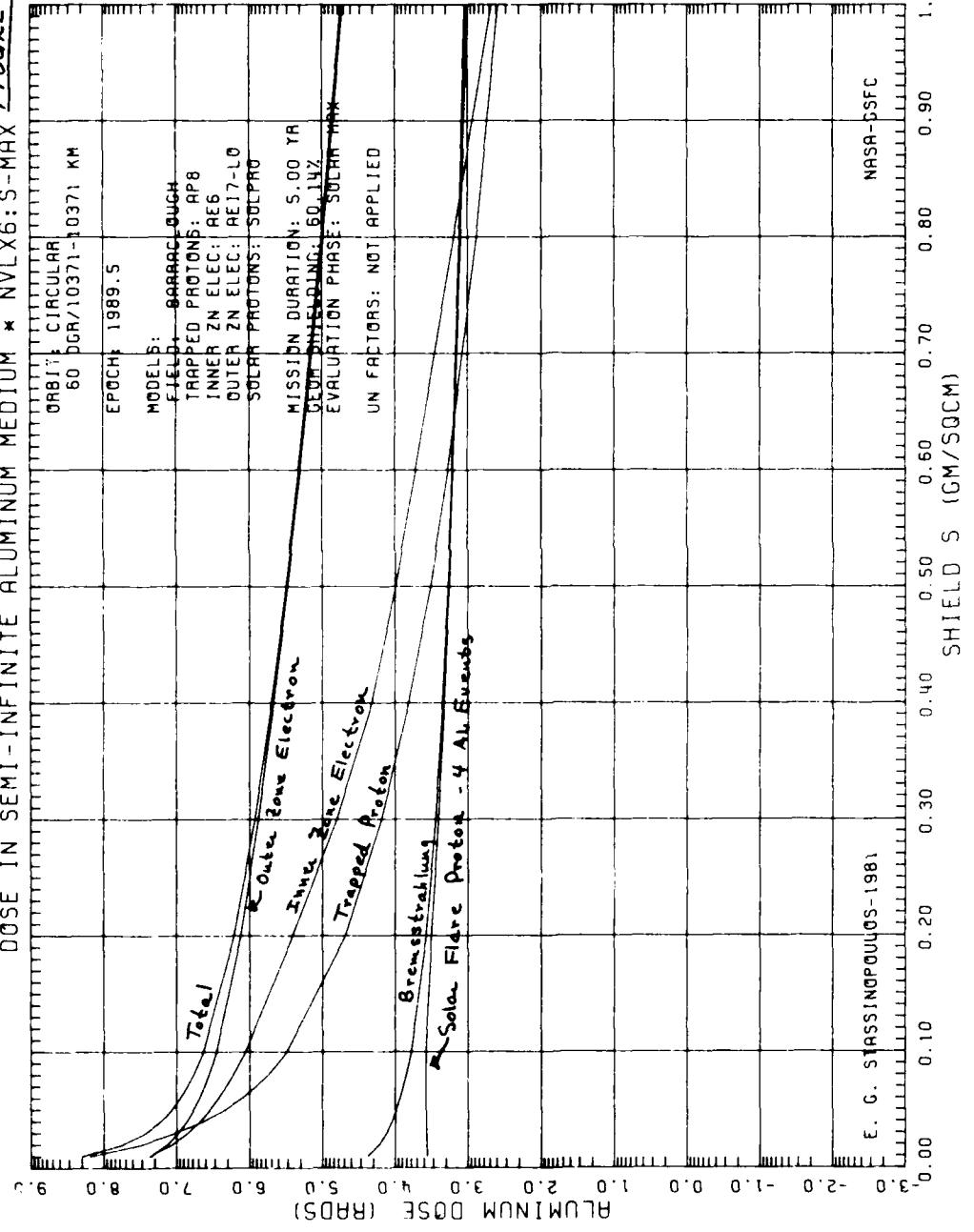


FIGURE 97



DOSAGE IN SEMI-INFINITE ALUMINUM MEDIUM * NVLX6: S-MAX

FIGURE 98



DOSE IN SEMI-INFINITE ALUMINUM MEDIUM * NVLX6: S-MAX Figure 99

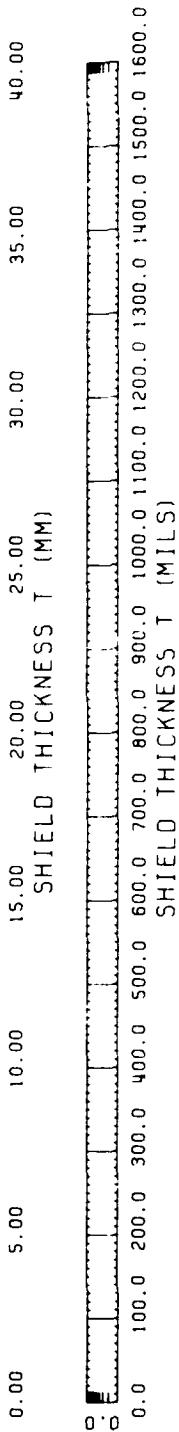
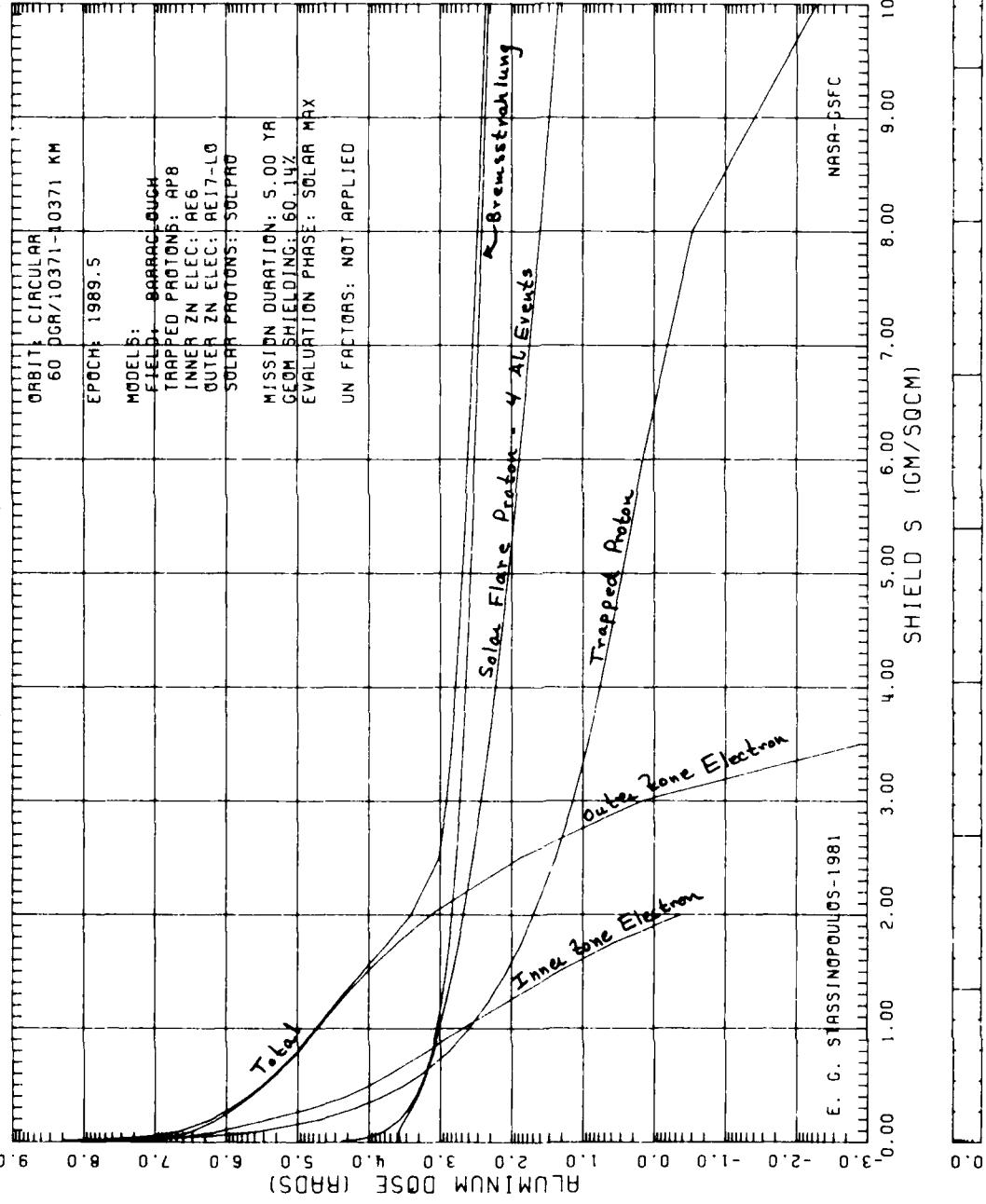
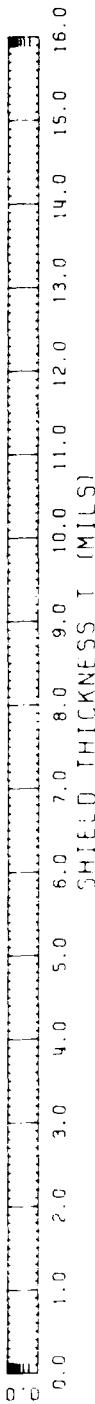
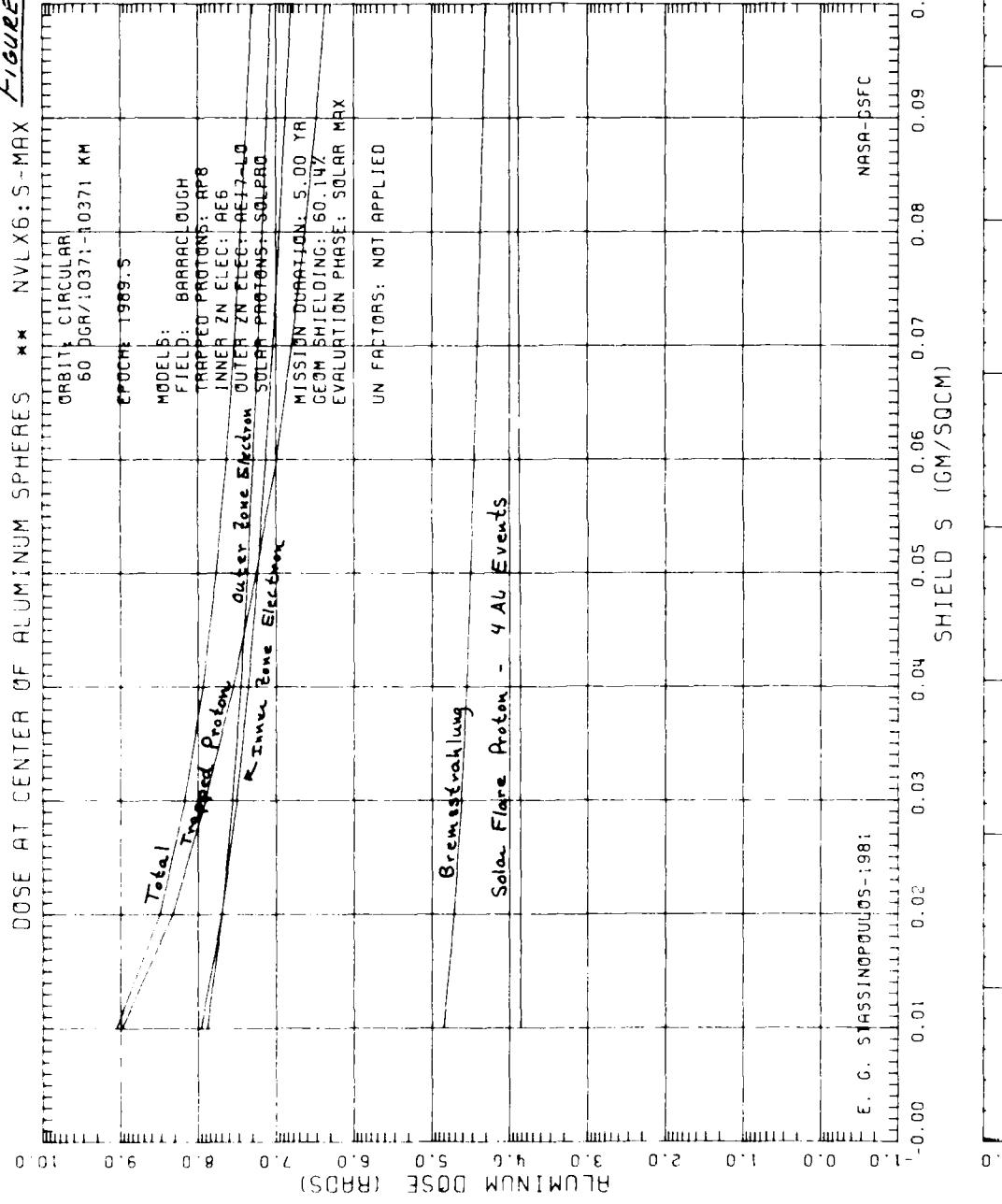


FIGURE 100



DOSE AT CENTER OF ALUMINUM SPHERES ** NVLX6: S-- MAX

FIGURE 101

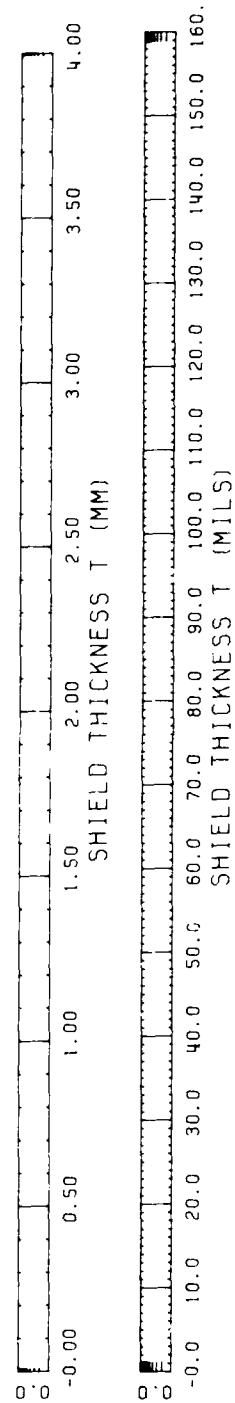
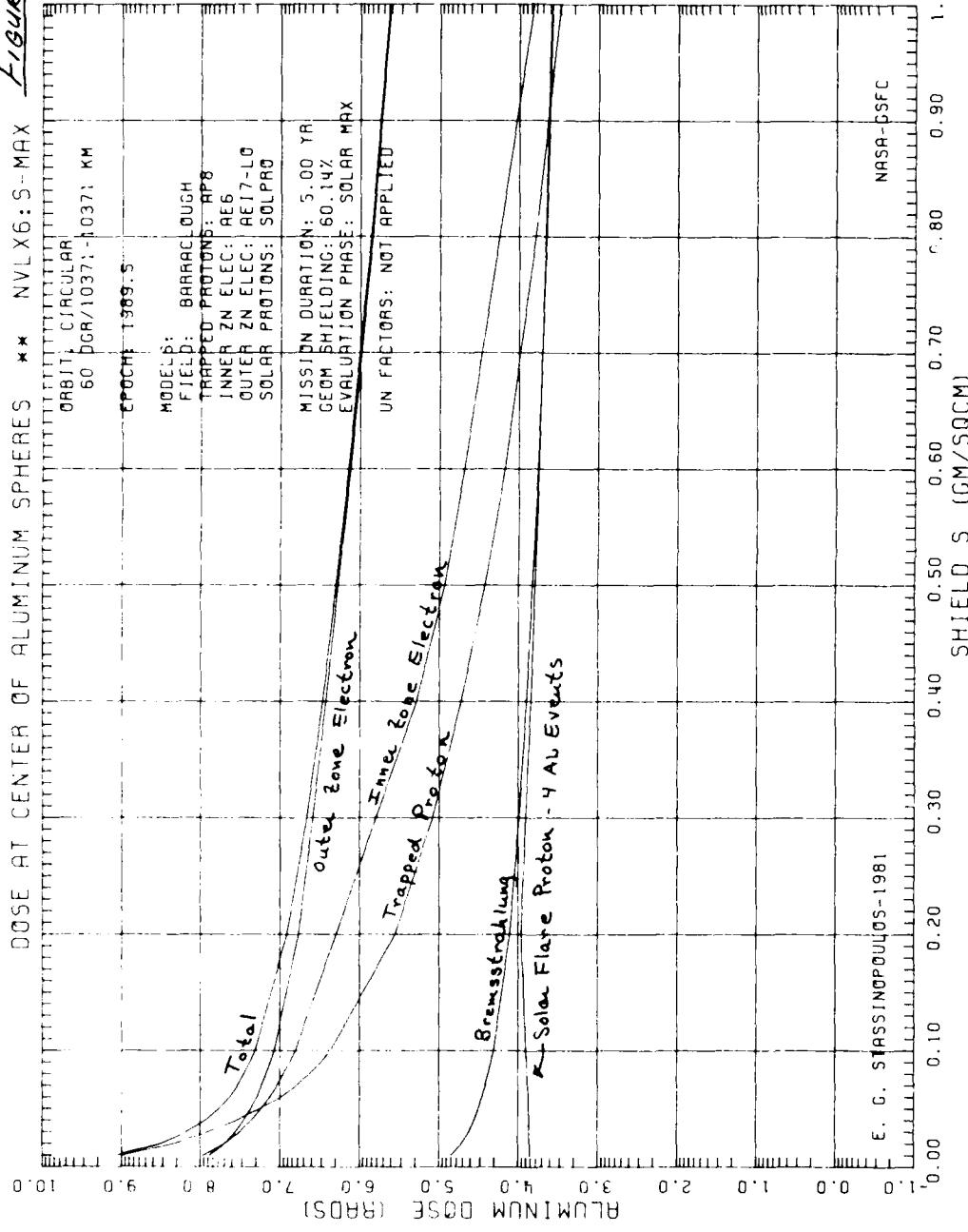
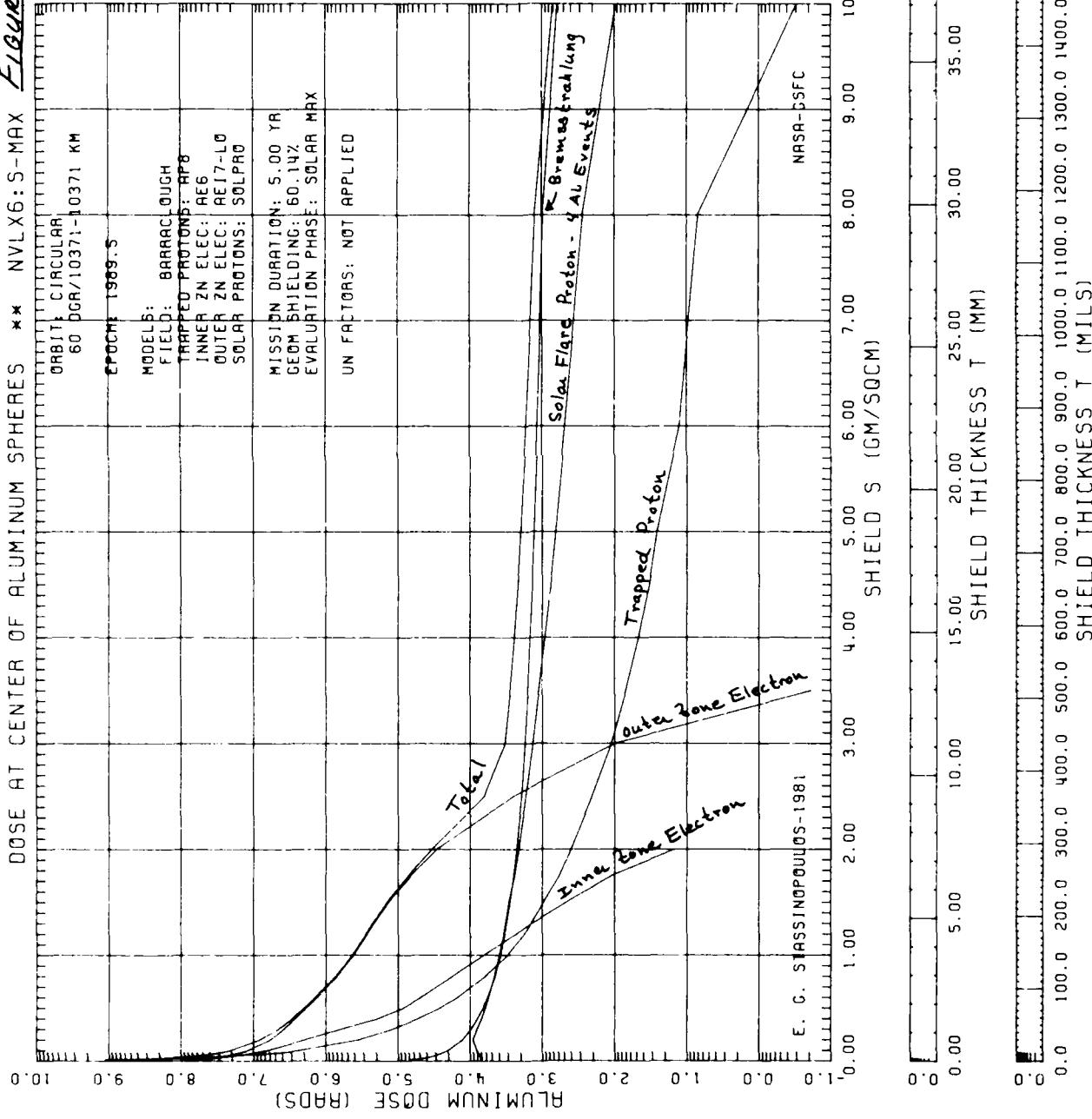
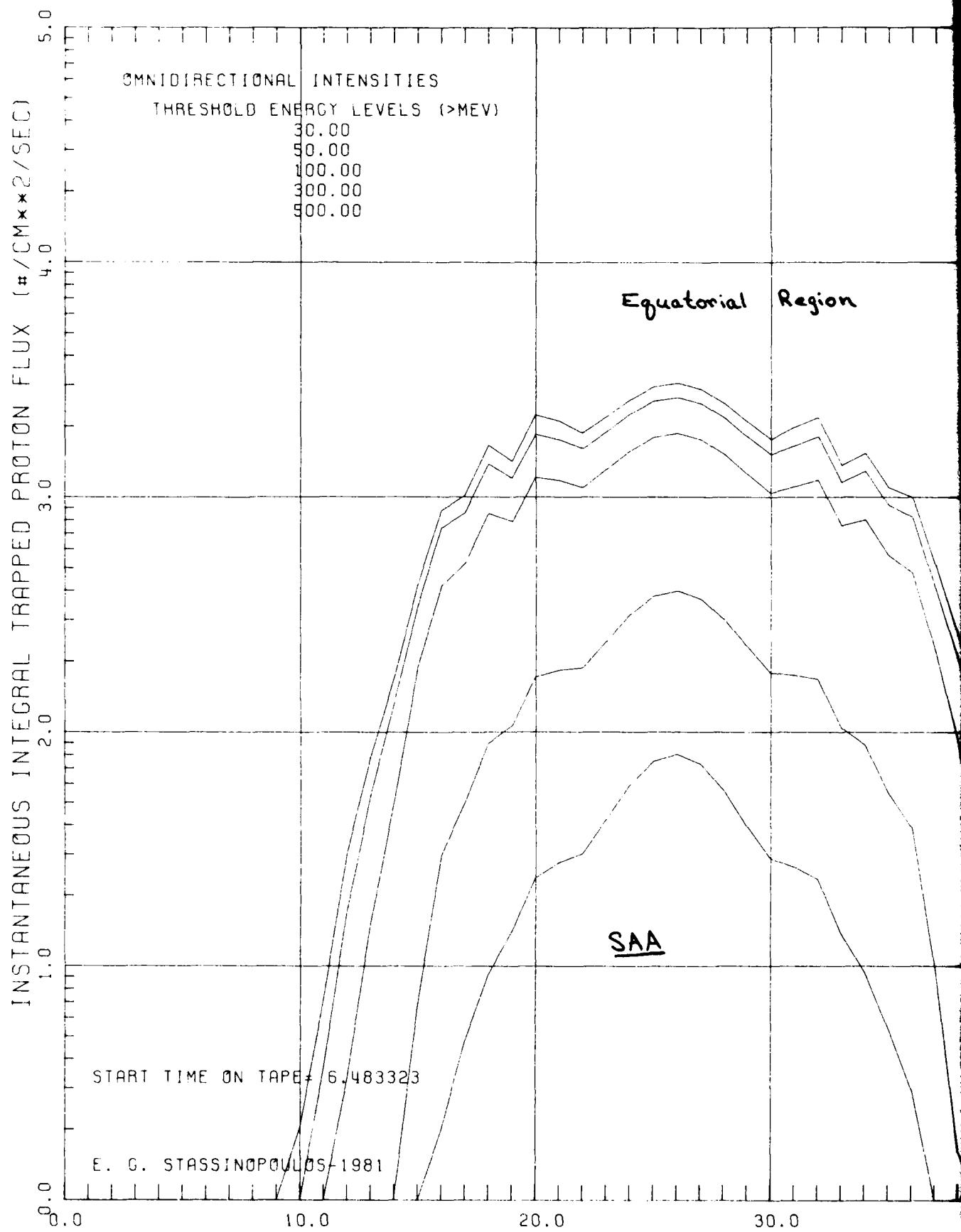
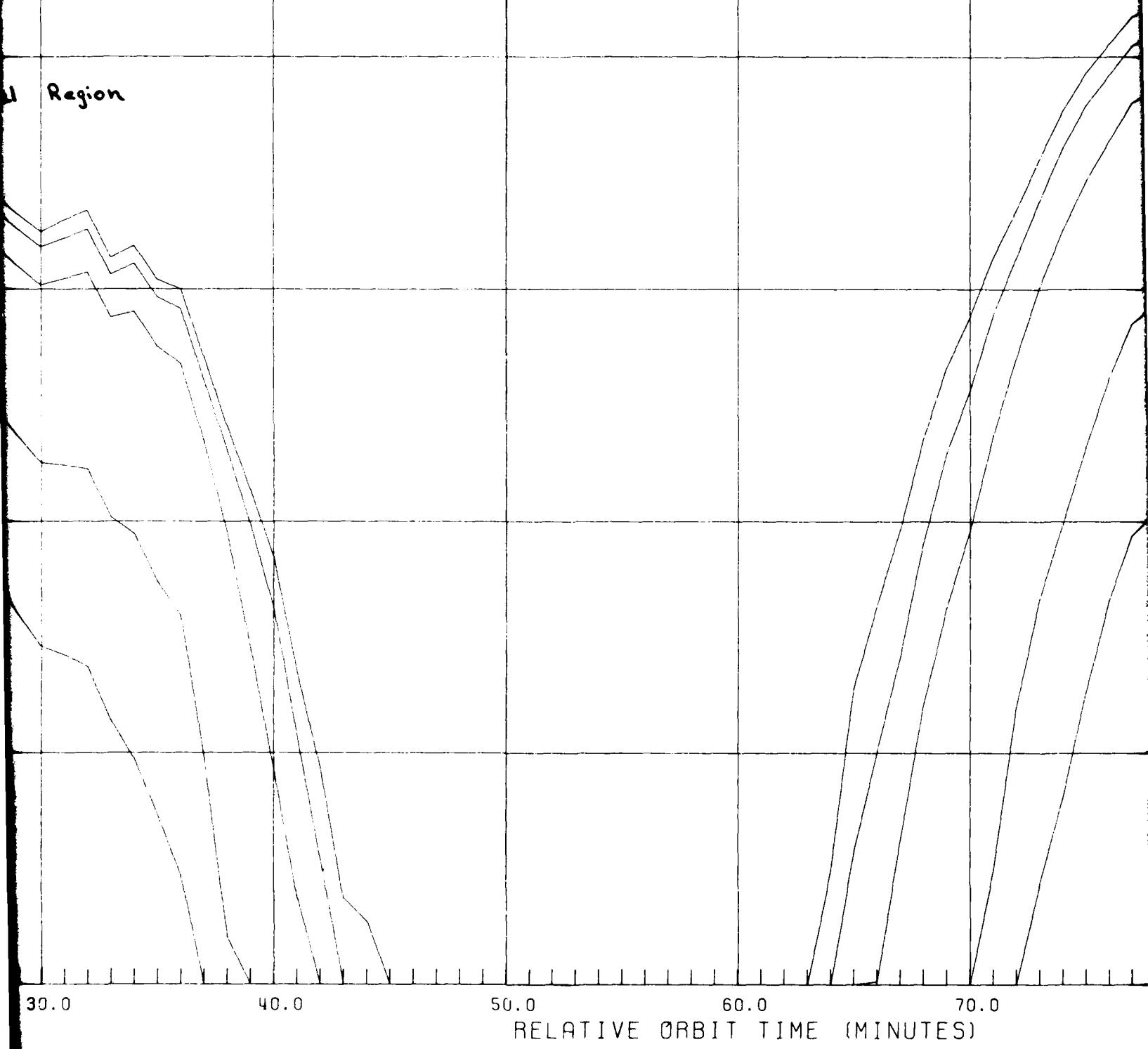


Figure 102





Region



ORBIT: NAVELEX 1
60 DGR/1667-1667 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 L

MISSION DURATION: 60.00

EVALUATION PHASE: SOLAR

UN FACTORS: NOT APPLIED

Equatorial Region

SAA

STOP TIME ON TAPE= 8.441

NAS

70.0

80.0

90.0

100.0

110.0

MINUTES)

Figure 103

ORBIT: NAVELEX 1
60 DGR/1667-1667 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

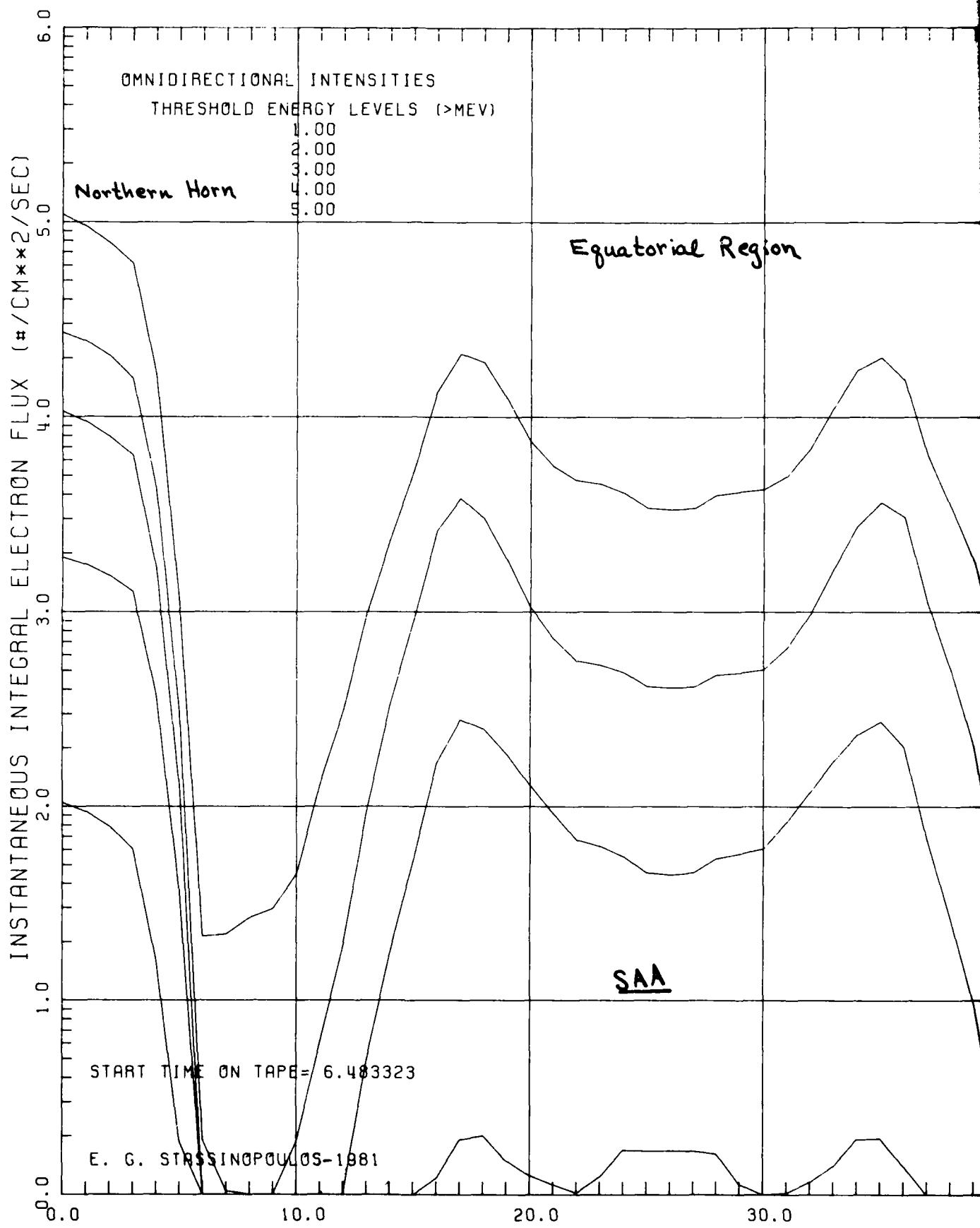
STOP TIME ON TAPE = 8.449993

NASA-GSFC

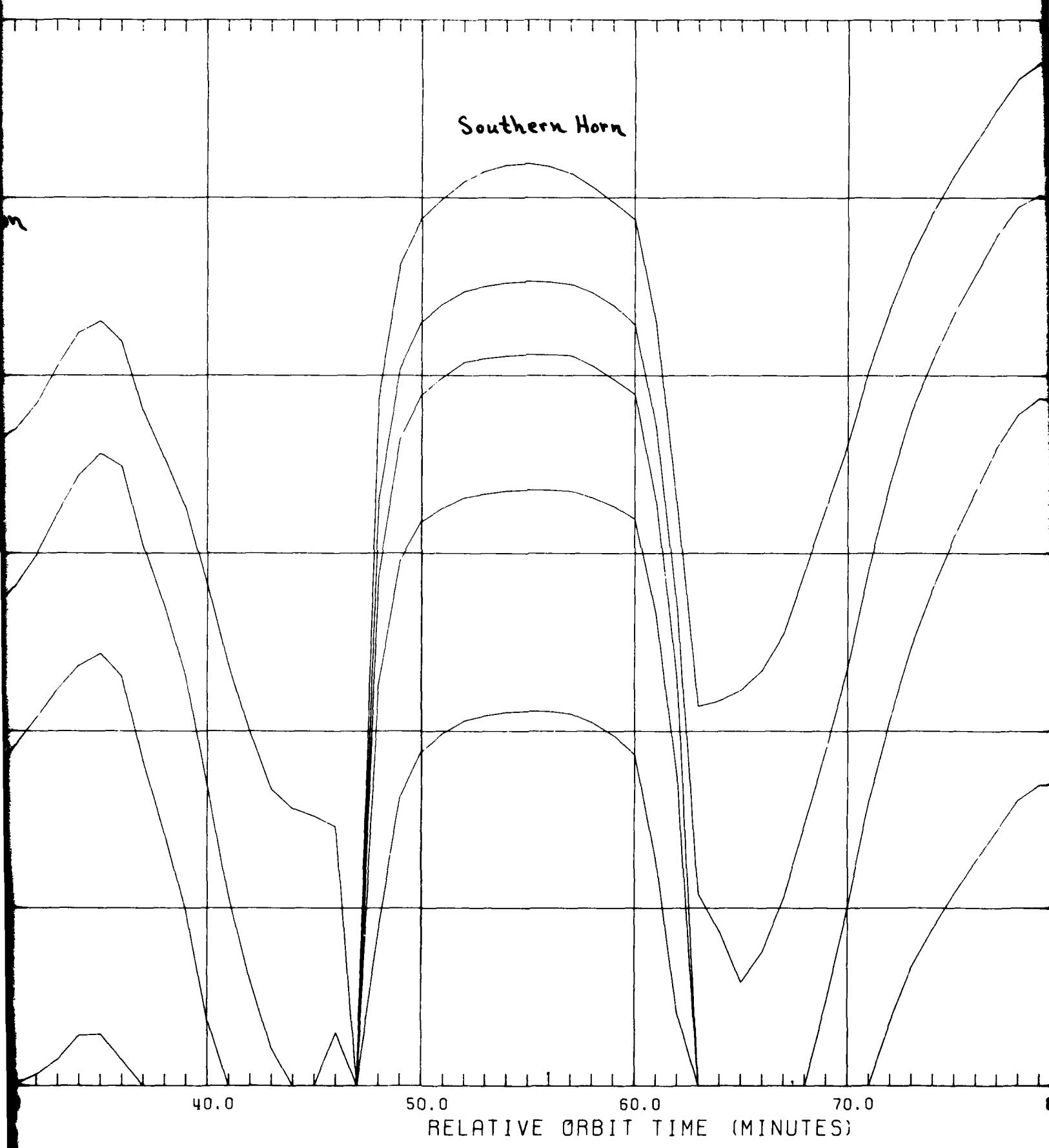
100.0

110.0

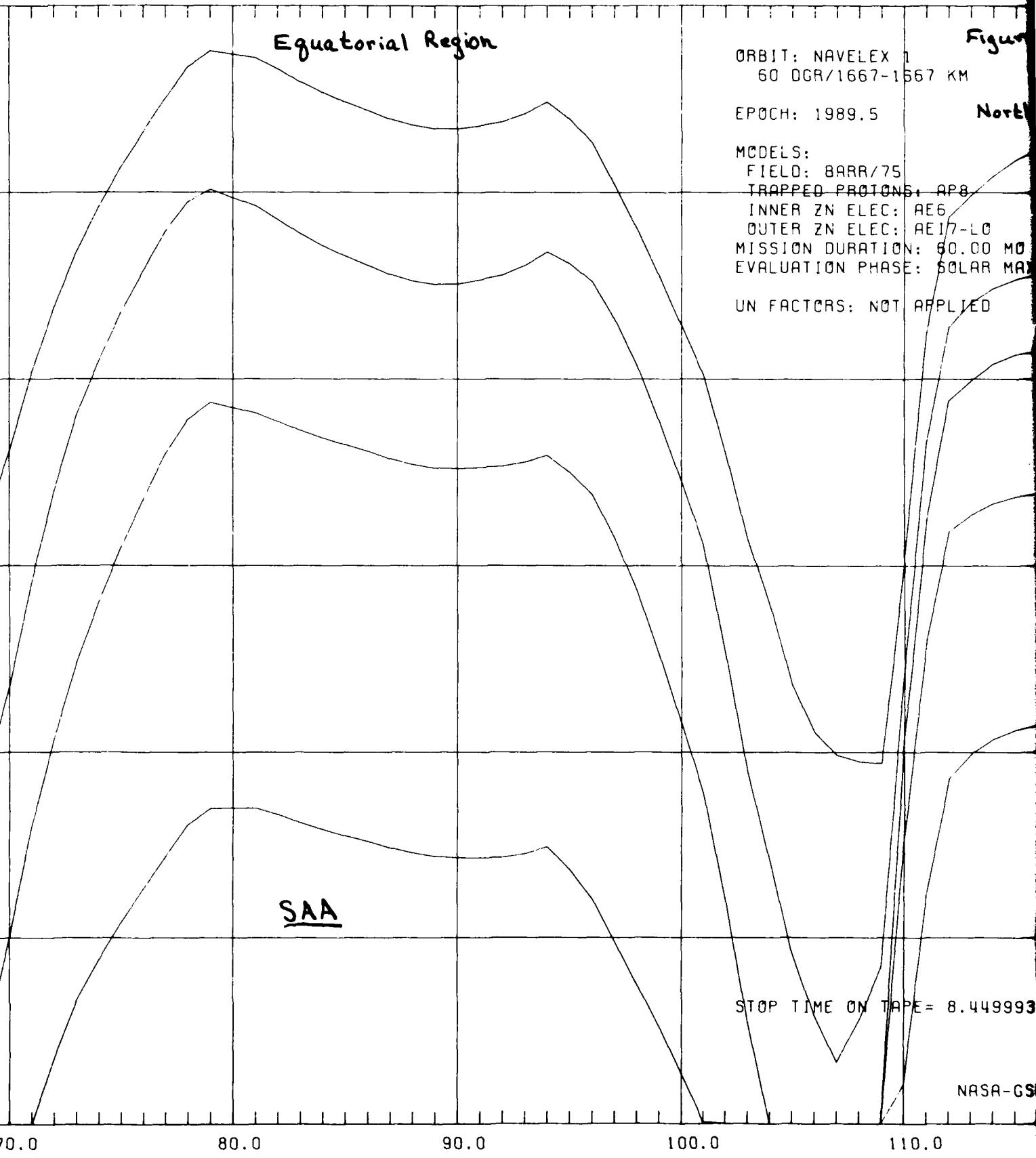
120.0



Southern Horn



Figure



MINUTES)

Figure 104

ORBIT: NAVELEX 1
60 DGR/1667-1567 KM

EPOCH: 1989.5

Northern Horn

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

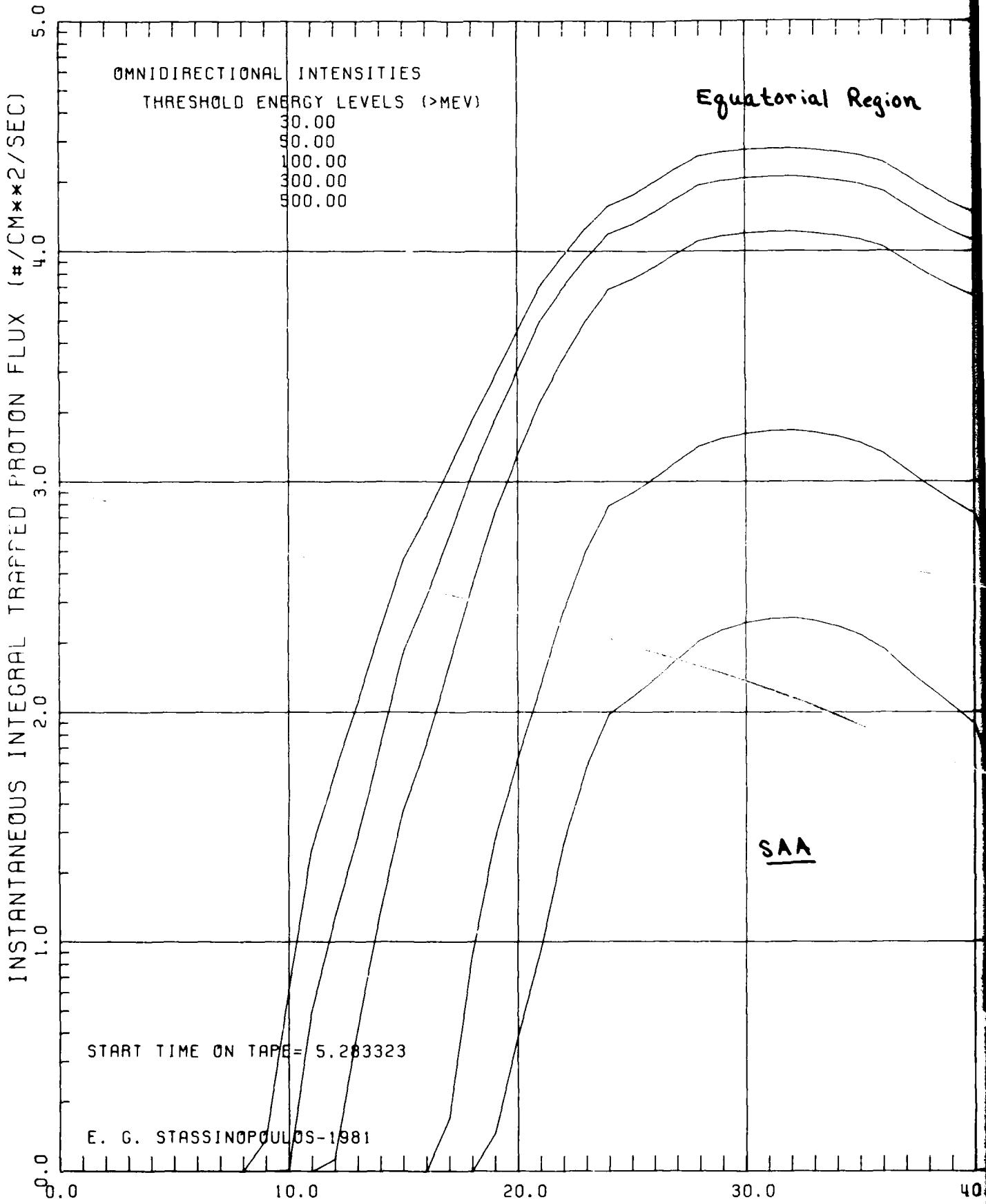
STOP TIME ON TAPE = 8.449993

NASA-GSFC

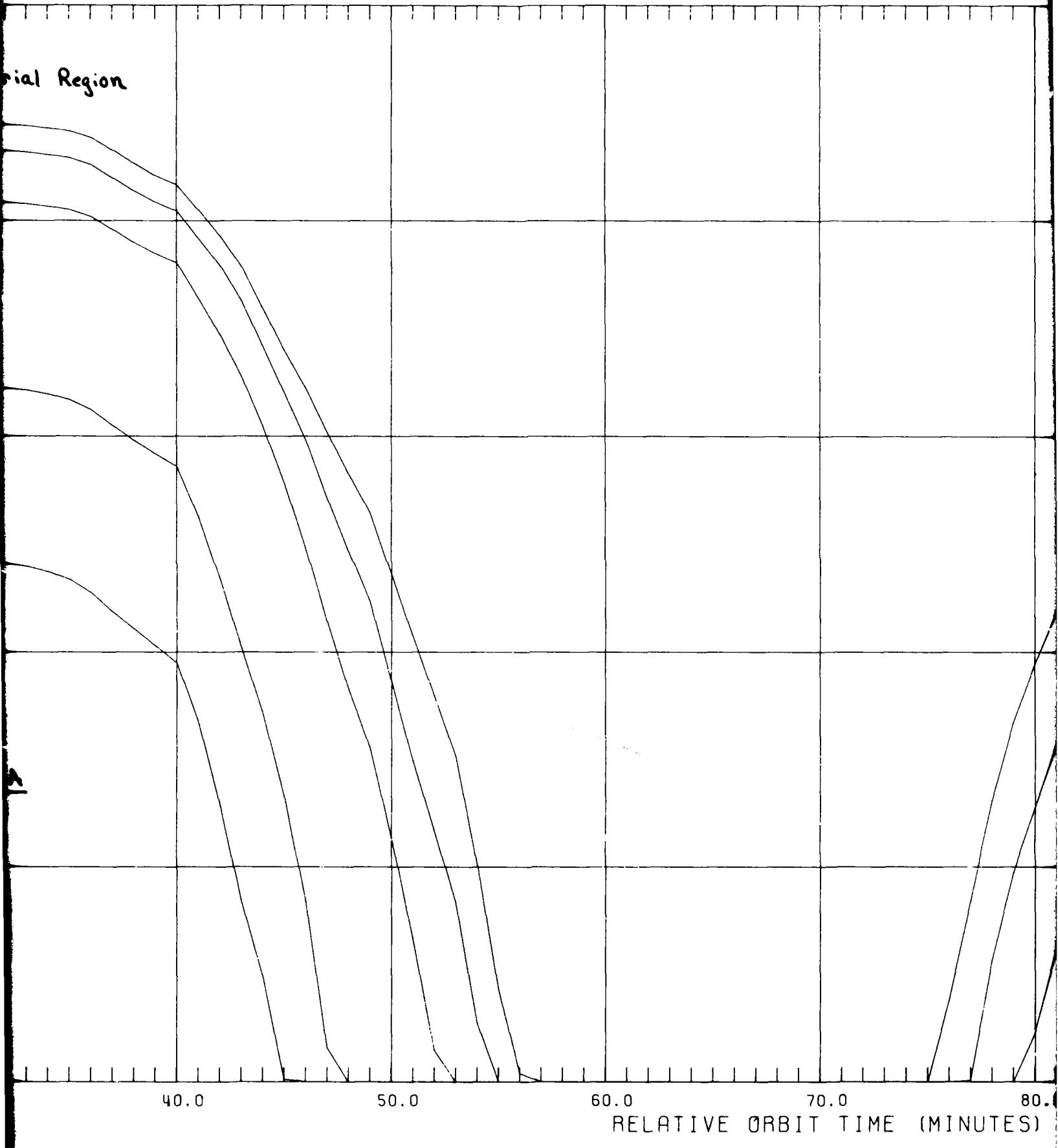
100.0

110.0

120.0



rial Region



Equatorial Region

SAA

ME (MINUTES)

80.0

90.0

100.0

110.0

120

region

Figure 105

ORBIT: NAVELEX 2
60 DGR/2593-2593 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

STOP TIME ON TAPE = 7.616656

NASA-GSFC

10.0 120.0 130.0 140.0

AD-A141 849 ORBITAL RADIATION STUDY FOR INCLINED CIRCULAR
TRAJECTORIES(U) NATIONAL AERONAUTICS AND SPACE
ADMINISTRATION GREENBELT MD GO.. E G STASSINOPoulos

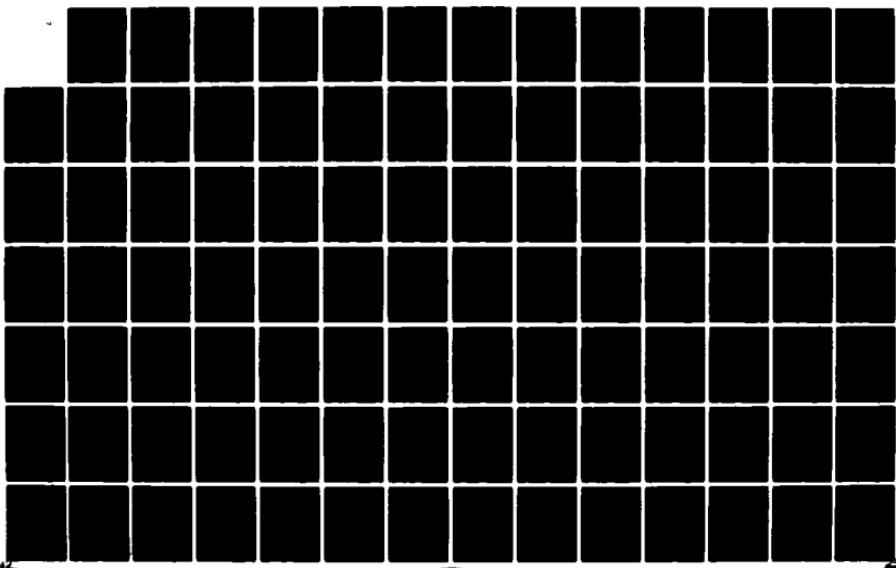
NOV 81 NASA-GSFC-X-601-81-28

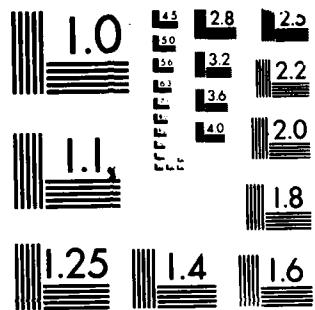
F/G 22/3

UNCLASSIFIED

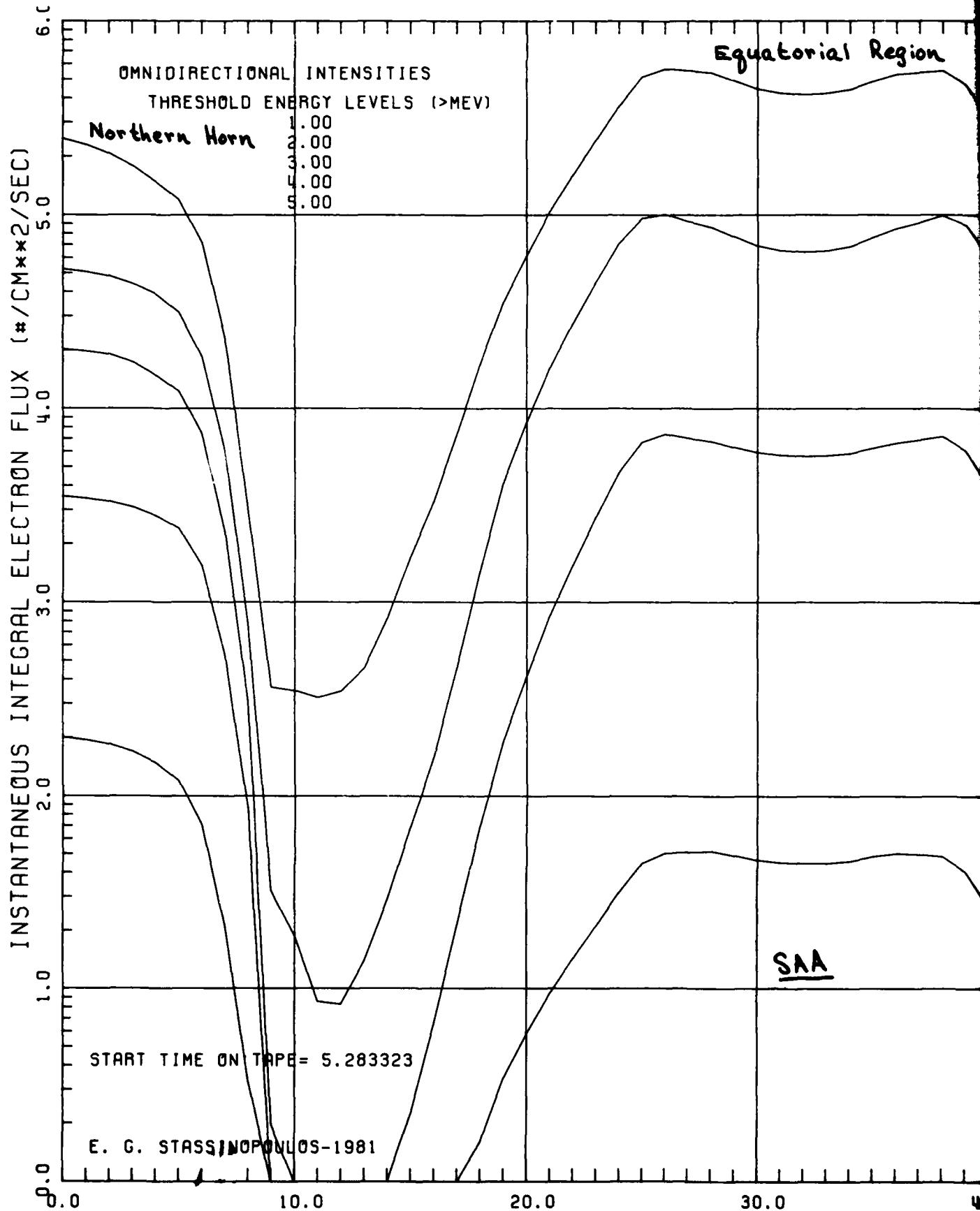
3/ S

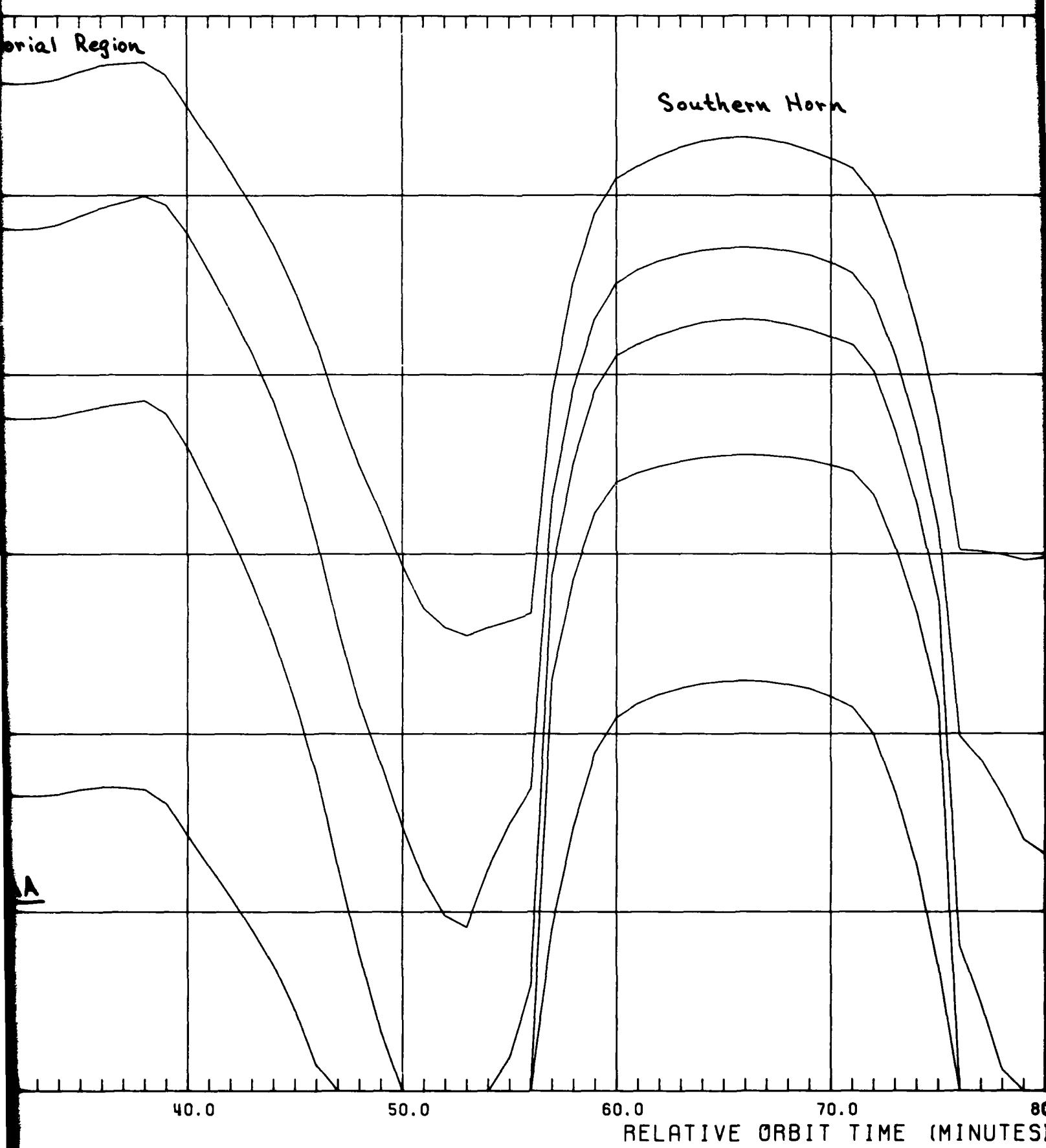
NL





MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

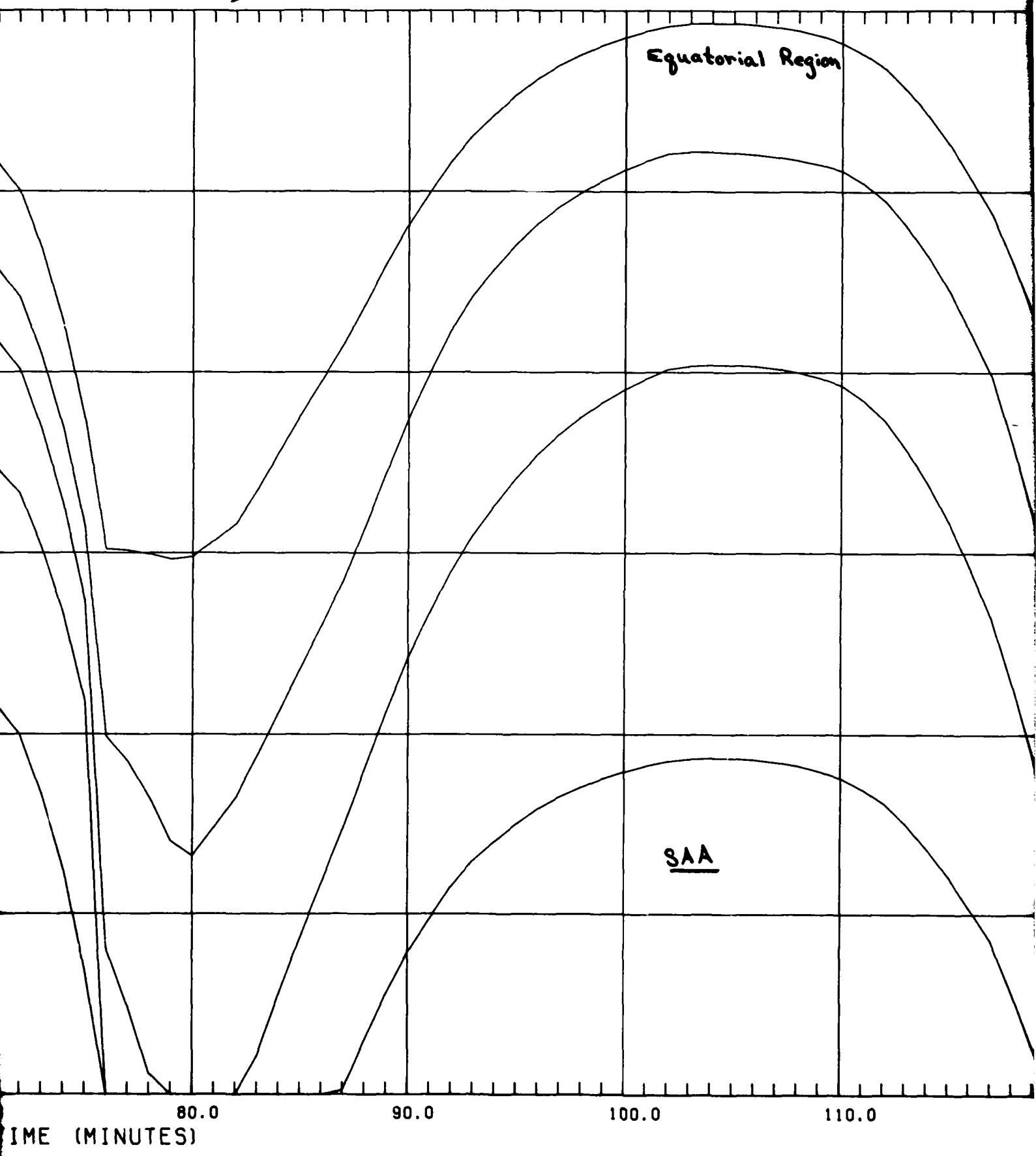




3

Equatorial Region

SAA



4

region

ORBIT: NAVELEX 2
60 DGR/2593-2593 KM

Figure 106

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern Horn

STOP TIME ON TAPE= 7.616656

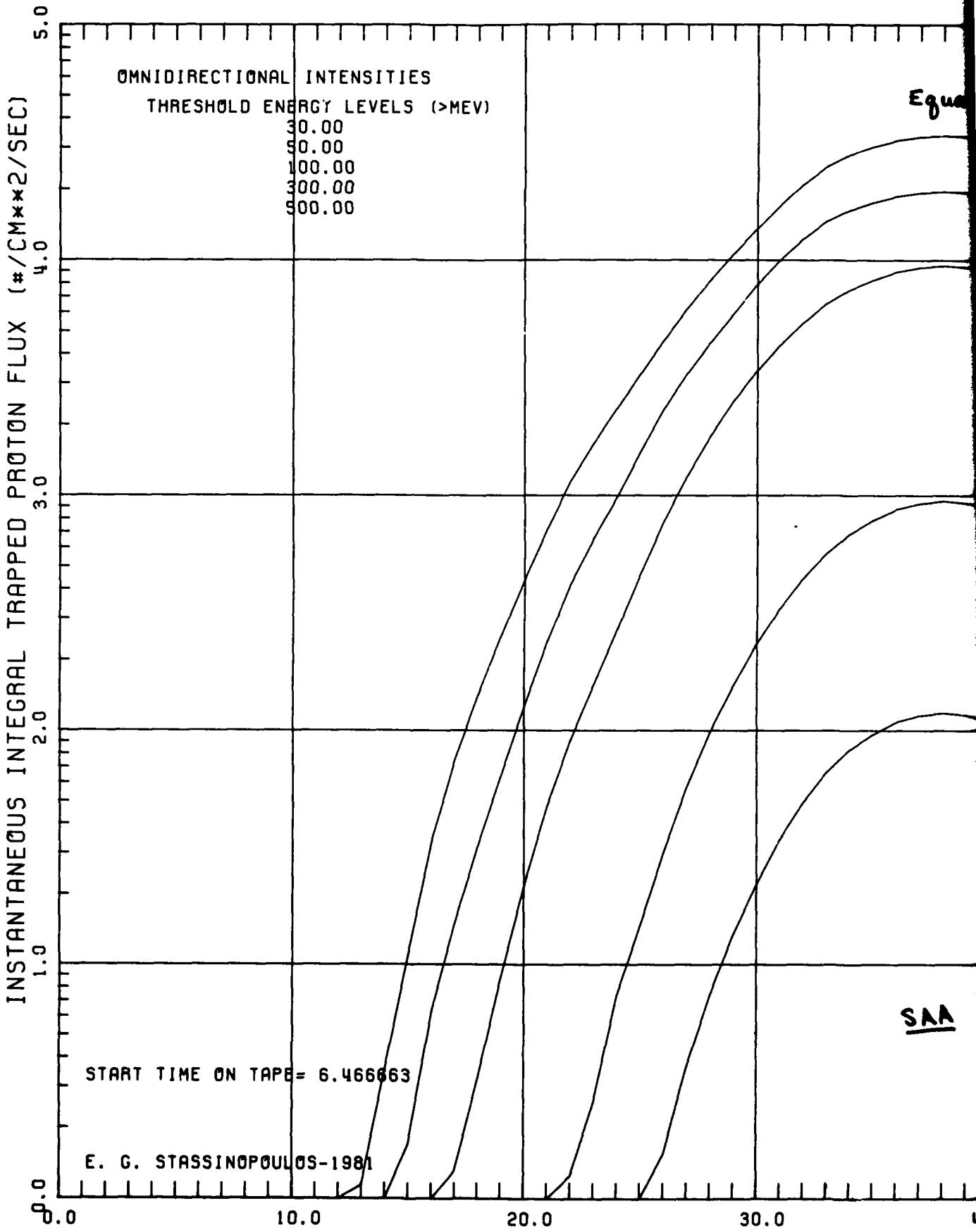
NASA-GSFC

110.0

120.0

130.0

140.0



1
2

Equatorial Region

SAA

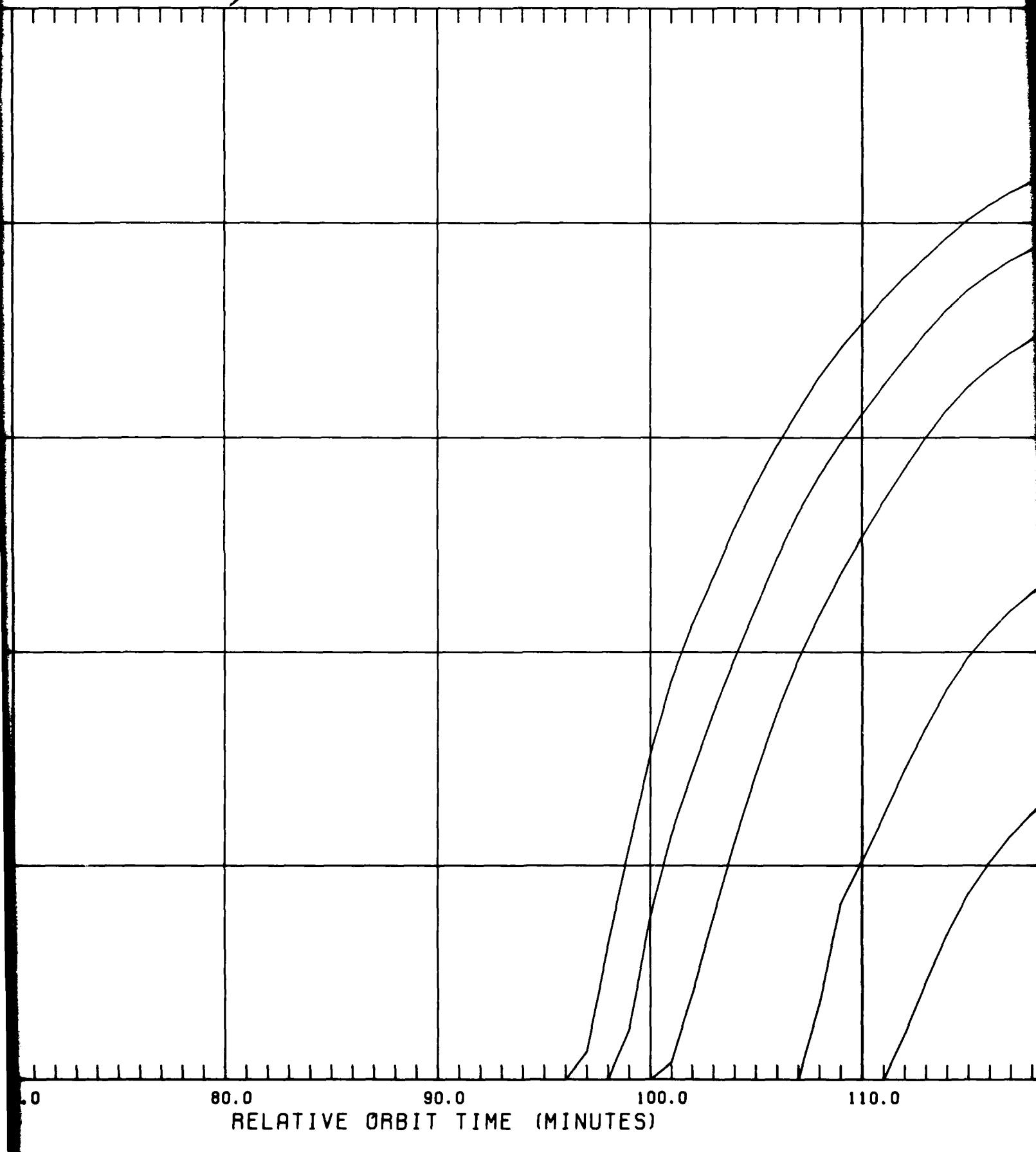
40.0

50.0

60.0

70.0

3



'4

Equatorial Region

SAA

0

120.0

130.0

140.0

150.0

5

Figure 107

ORBIT: NAVELEX 3
60 DGR/3889-3889 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AEI7 L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

STOP TIME ON TAPE= 9.316662

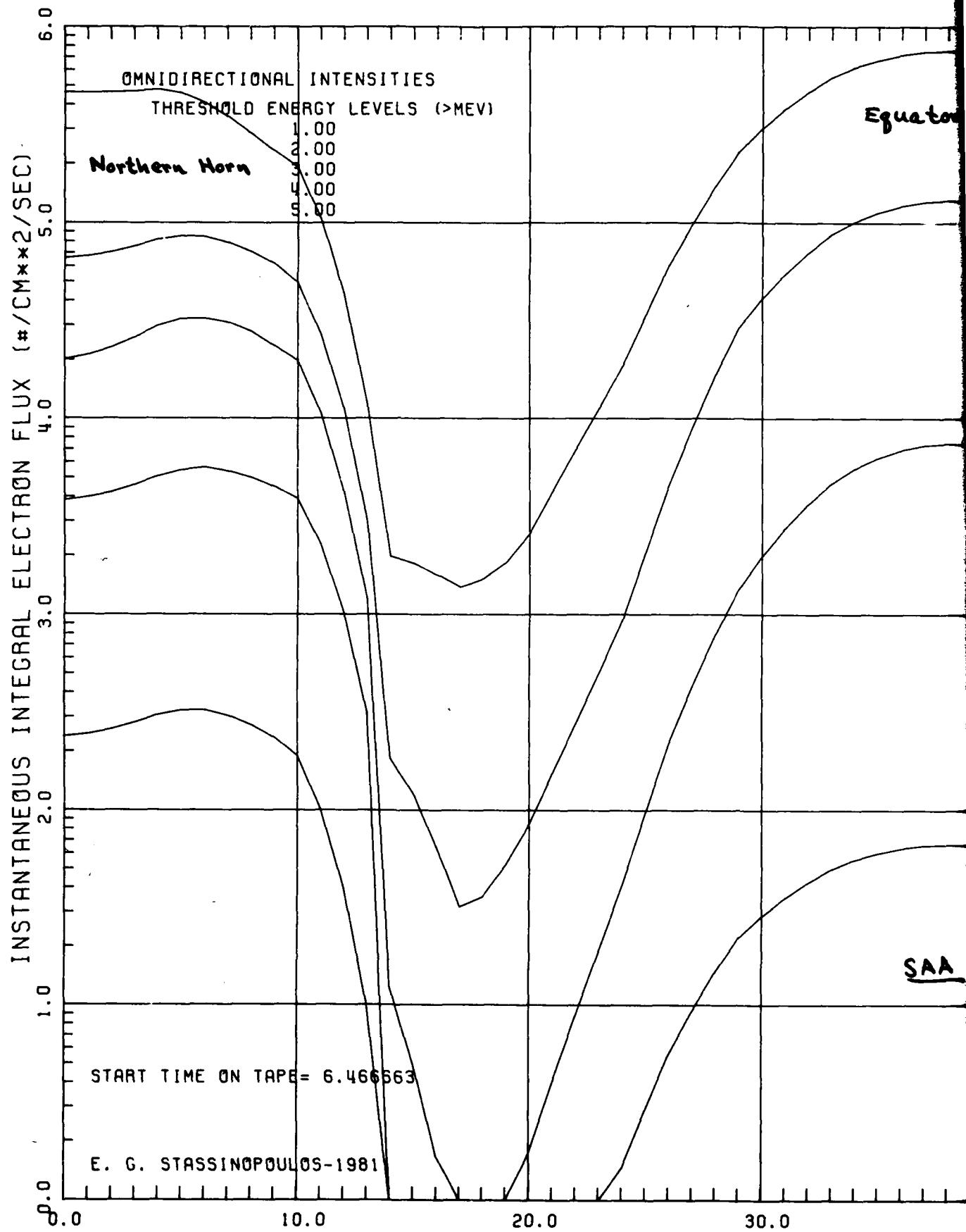
NASA-GSFC

150.0

160.0

170.0

180.0



12

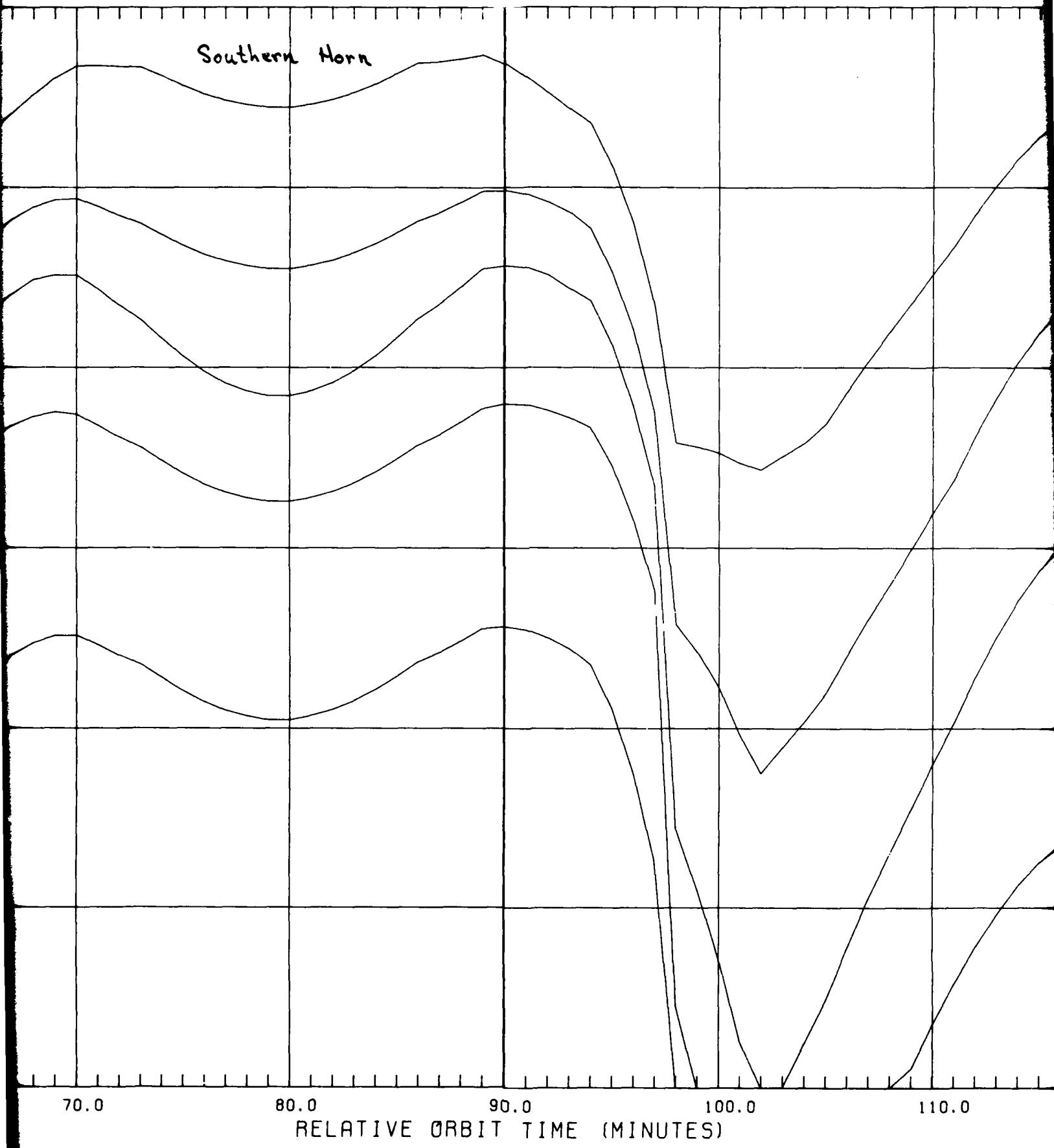
Equatorial Region

SAA

30.0 40.0 50.0 60.0 70.0

13

Southern Horn



1 4

Nov

Equatorial Region

SAA

110.0 120.0 130.0 140.0 150.0

5

Northern Horn

Figure 108

ORBIT: NAVELEX 3
60 DGR/3889-3889 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AEI7-L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

STOP TIME ON TAPE= 9.316662

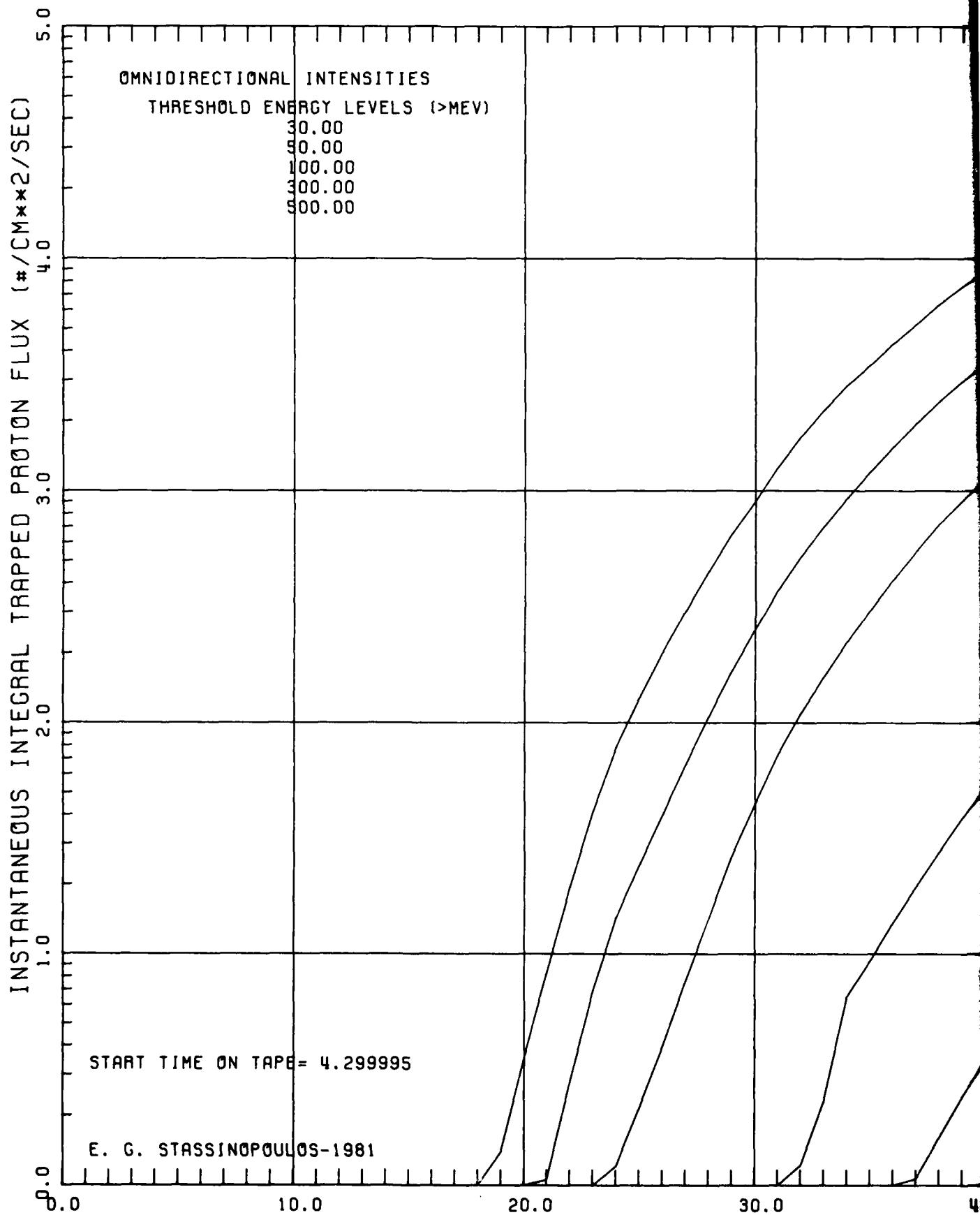
NASA-GSFC

150.0

160.0

170.0

180.0



2

Equatorial Region

SAA

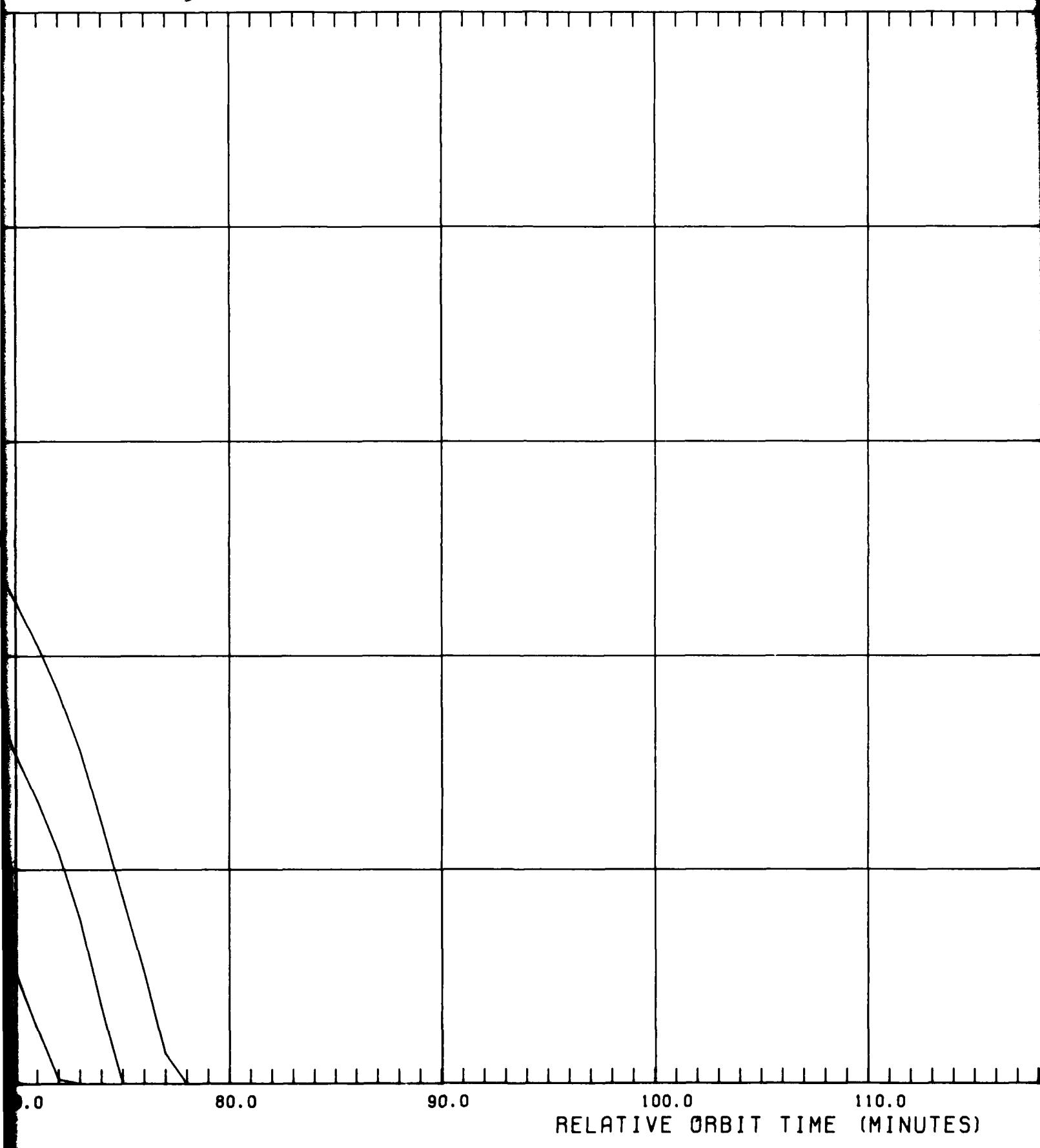
40.0

50.0

60.0

70.0

3



4'

Equatorial

SAA

10.0
(MINUTES)

120.0

130.0

140.0

150.0

5.

ORBIT: NAV
60 DGR/

EPOCH: 190

MODELS:
FIELD: BR
TRAPPED P
INNER ZN
OUTER ZN
MISSION DU
EVALUATION

UN FACTORS

Equatorial Region

SAA

STOP TIME

50.0

160.0

170.0

180.0

190.0

Figure 109

ORBIT: NAVELEX
60 DGR/5186-5186 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-L6

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

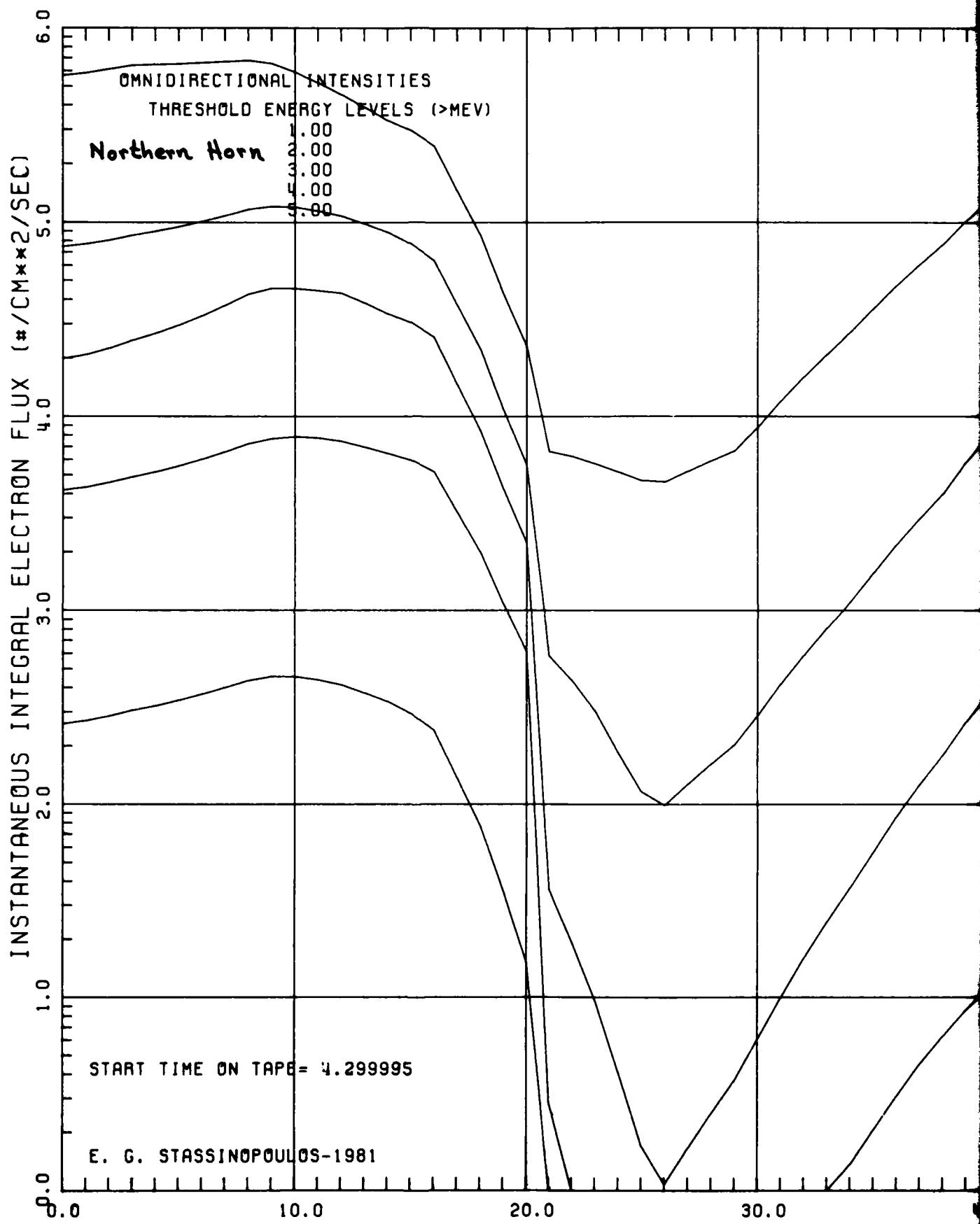
STOP TIME ON TAPE= 7.716662

NASA-GSFC

190.0

200.0

210.0



2

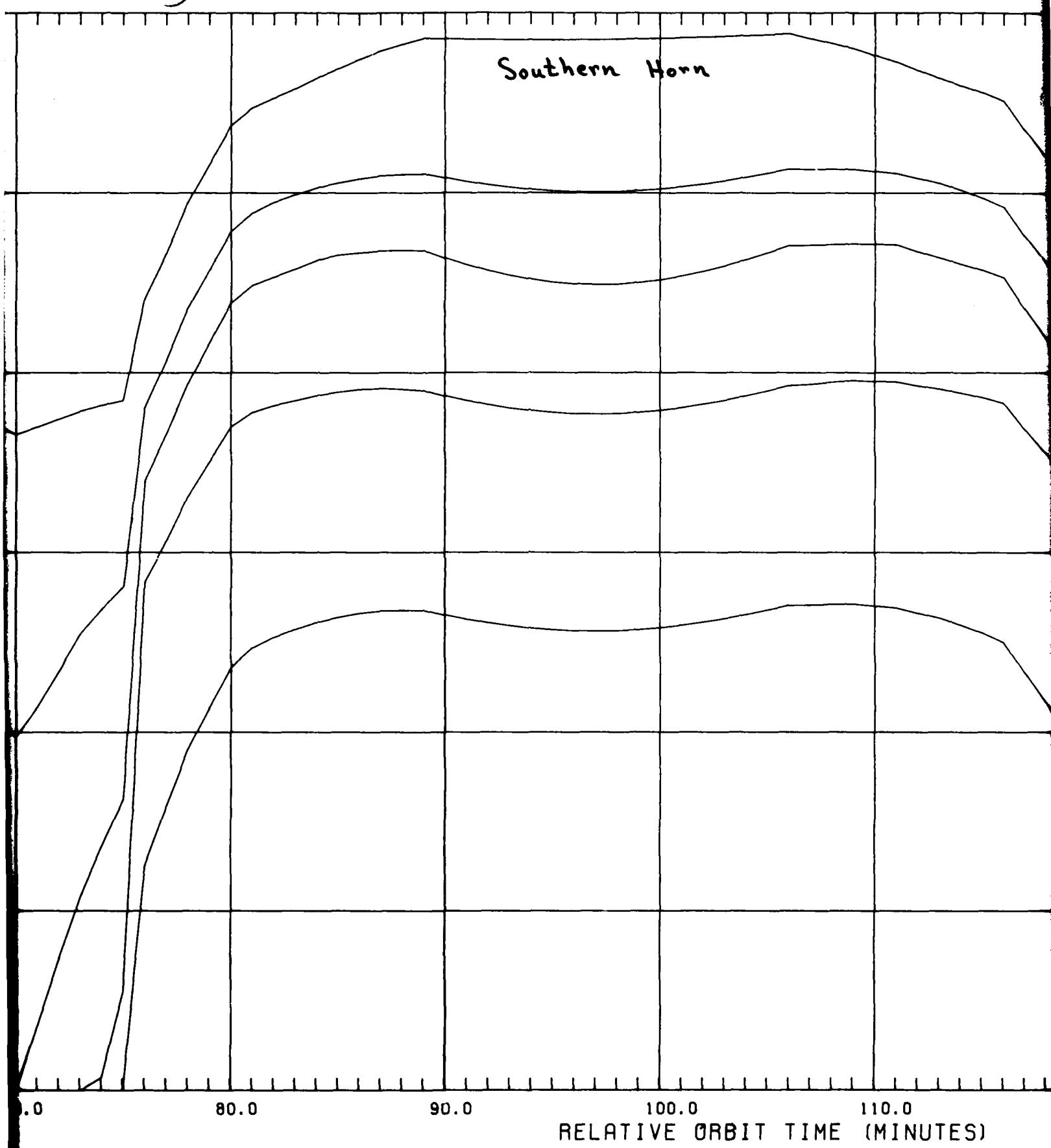
Equatorial Region

SAA



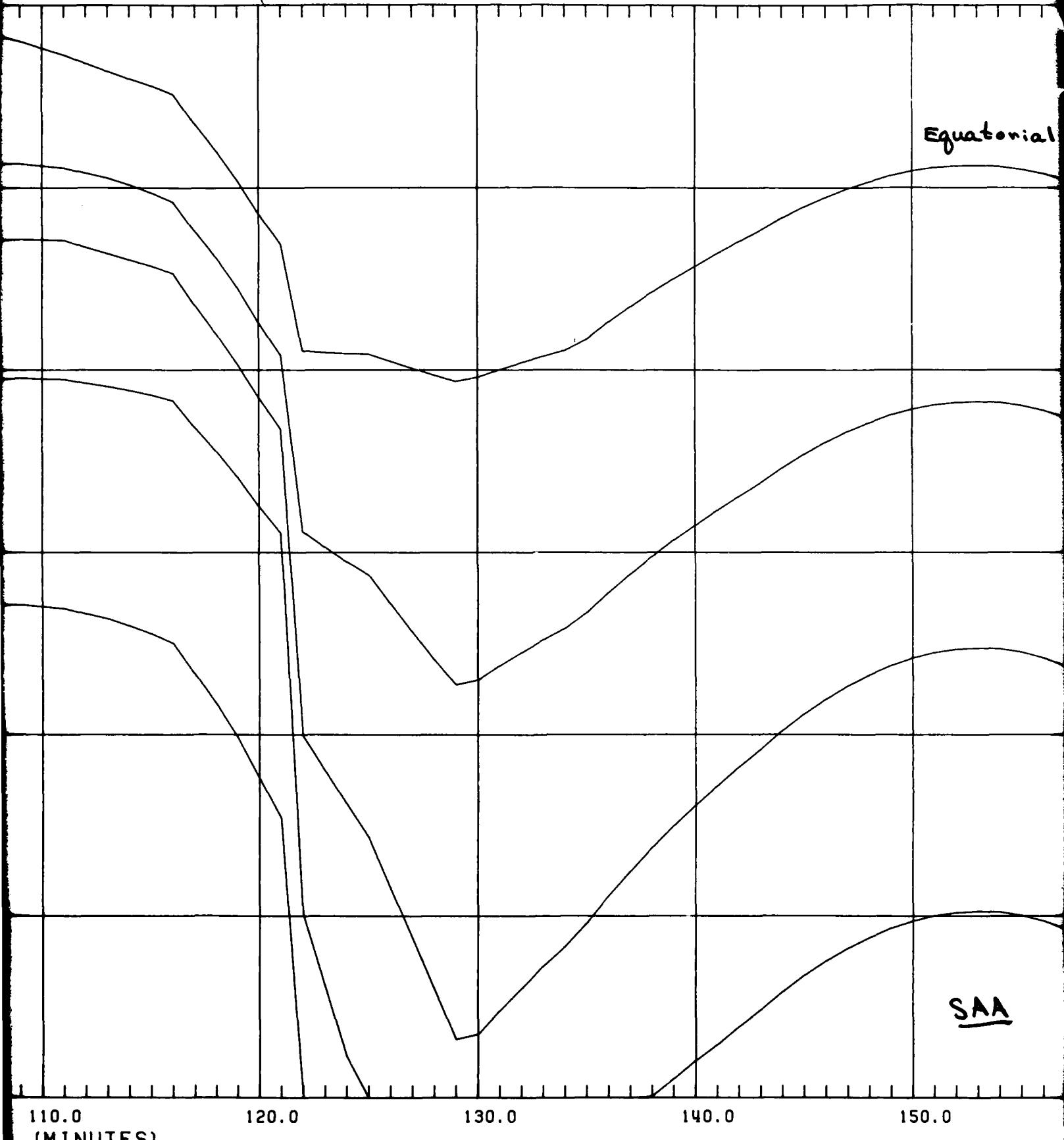
3

Southern Horn



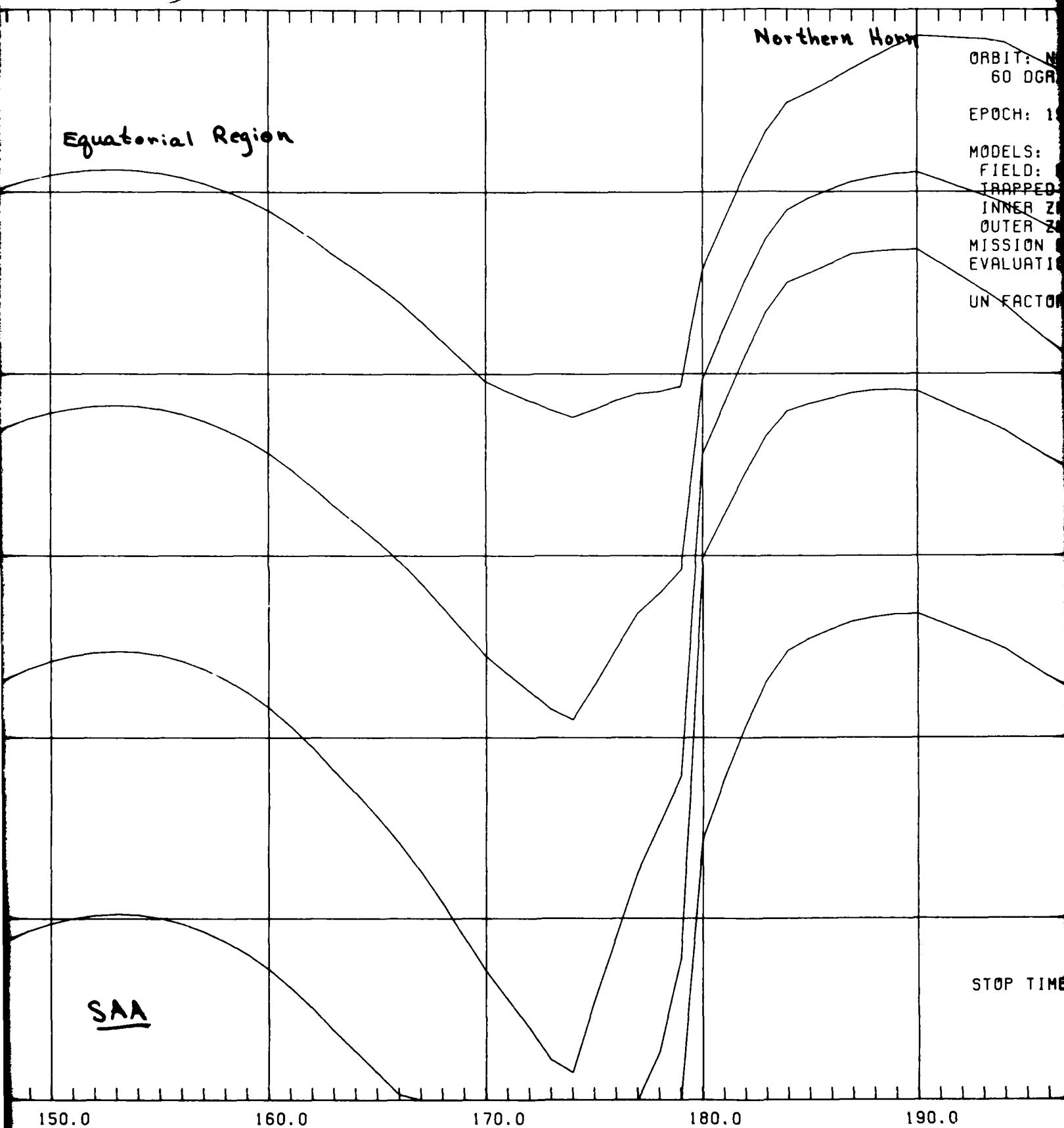
4
Equatorial

SAA



110.0
(MINUTES)

120.0 130.0 140.0 150.0



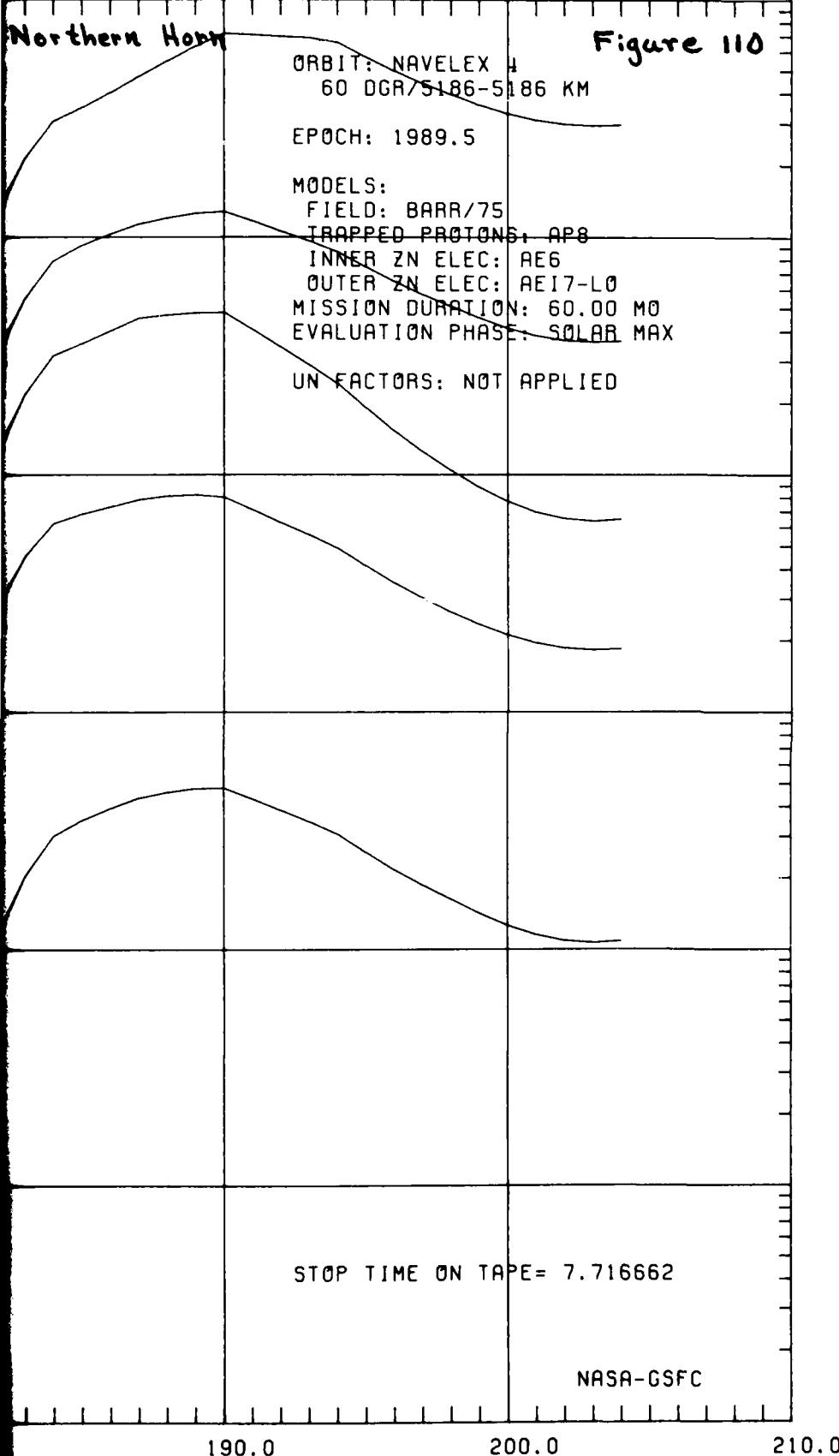
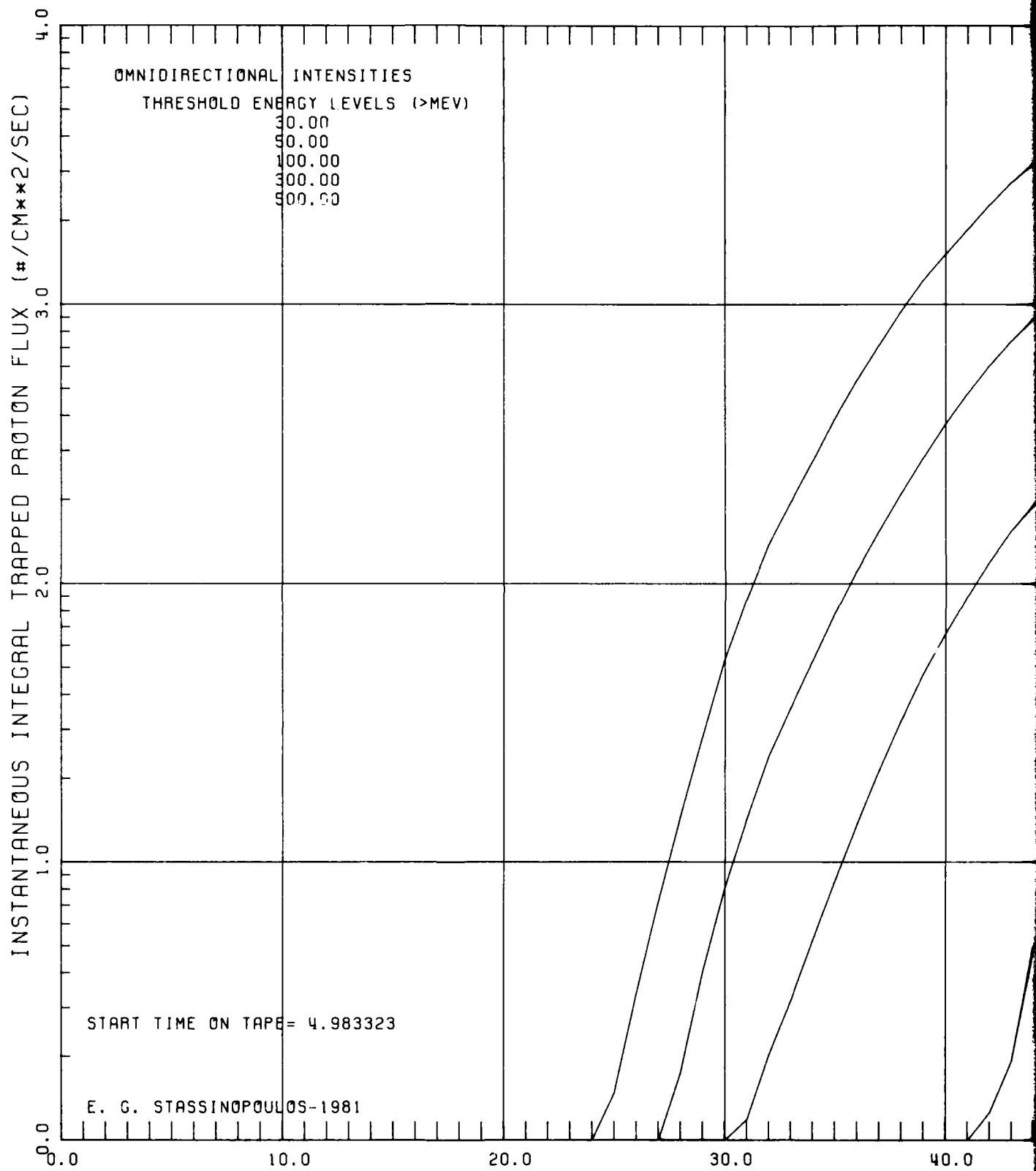


Figure 110



2'

Equatorial Region

SAA

40.0

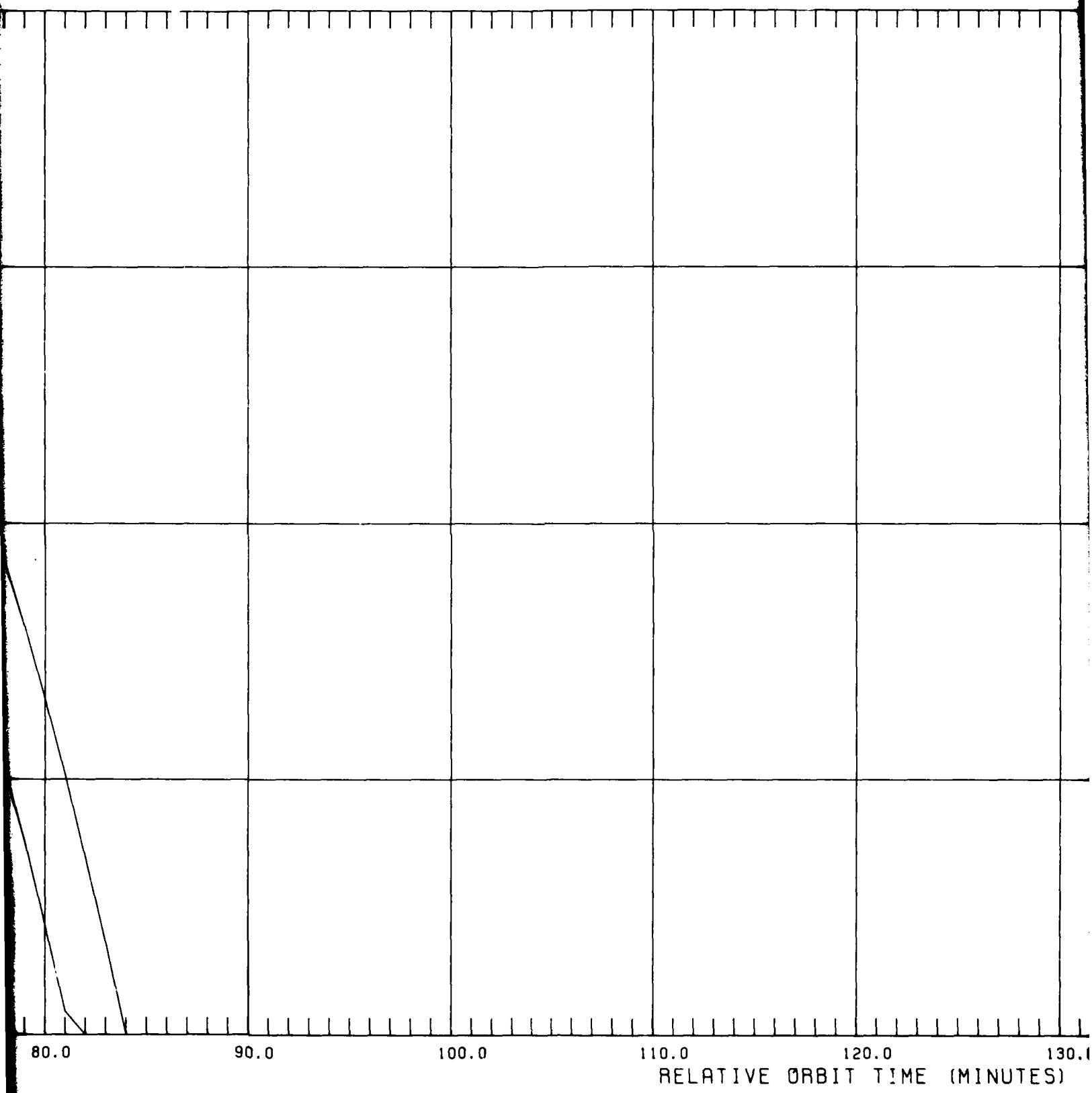
50.0

60.0

70.0

80.0

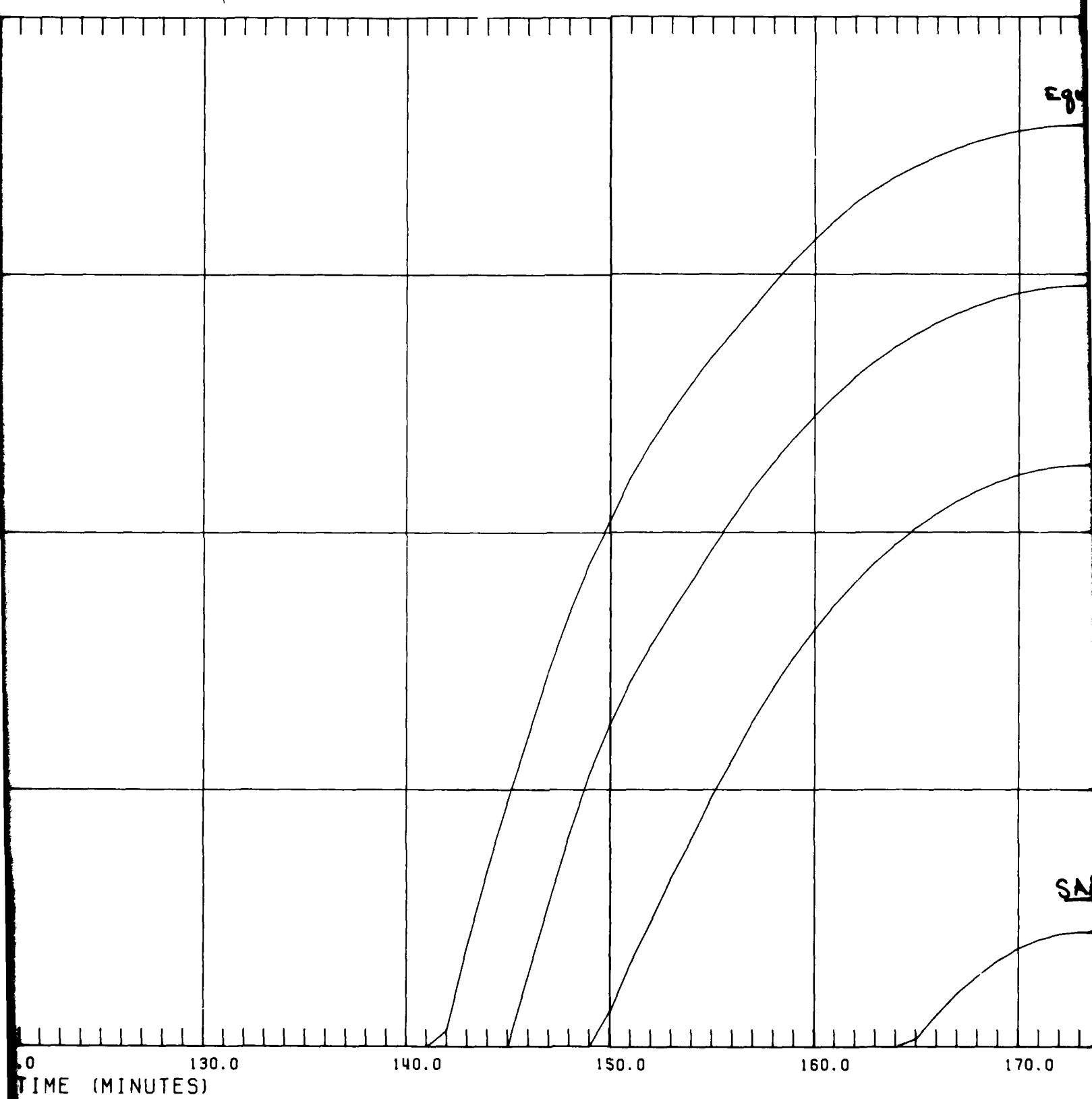
3'



4

Ego

SN



S'

Equatorial Region

SAA

170.0

180.0

190.0

200.0

210.0

6
Figure III

ORBIT: NAVELEX 5
60 DGR/6389-6389 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AEG
OUTER ZN ELEC: AEI7-L0
MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

STOP TIME ON TAPE= 8.933318

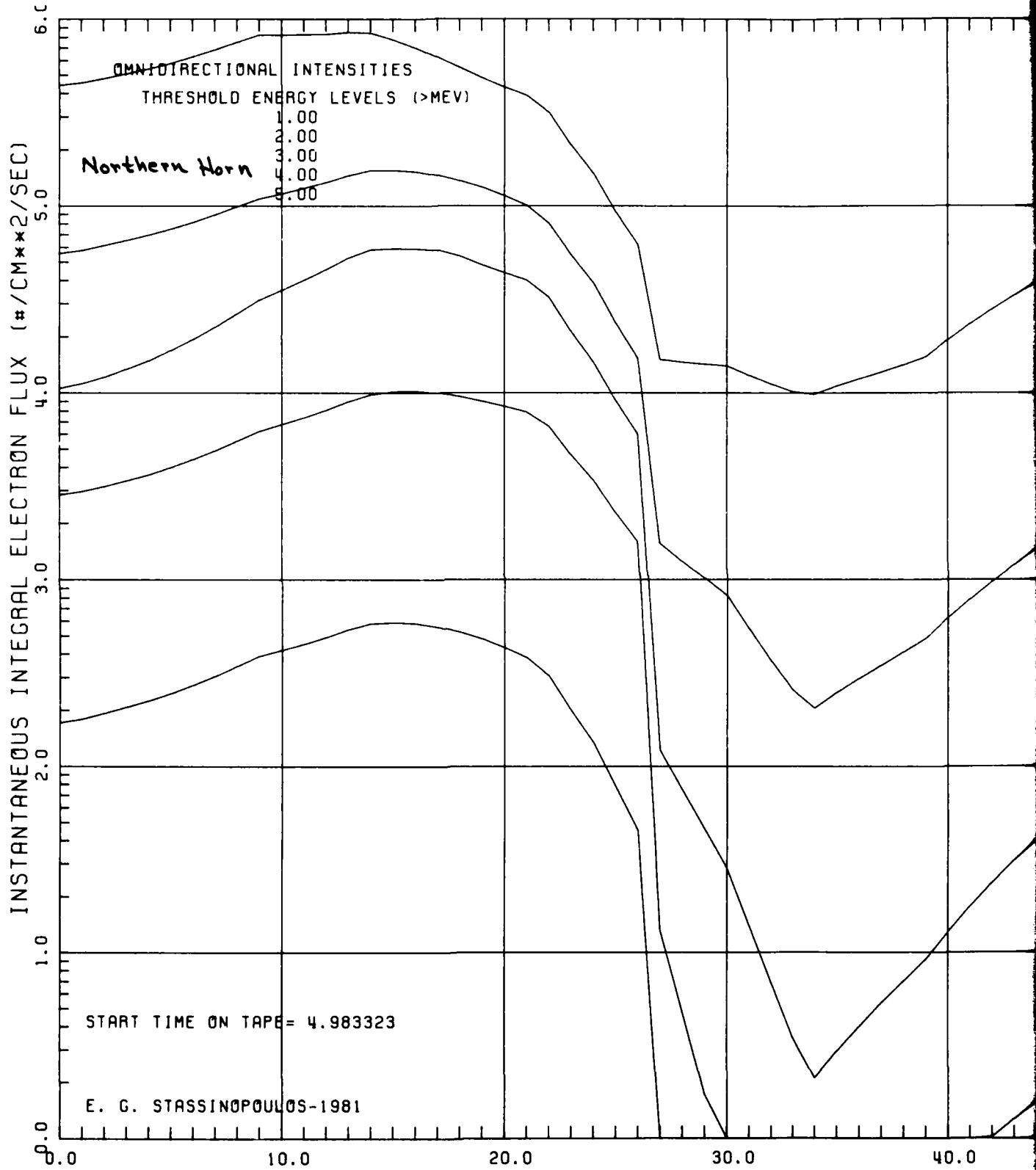
NASA-GSFC

210.0

220.0

230.0

240.0



2

Equatorial Region

SAA

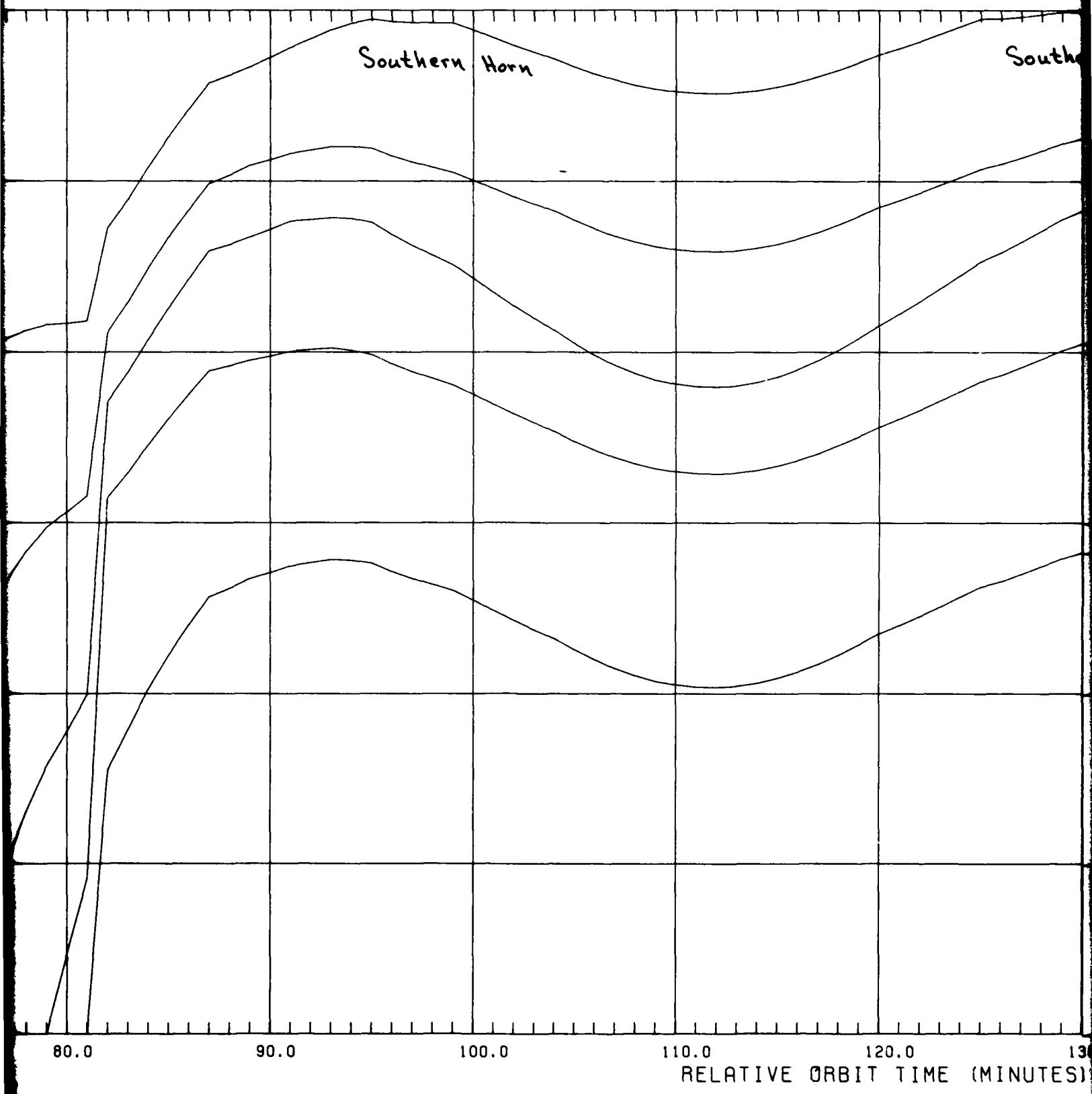
40.0

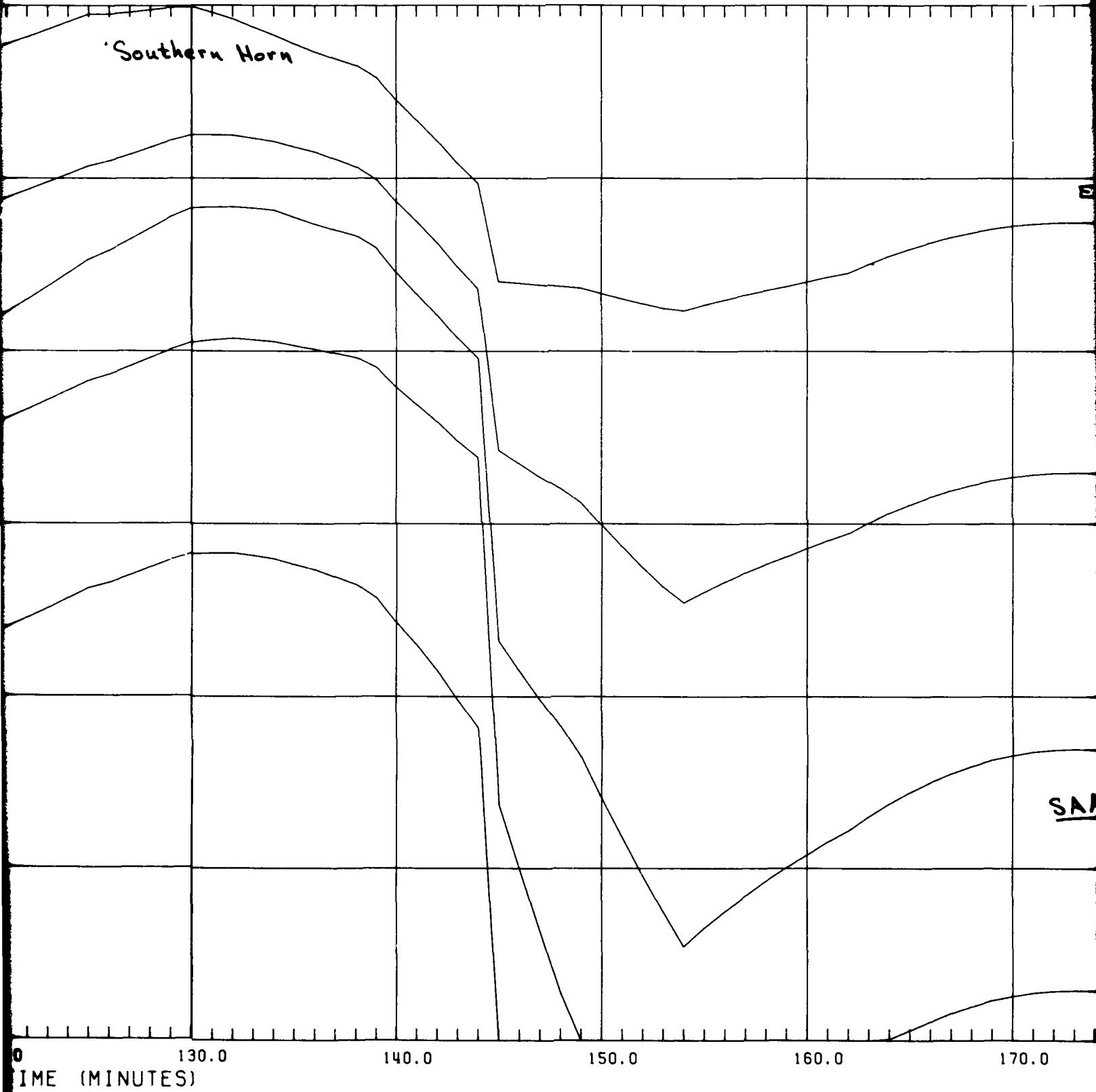
50.0

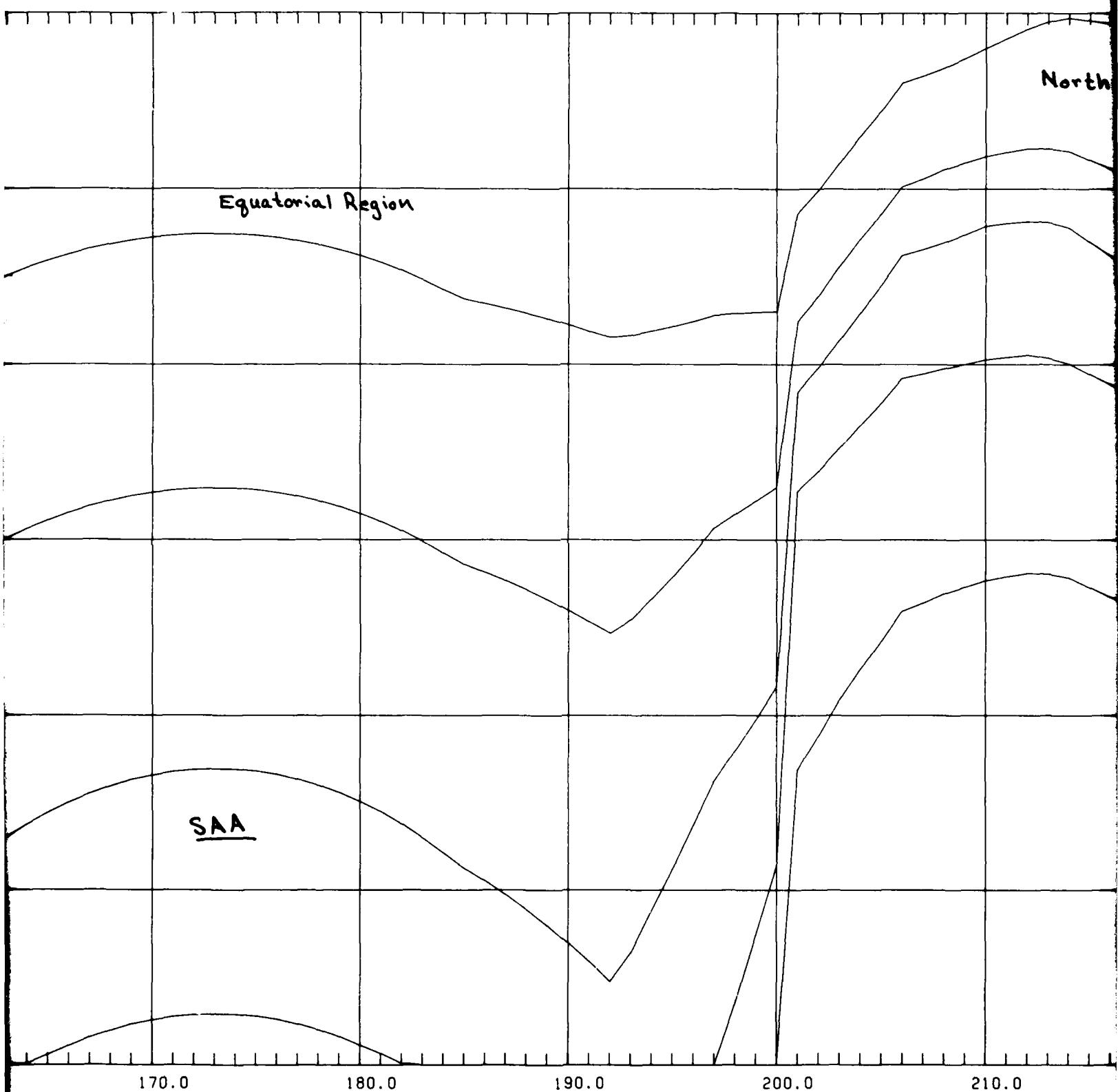
60.0

70.0

80.0







Northern Horn

Figure 112

ORBIT: NAVELEX 5
60 DGR/6389-6389 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-L0

MISSION DURATION: 60.00 MO

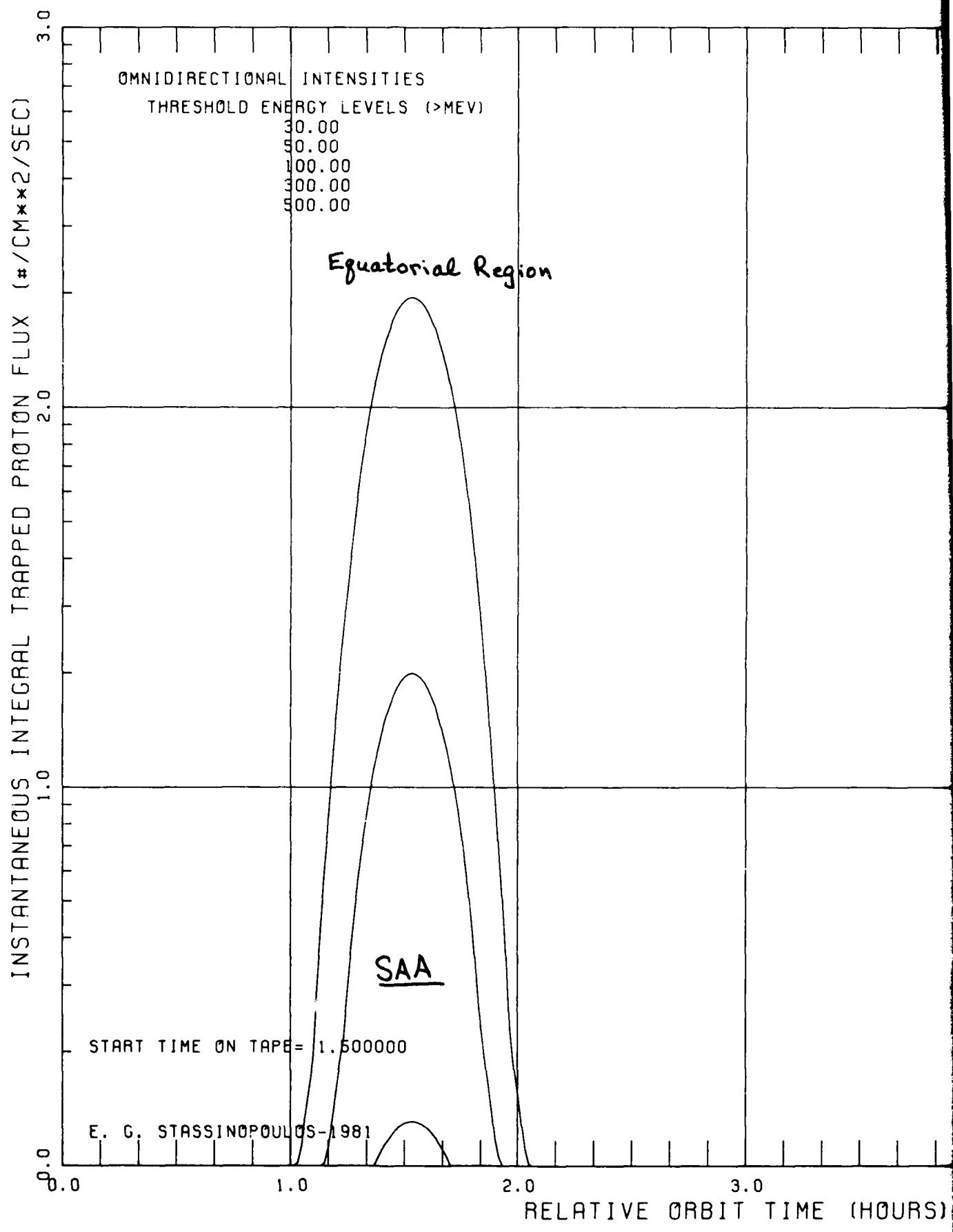
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

STOP TIME ON TAPE= 8.933318

NASA-GSFC

.0 210.0 220.0 230.0 240.0



ORBIT: NAVELEX 6
60 DGR/10371-10371 KM

Figure 113

EPOCH: 1989.5

MODELS:

FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AEI7-L0
MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Equatorial Region

SAA

STOP TIME ON TAPE = 7.483318

NASA-GSFC

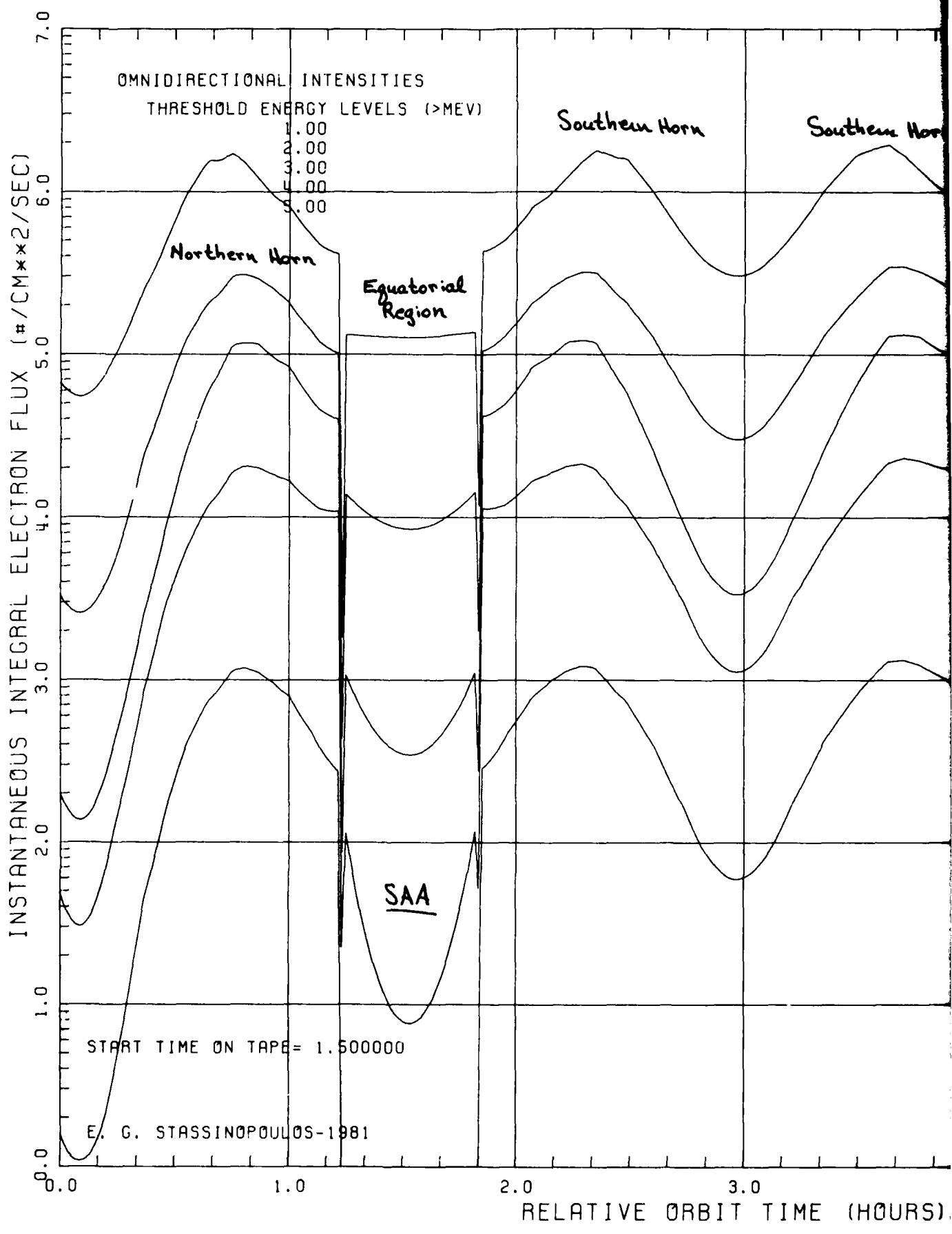
3.0

4.0

5.0

6.0

BIT TIME (HOURS)



2

Figure 114

ORBIT: NAVELEX 6
60 DGR/10371-10371 KM
EPOCH: 1989.5
MODELS:
FIELD: BARRH/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AE17-L0
MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX
UN FACTORS: NOT APPLIED

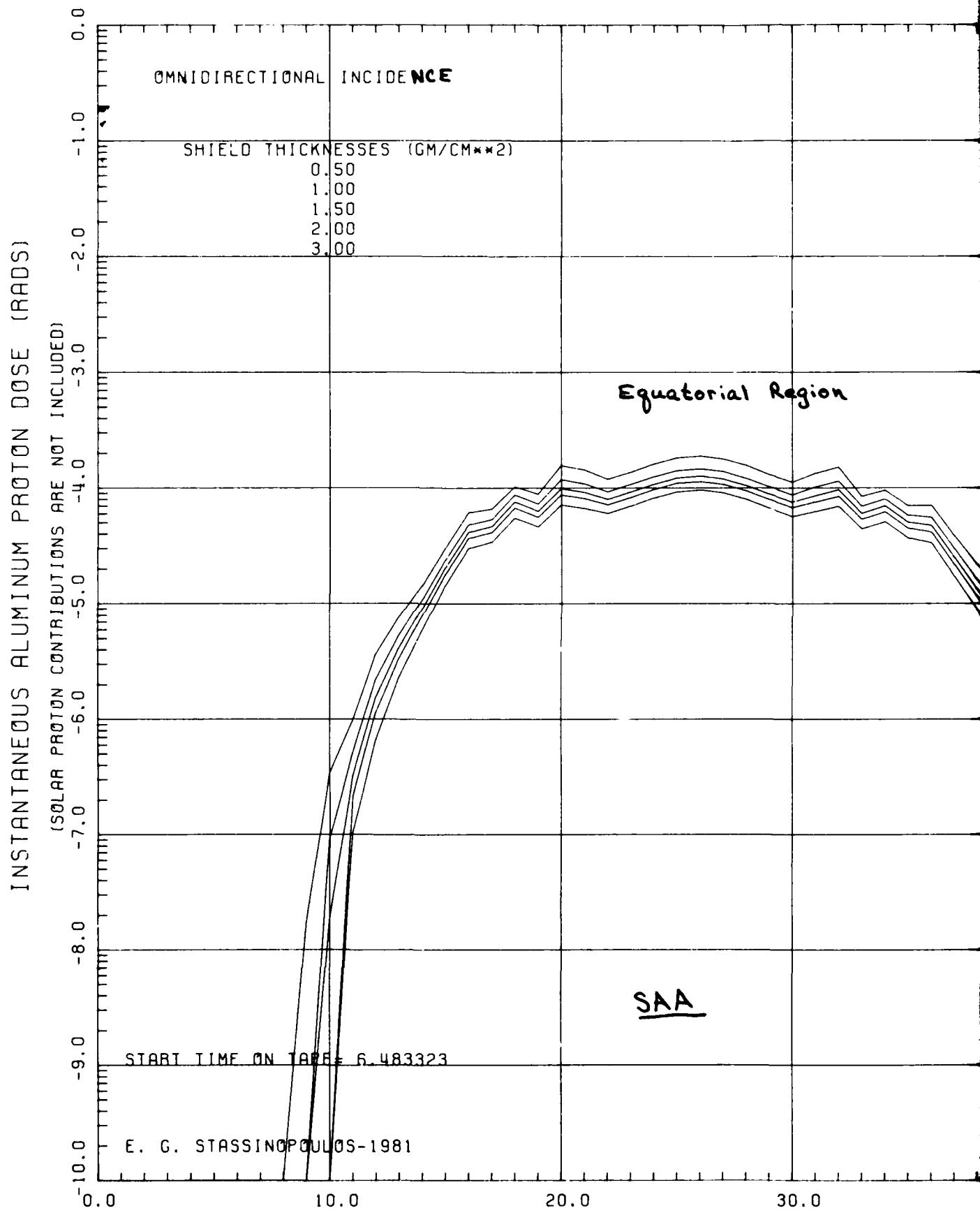
Equatorial Region

SAA

STOP TIME ON TAPE = 7.483318

NASA-GSFC

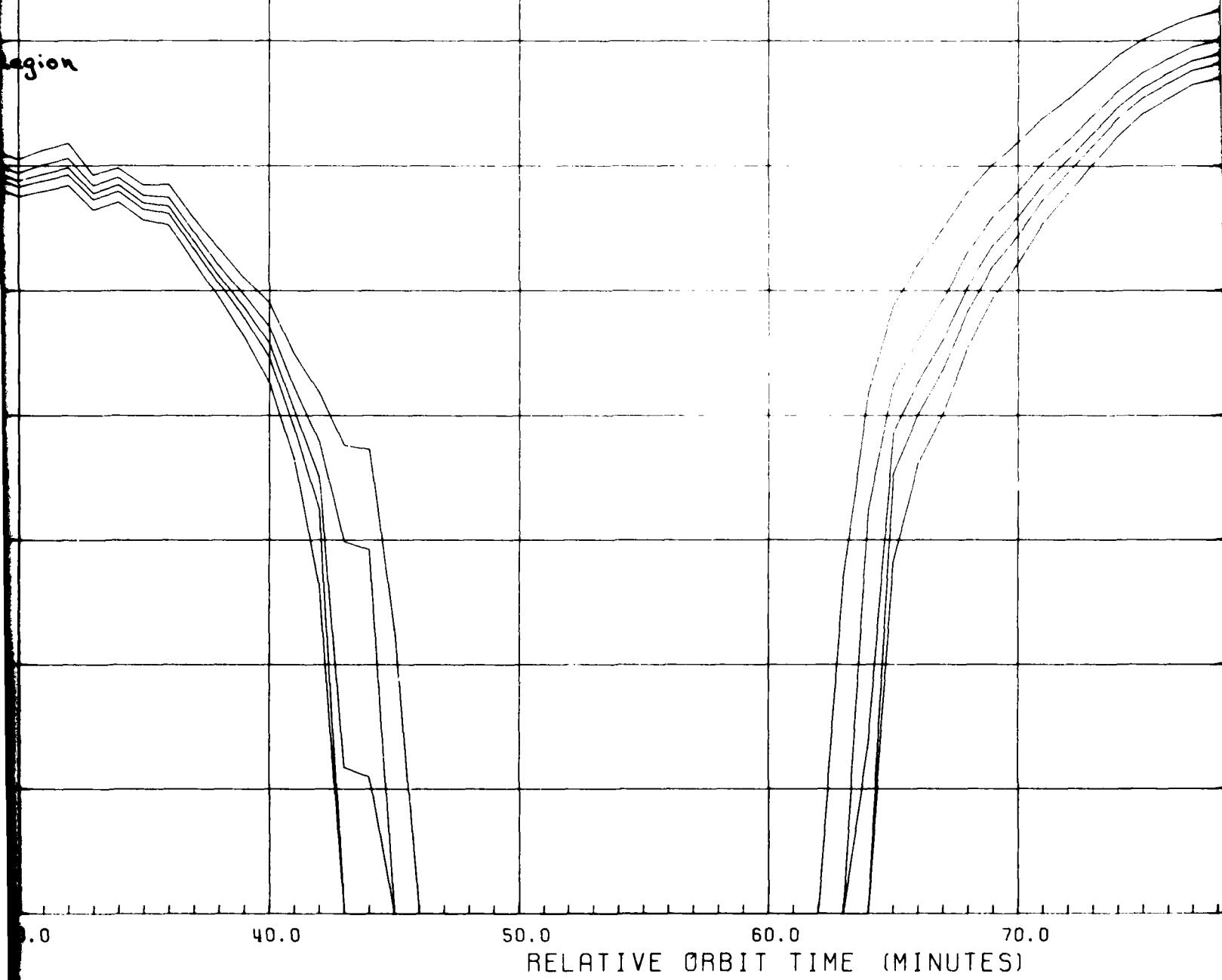
3.0 4.0 5.0 6.0
RBIT TIME (HOURS)



DOSE AT TRANSMISSION SURFACE OF FINITE ALUMINUM SLAB

(= DOSE IN SEMI-INFINITE ALUMINUM MEDIUM)

region



OF FINITE ALUMINUM SLAB SHIELDS

(FINITE ALUMINUM MEDIUM)

ORBIT: NAVELEX 1
60 DGR/1667-16

EPOCH: 1989.5

MODELS:
FIELD: BARR/75
TRAPPED PROTONS
INNER ZN ELEC:
OUTER ZN ELEC:

MISSION DURATION
EVALUATION PHASES

UN FACTORS: NOT

Equatorial Region

SAA

STOP TIME ON TPF

70.0

80.0

90.0

100.0

110

TIME (MINUTES)

Figure 115

ORBIT: NAVELEX
60 DGR/1667-1667 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AE17 L0

MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

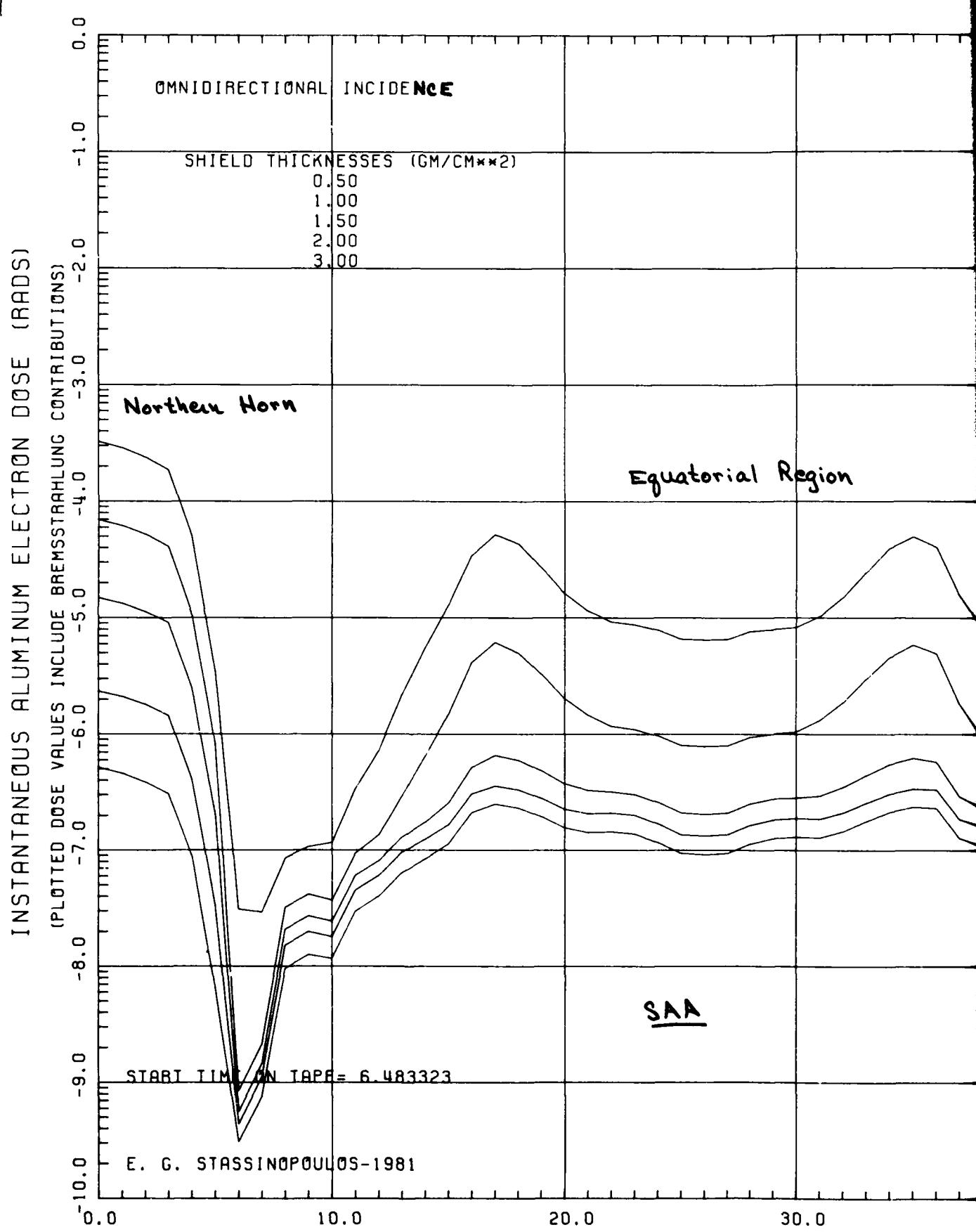
STOP TIME ON TAPF = 8.449993

NASA-GSFC

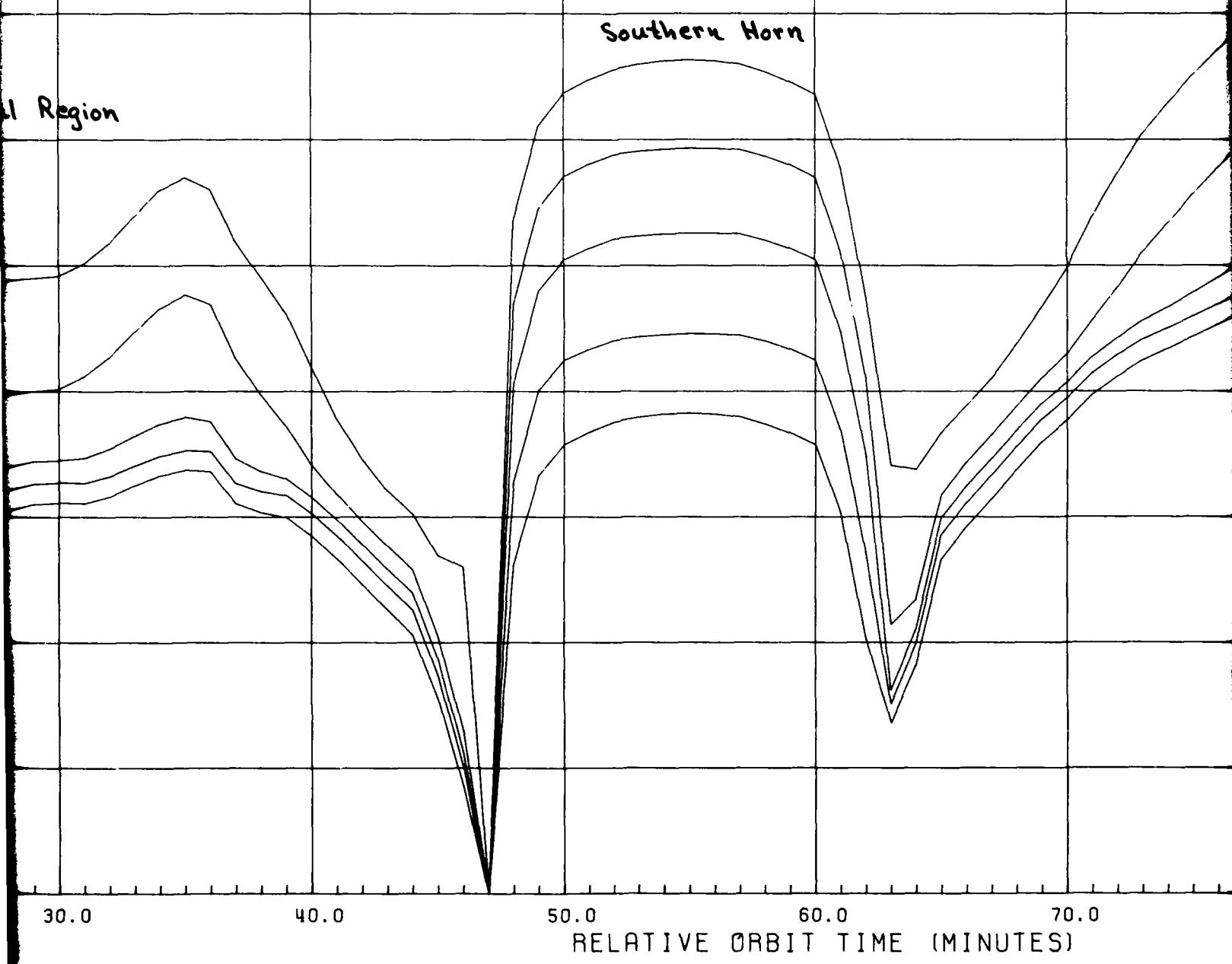
100.0

110.0

120.0



2
DOSE AT TRANSMISSION SURFACE OF FINITE ALUMINUM S



3 1

FINITE ALUMINUM SLAB SHIELDS

Figure

ORBIT: NAVELEX 1
60 DGR/1667-1667 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 L

MISSION DURATION: 60.0

EVALUATION PHASE: SOLAR

UN FACTORS: NOT APPLIED

Equatorial Region

No

SAA

STOP TIME ON TAPF = 8.4

NAS

70.0

80.0

90.0

100.0

110.0

MINUTES)

Figure 116

ORBIT: NAVELEX 1
60 DGR/1667-1667 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 LO

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern Horn

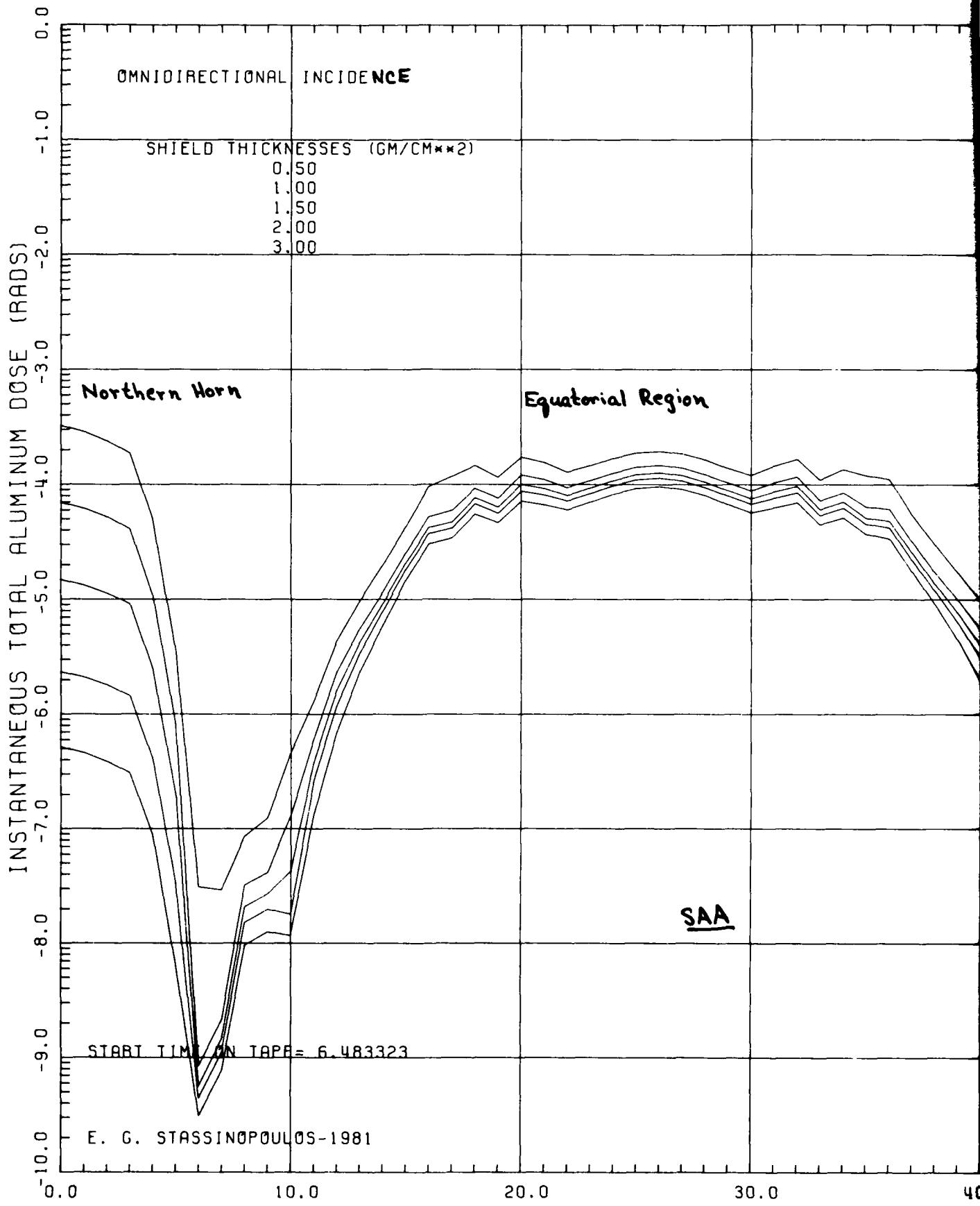
STOP TIME ON TAPF = 8.449993

NASA-GSFC

100.0

110.0

120.0



DOSE AT TRANSMISSION SURFACE OF FINITE ALUMINUM SLAB

Southern Horn



E ALUMINUM SLAB SHIELDS

Figure

ORBIT: NAVELEX 1
60 DGR/1667-1667 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Equatorial Region

Northern

SAA

STOP TIME ON TAPE = 8.449993

NASA-GSF

70.0 80.0 90.0 100.0 110.0

TES)

Figure 117

ORBIT: NAVELEX 1
60 DGR/1667-1667 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern Horn

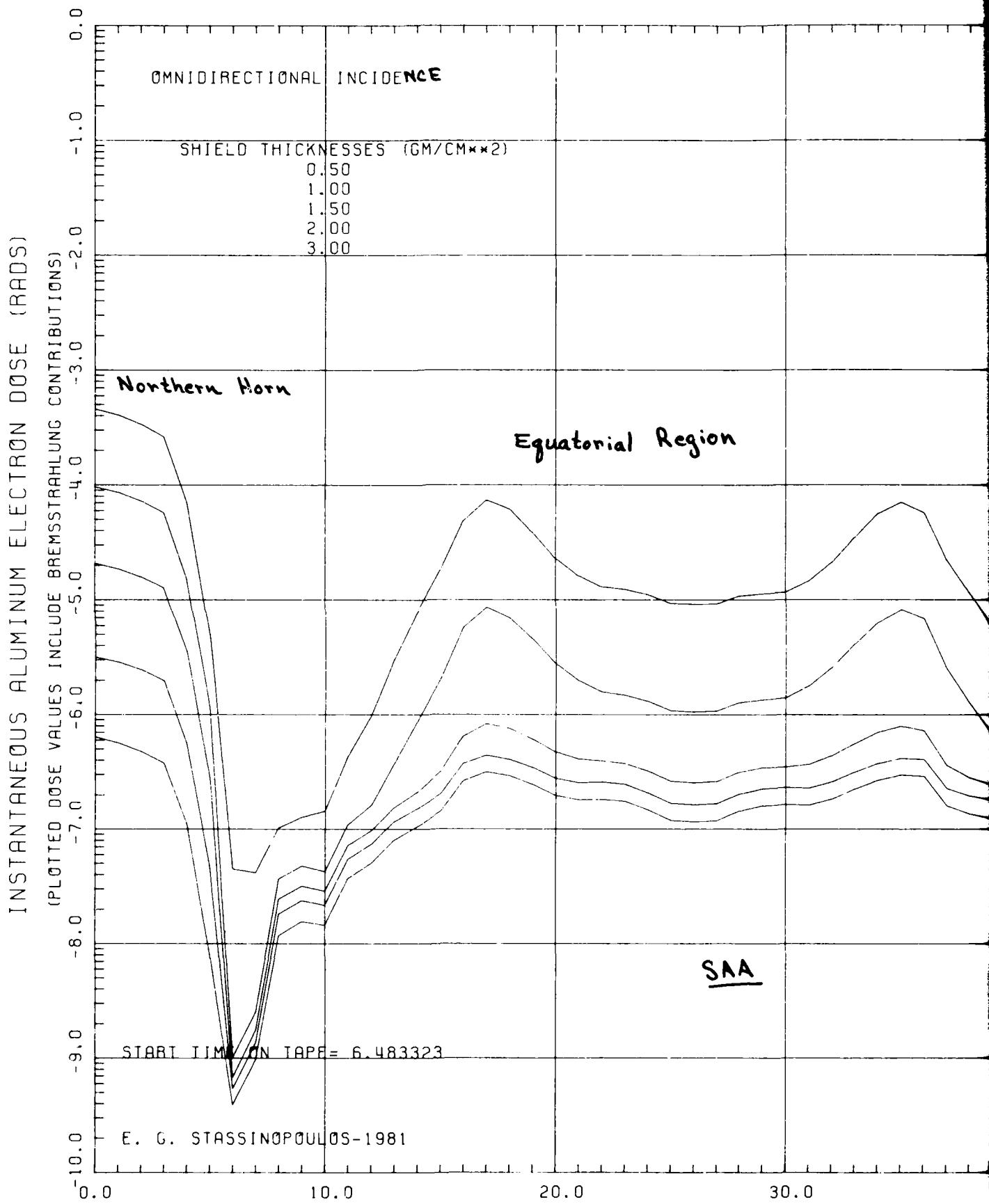
STOP TIME ON TAPF = 8.449993

NASA-GSFC

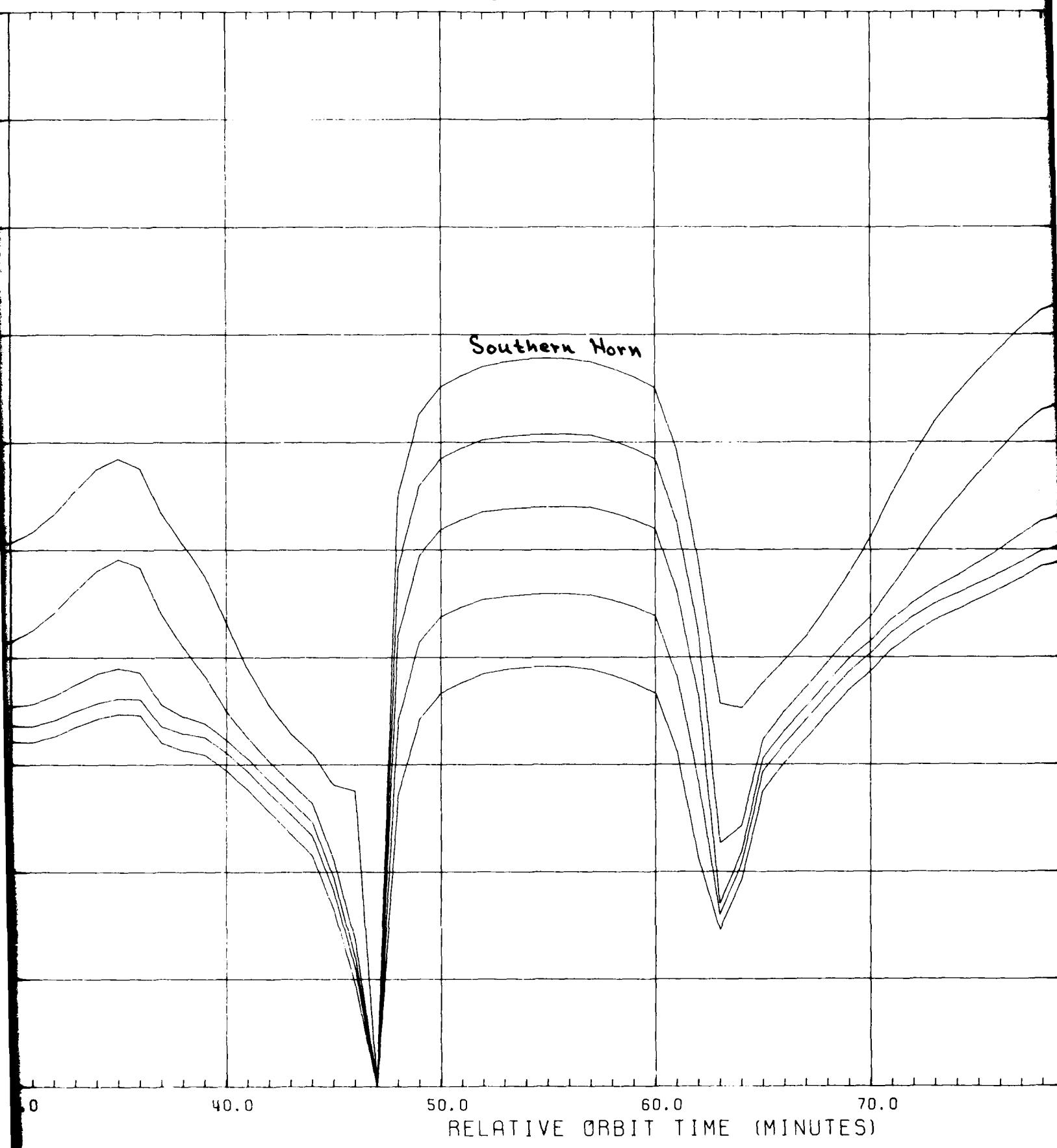
100.0

110.0

120.0



DOSE IN SEMI-INFINITE ALUMINUM MEDIUM



3

Figure 118

ORBIT: NAVELEX
60 OGR/1667-1667 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-LB

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Equatorial Region

Northern Horn

SAA

STOP TIME ON TAPF = 8.449993

NASA-GSFC

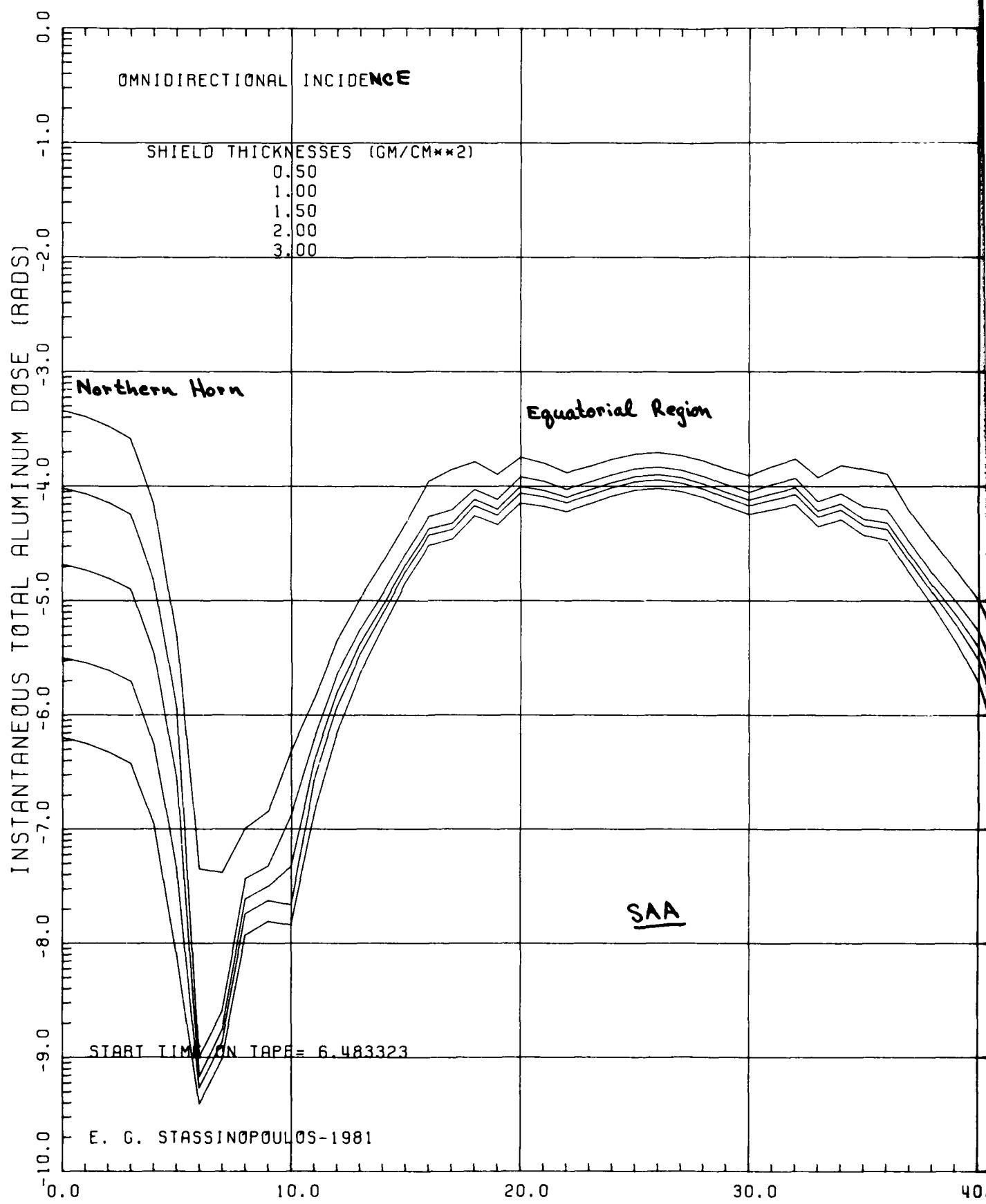
80.0

90.0

100.0

110.0

120.0

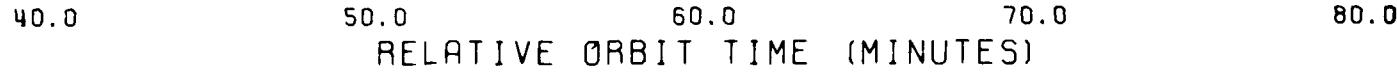


2

DOSE IN SEMI-INFINITE ALUMINUM MEDIUM

Southern Horn

SAA



3

JM

Figure 119

ORBIT: NAVELEX 1
60 DGR/1667-1667 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Equatorial Region

Northern Horn

SAA

STOP TIME ON TAPE = 8.449993

NASA-GSFC

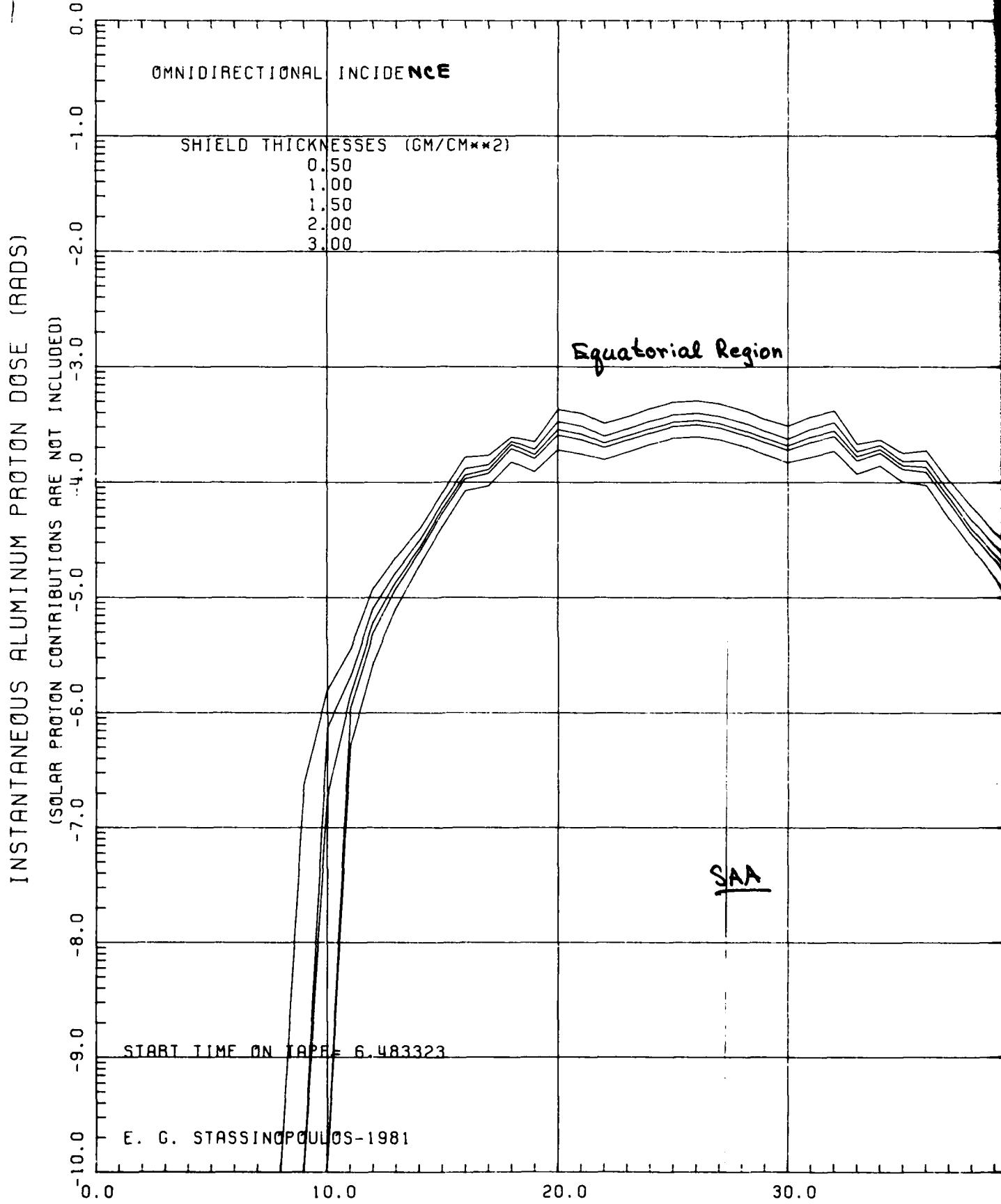
80.0

90.0

100.0

110.0

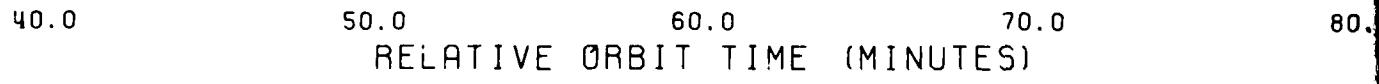
120.0



'2

DOSE AT CENTER OF ALUMINUM SPHERES

SAN



3
Figure 120

ORBIT: NAVELEX 1
60 DGR/1667-1667 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 LO

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Equatorial Region

SAA

STOP TIME ON TAPE = 8.449993

NASA-GSFC

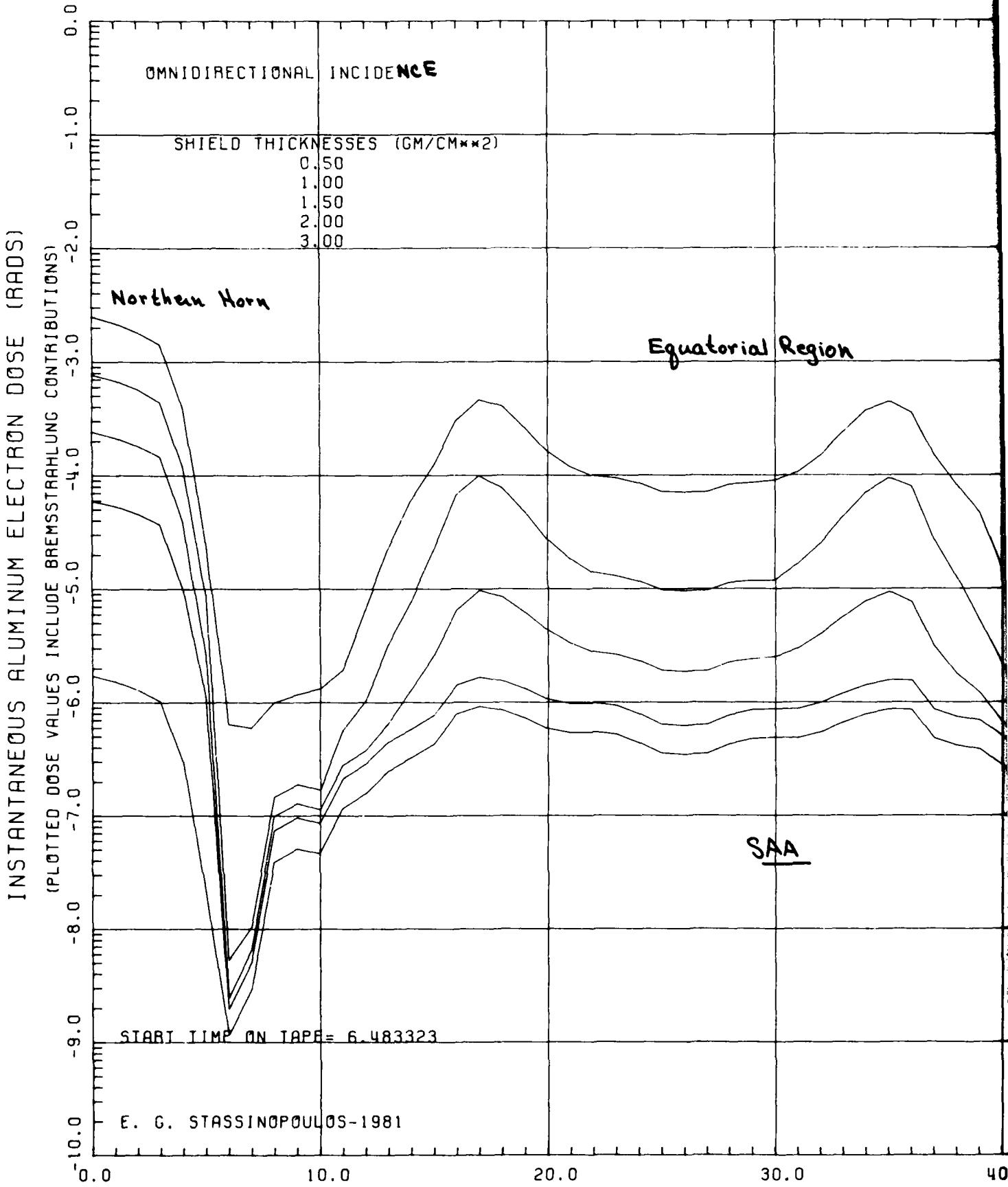
80.0

90.0

100.0

110.0

120.0



DOSE AT CENTER OF ALUMINUM SPHERES

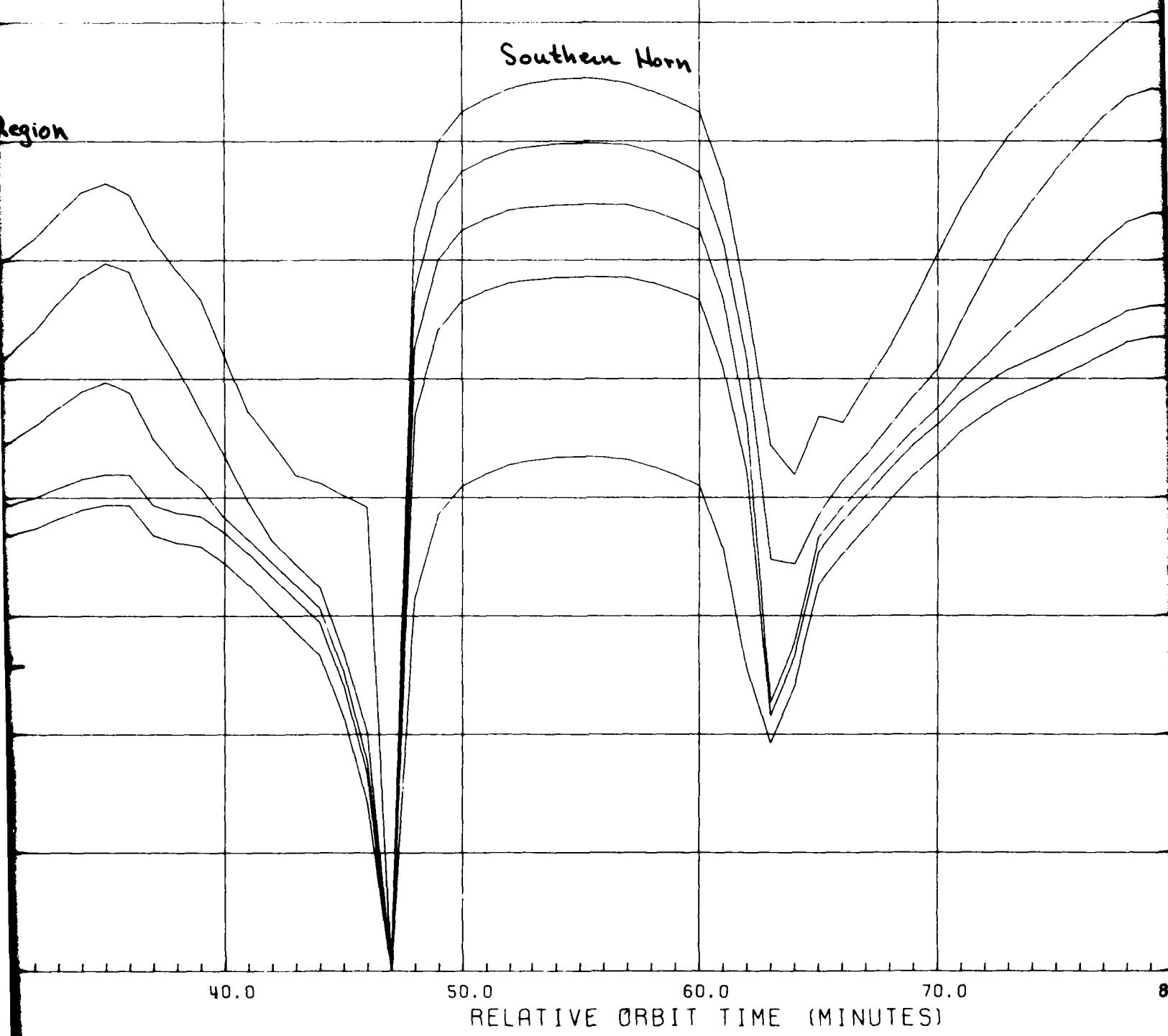
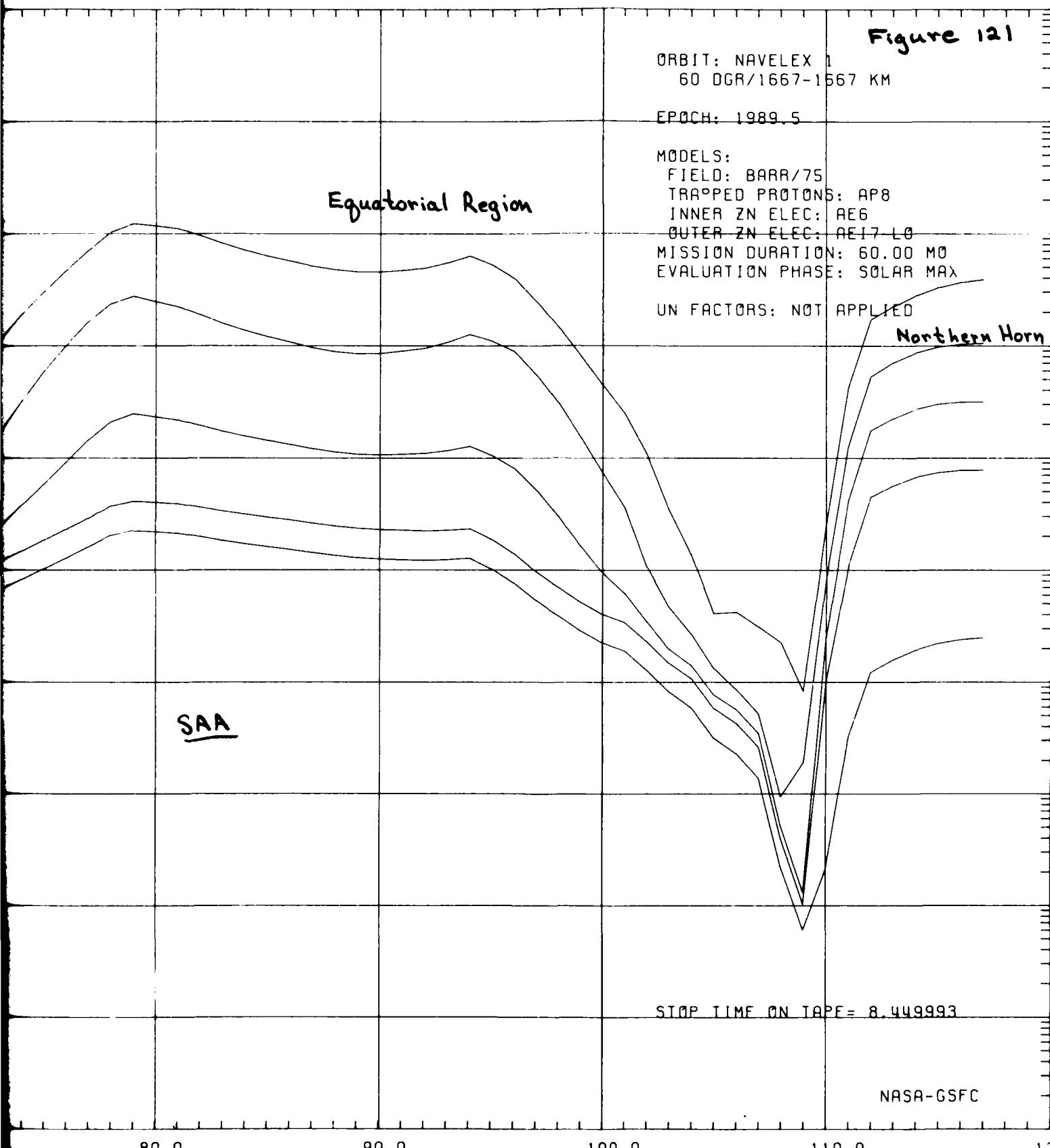
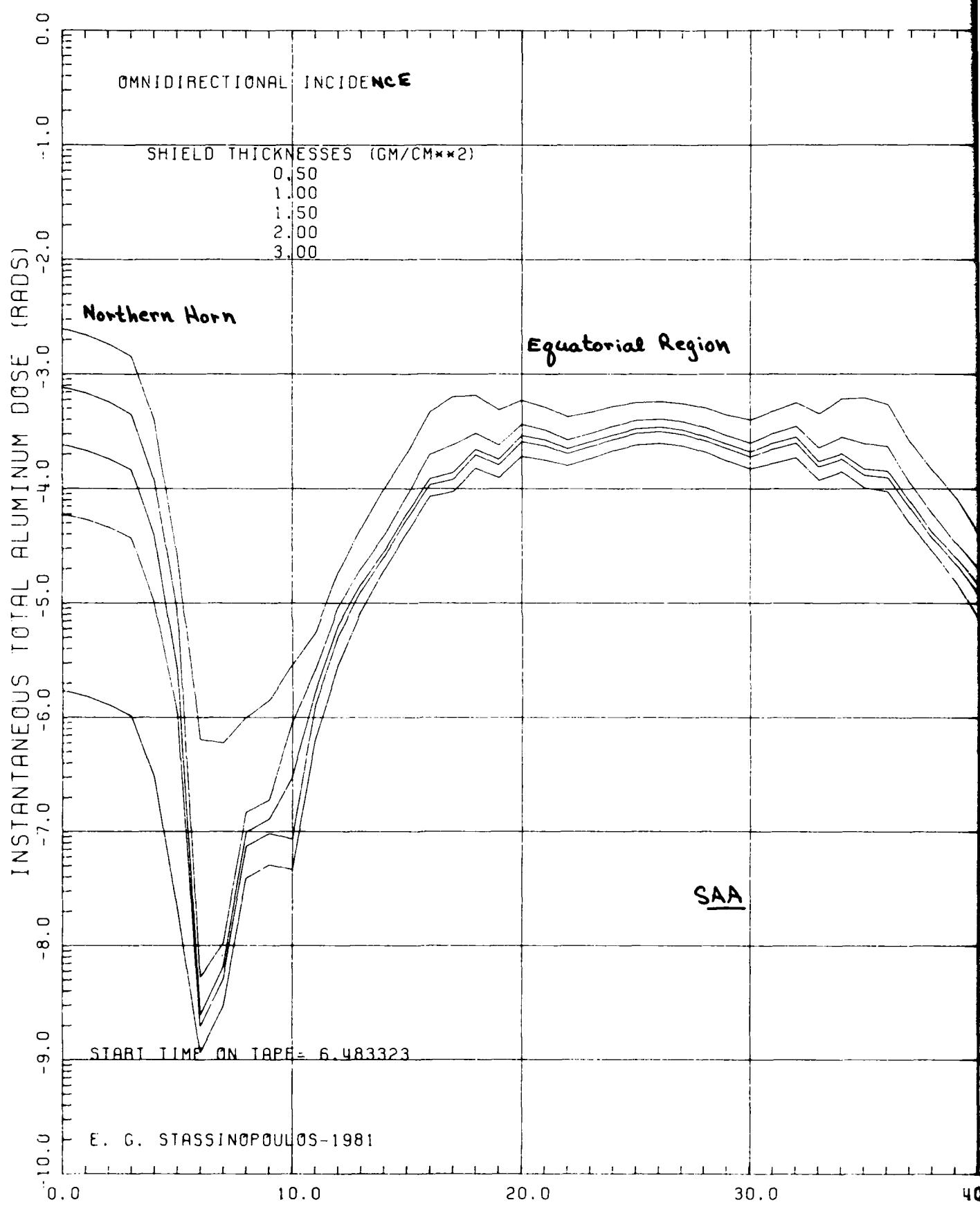


Figure 121





DOSE AT CENTER OF ALUMINUM SPHERES

Southern Horn

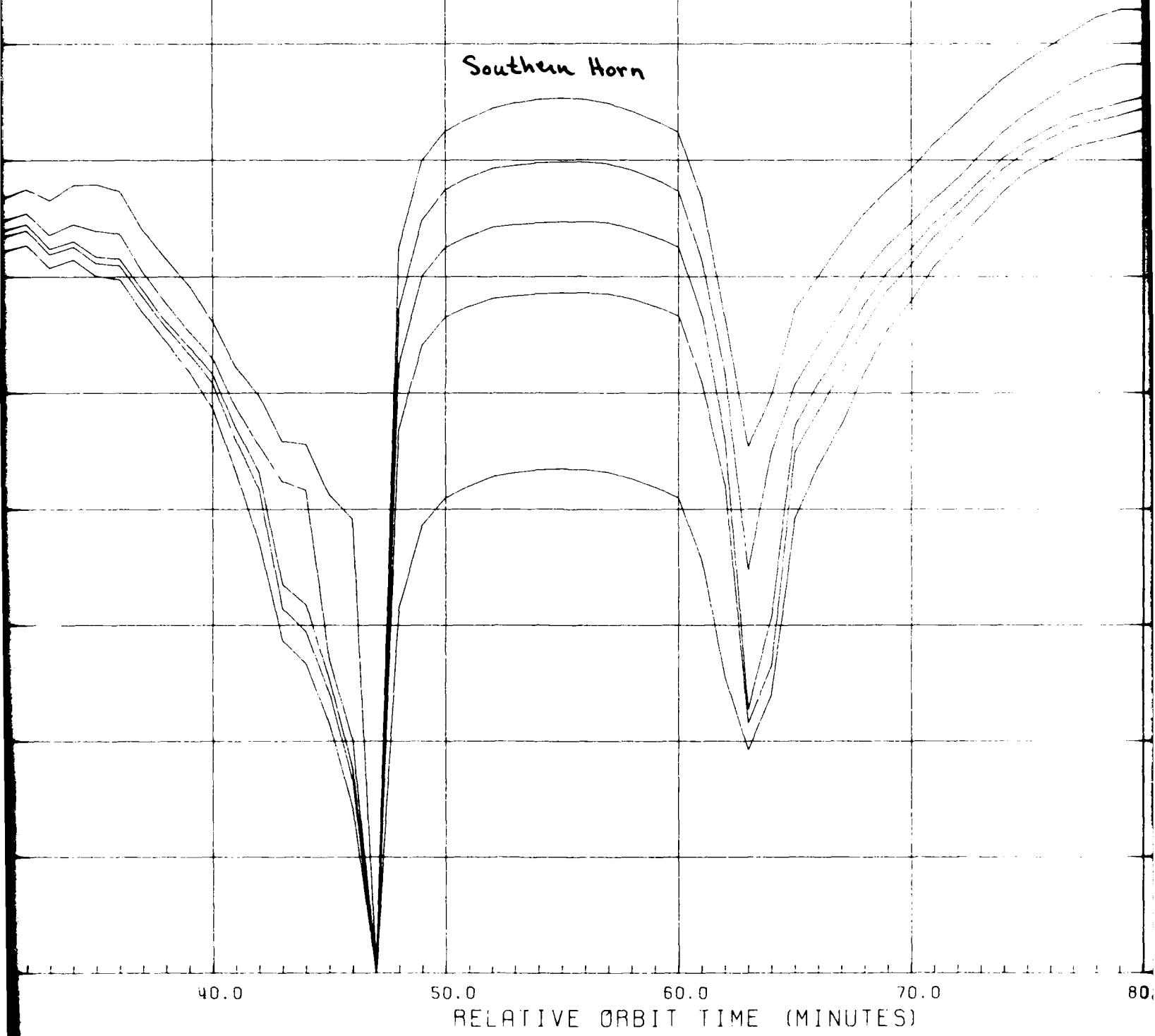


Figure 122

ORBIT: NAVELEX
60 DGR/1667-1667 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: RP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 LO

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Equatorial Region

Northern Horn

SAA

STOP TIME ON TAPE = 8.449993

NASA-GSFC

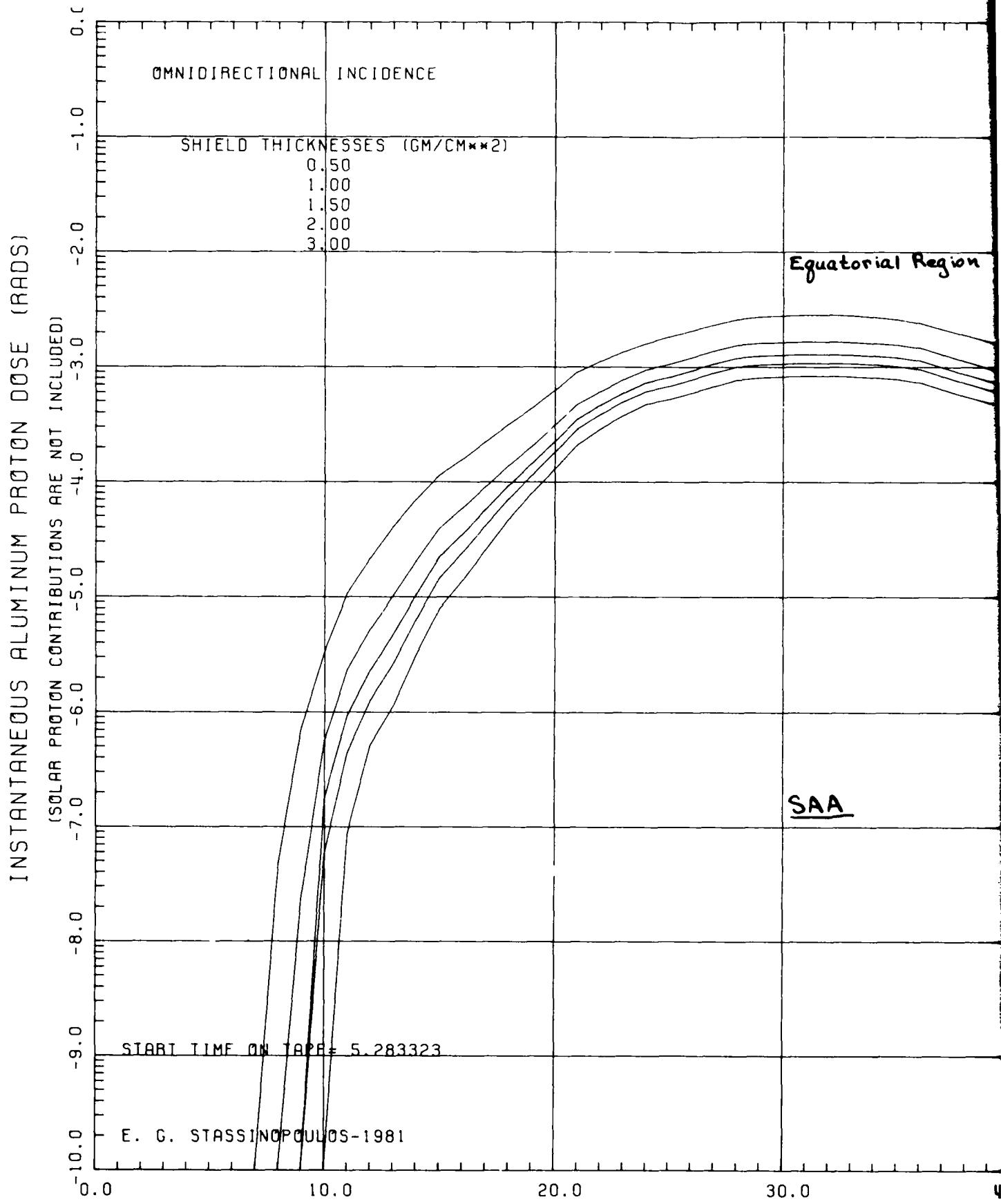
80.0

90.0

100.0

110.0

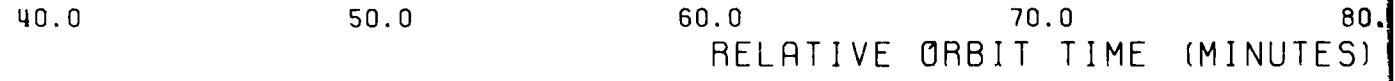
120.0



DOSE AT TRANSMISSION SURFACE OF FINITE AL

C = DOSE IN SEMI-INFINITE ALUMINUM

atorial Region



OF FINITE ALUMINUM SLAB SHIELDS

(FINITE ALUMINUM MEDIUM)

Equatorial Region

SAA

80.0

90.0

100.0

110.0

120.0

(MINUTES)

Figure 123

ORBIT: NAVELEX 2
60 DGR/2593-2593 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-L8

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Region

STOP TIME ON TAPE = 7.616656

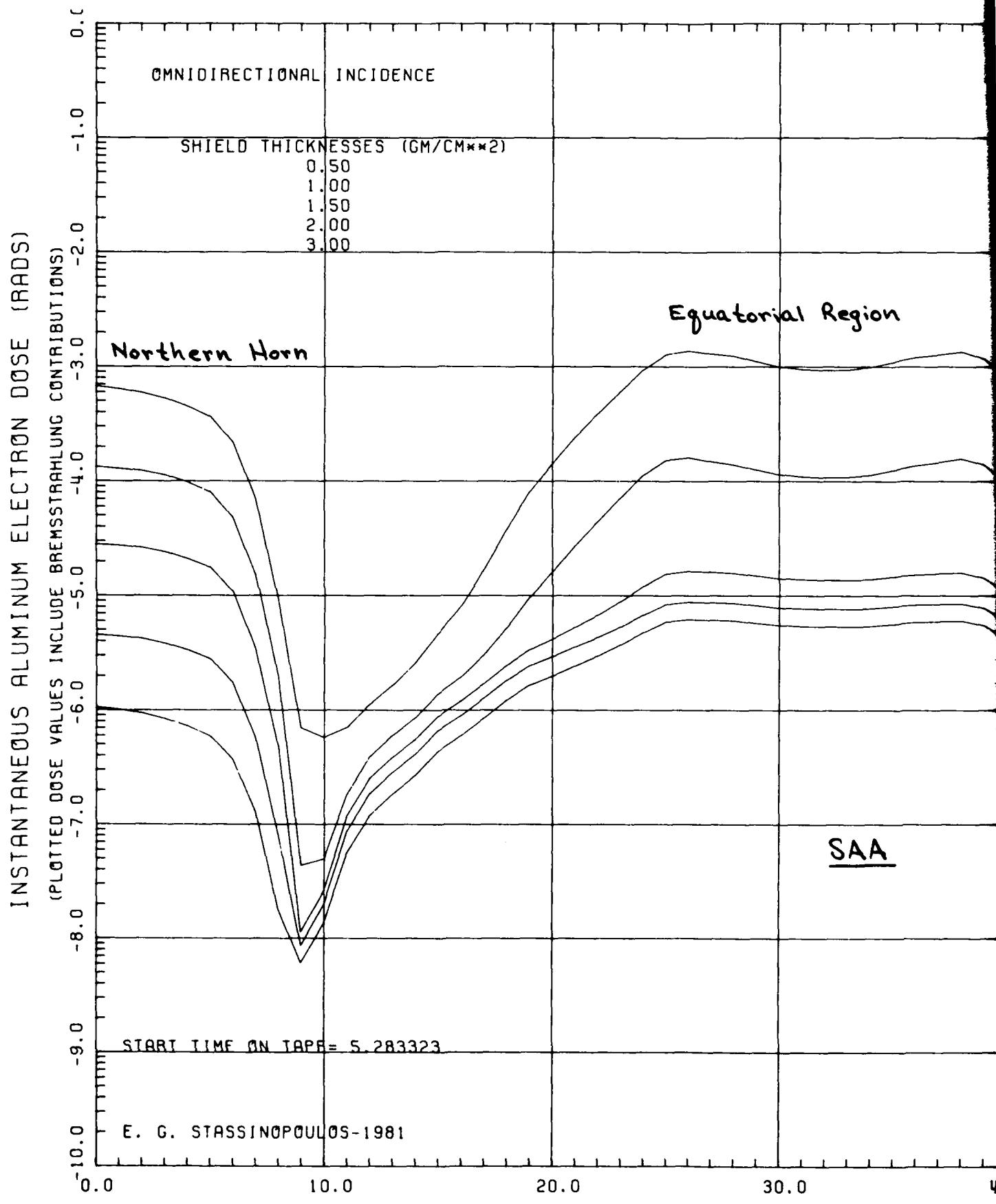
NASA-GSFC

110.0

120.0

130.0

140.0



2
DOSE AT TRANSMISSION SURFACE OF FINITE R

Region

Southern Horn

SAA

40.0

50.0

60.0

70.0

80

RELATIVE ORBIT TIME (MINUTES)

OF FINITE ALUMINUM SLAB SHIELDS

Equatorial Region

SAA

(MINUTES)

80.0

90.0

100.0

110.0

120.1

Figure 124

ORBIT: NAVELEX 2
60 DGR/2593-2593 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern Horn

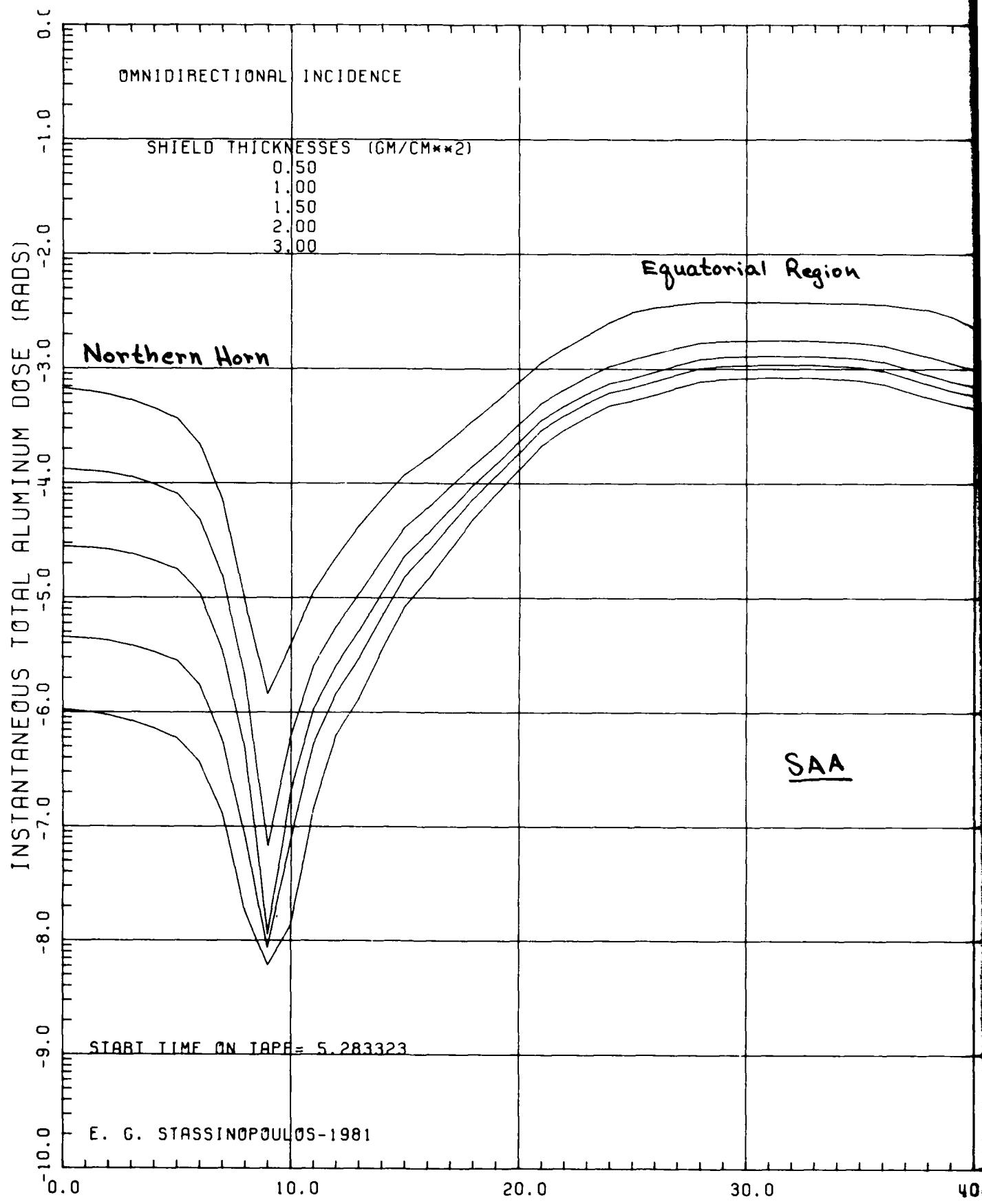
STOP TIME ON TAPF = 7.616656

NASA-GSFC

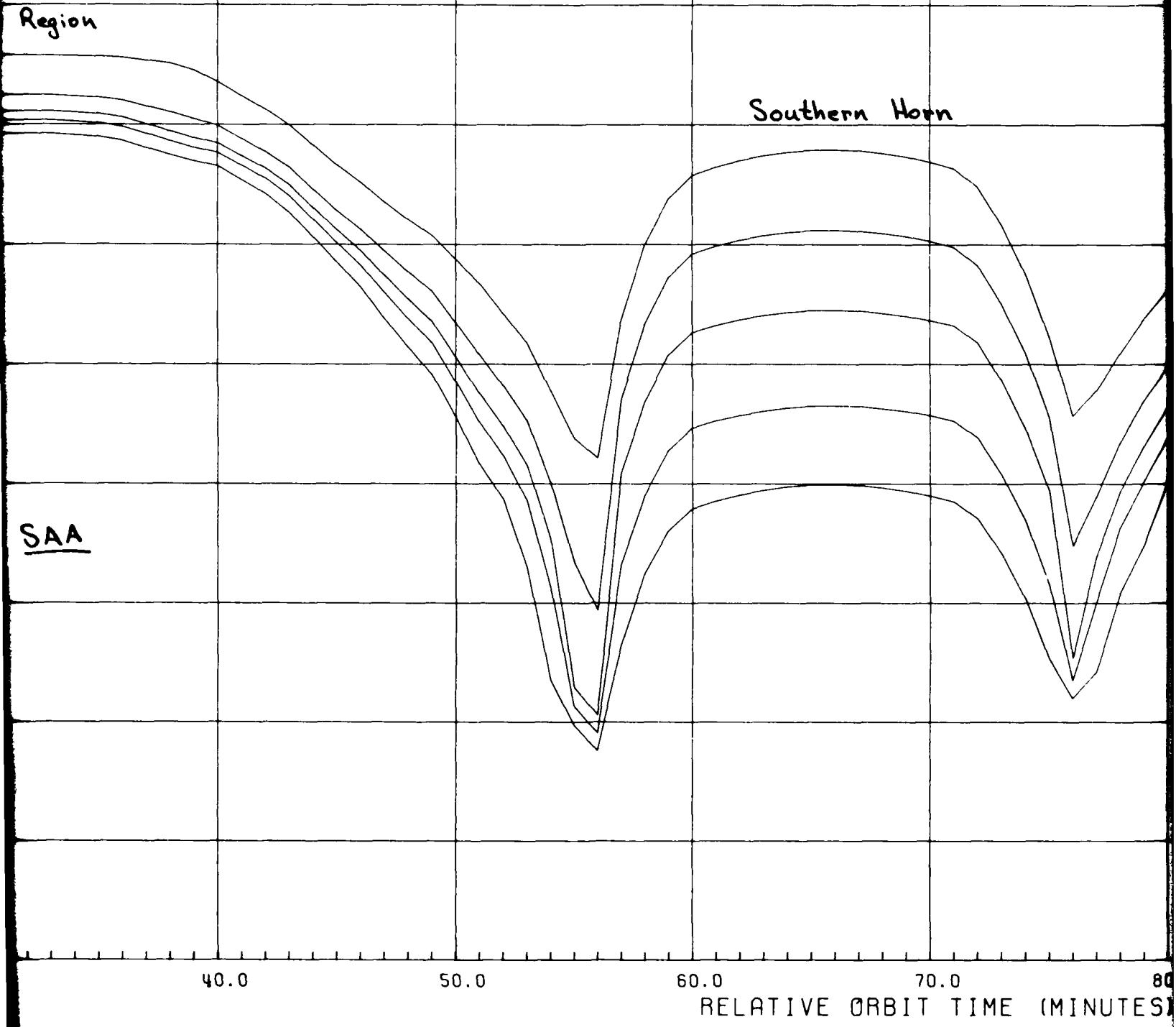
120.0

130.0

140.0



DOSAGE AT TRANSMISSION SURFACE OF FINITE A



E OF FINITE ALUMINUM SLAB SHIELDS

Equatorial Region

SAA

TIME (MINUTES)

Figure 125

ORBIT: NAVELEX 2
60 OGR/2593-2593 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

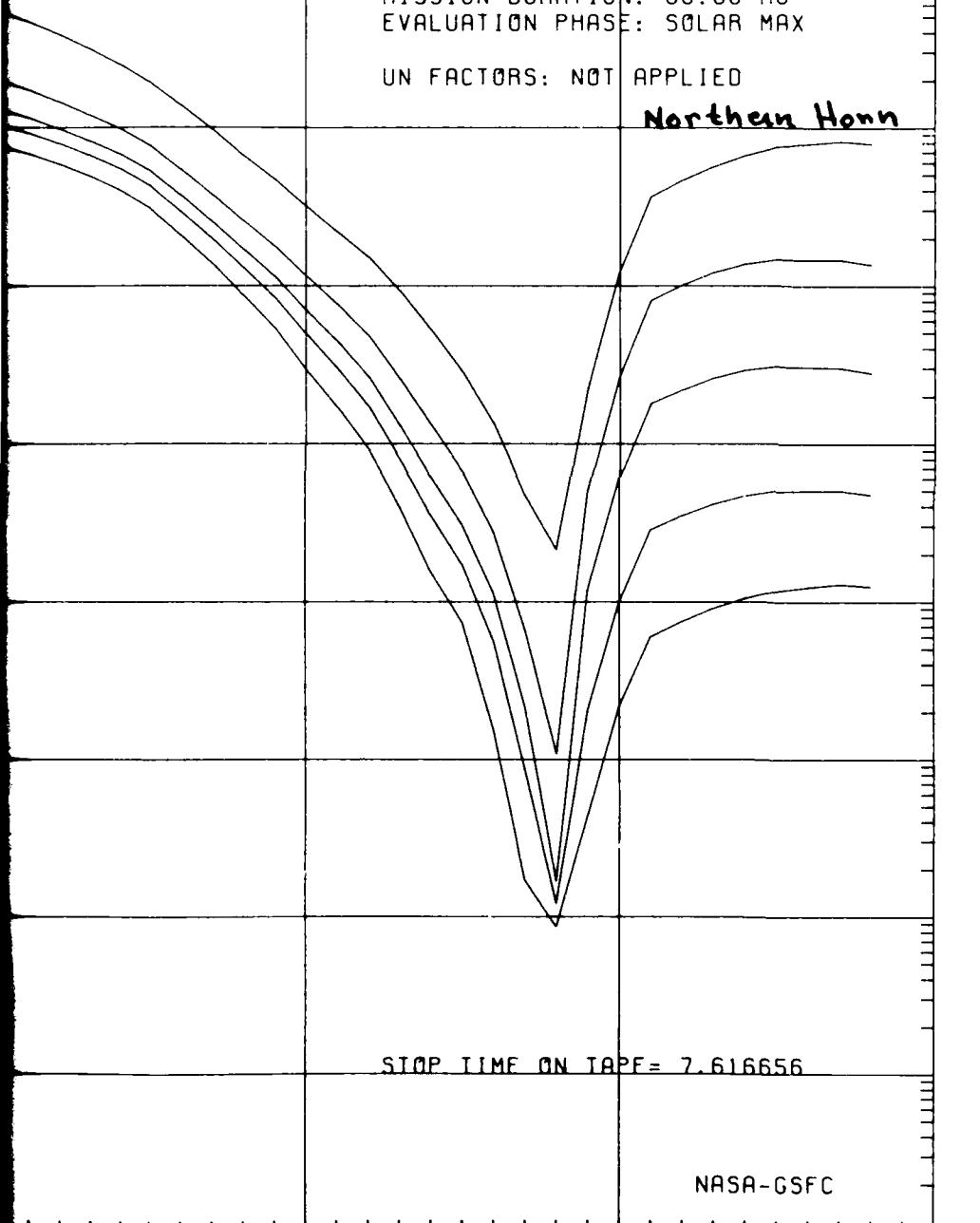
UN FACTORS: NOT APPLIED

Northern Hem

STOP TIME ON TAPE = 7.616656

NASA-GSFC

Region

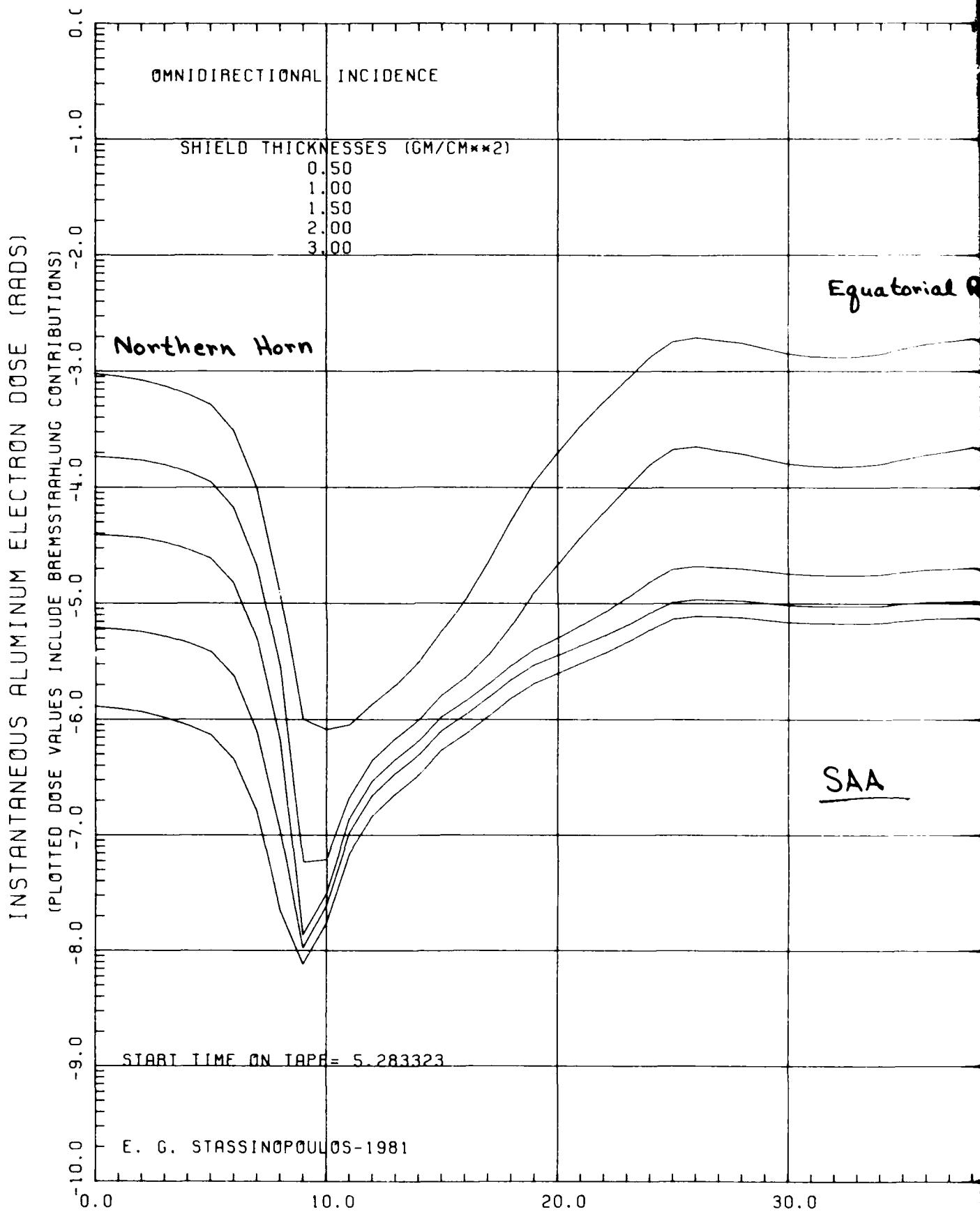


0.0

120.0

130.0

140.0



DOSE IN SEMI-INFINITE ALUMINU

Equatorial Region

Southern Horn

SAA

40.0

50.0

60.0

70.0

RELATIVE ORBIT TIME (MINUTES)

ITE ALUMINUM MEDIUM

Equatorial Region

SAA

80.0

90.0

100.0

110.0

TIME (MINUTES)

Figure 126

ORBIT: NAVELEX 2
60 DGR/2593-2593 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AE17-L0

MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern Horn

STOP TIME ON TAPE = 7.616656

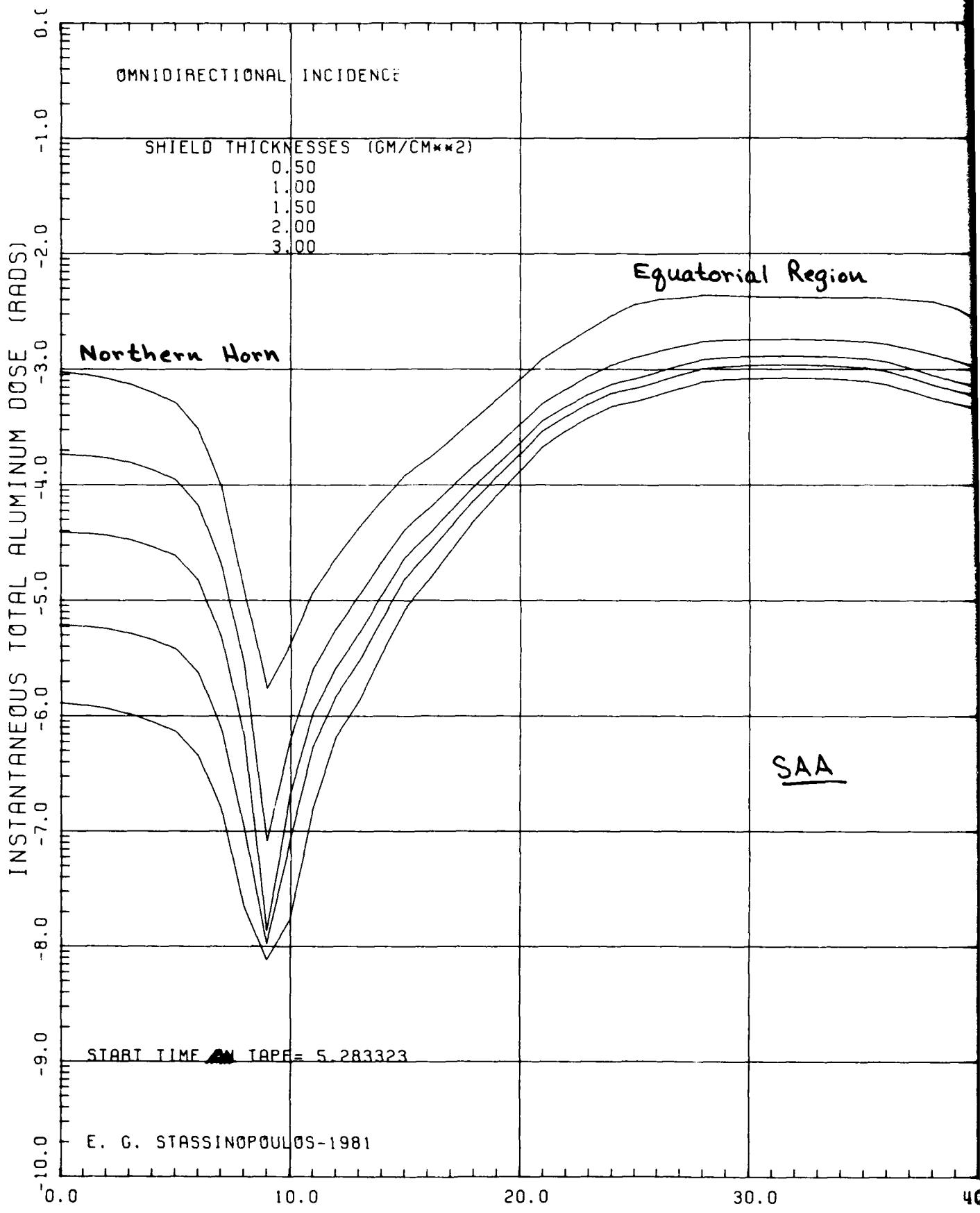
NASA-GSFC

110.0

120.0

130.0

140.0



2'

DOSE IN SEMI-INFINITE ALUMINUM

Region

Southern Horn

SAA

40.0

50.0

60.0

70.0

80

RELATIVE ORBIT TIME (MINUTES)

ITE ALUMINUM MEDIUM

Equatorial Region

SAA

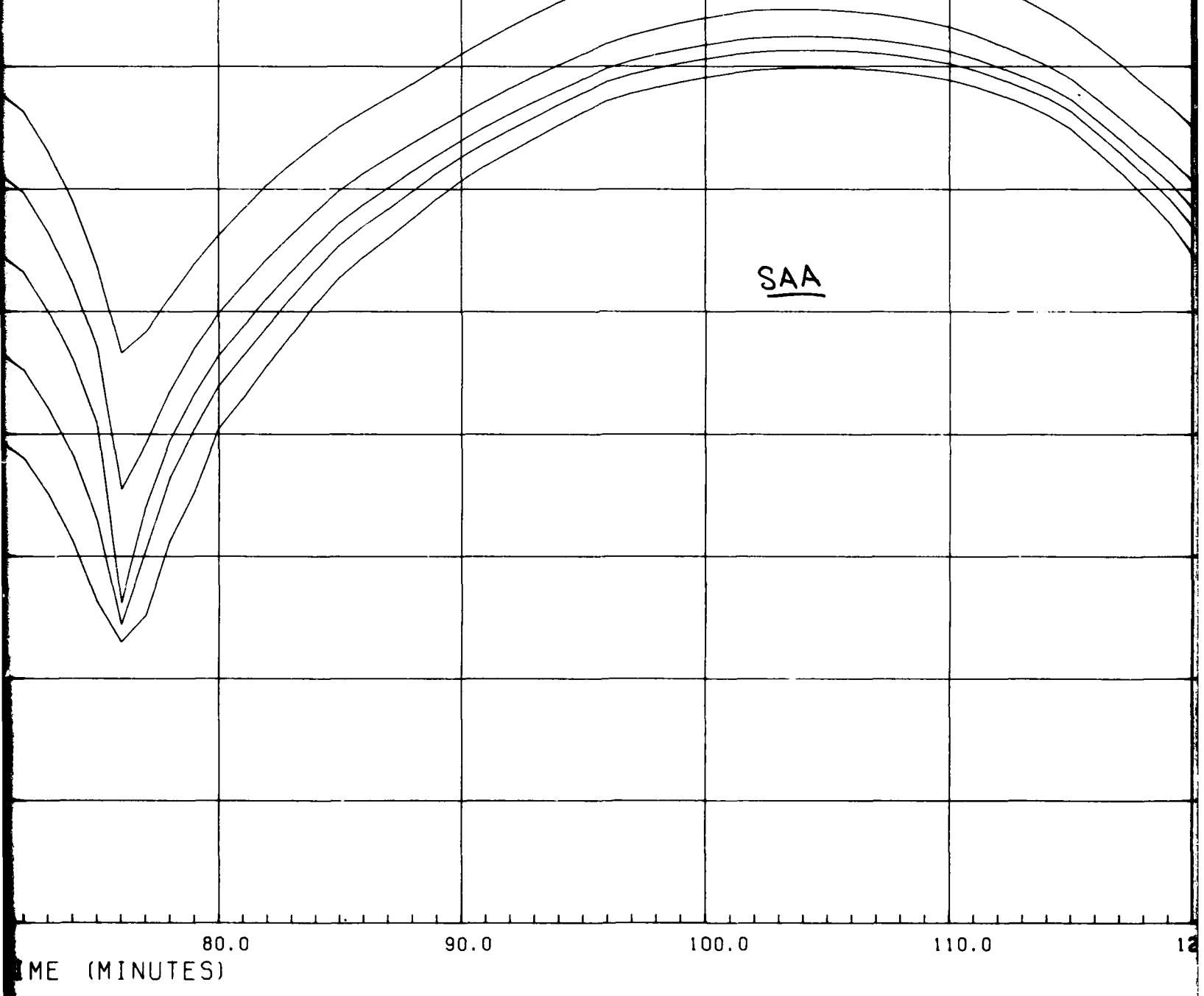


Figure 127

ORBIT: NAVELEX 2
60 DGR/2593-2593 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

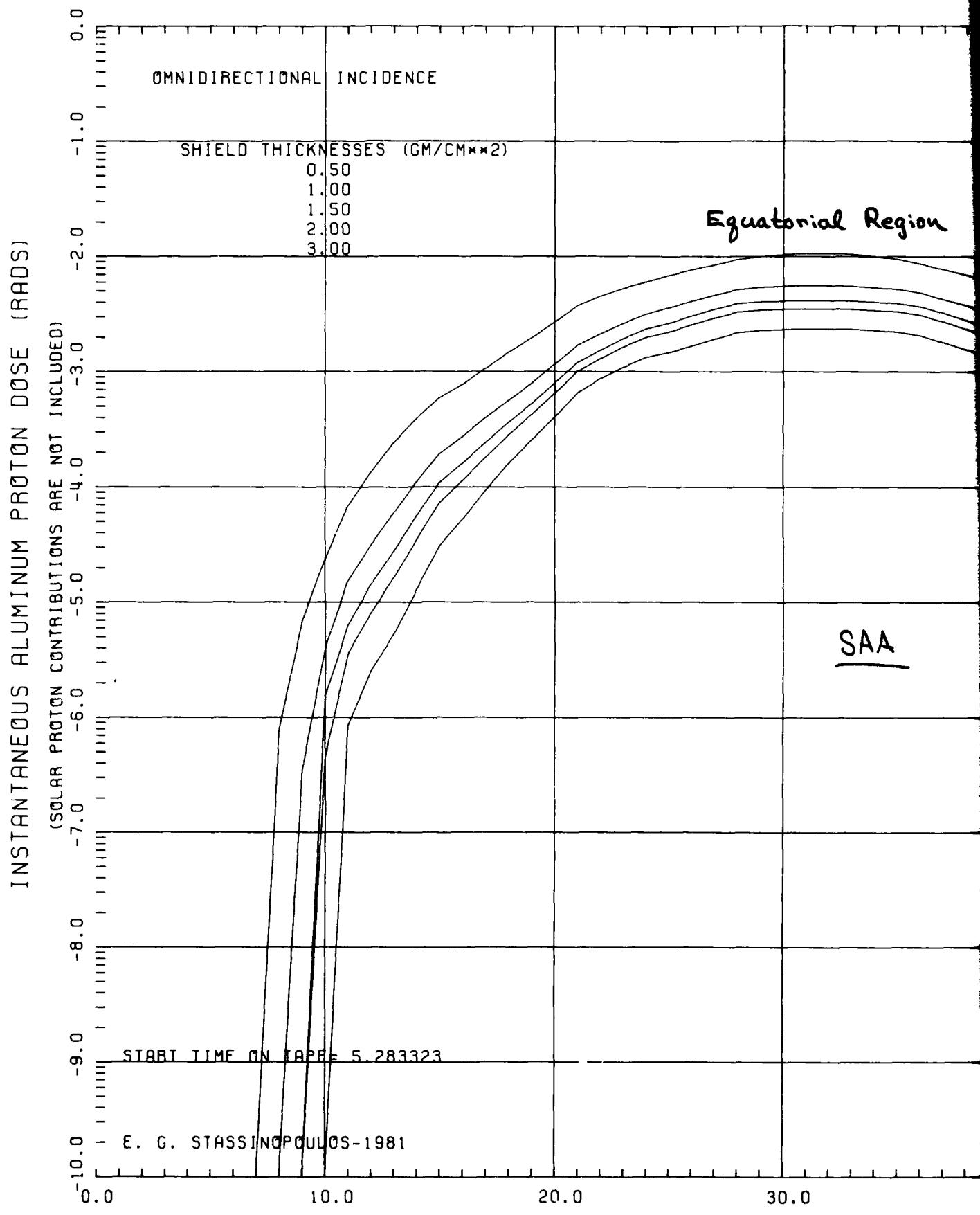
UN FACTORS: NOT APPLIED

Northern
Horn

STOP TIME ON TAPF = 7.616656

NASA-GSFC

120.0 130.0 140.0



DOSE AT CENTER OF ALUMINUM

atorial Region

SAA



F ALUMINUM SPHERES

Equatorial Region

SAA

80.0 90.0 100.0 110.0
TIME (MINUTES)

Figure 128

ORBIT: NAVELEX 2
60 DGR/2593-2593 KM

EPOCH: 1989.5

Region

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

STOP TIME ON TAPF = 7.616656

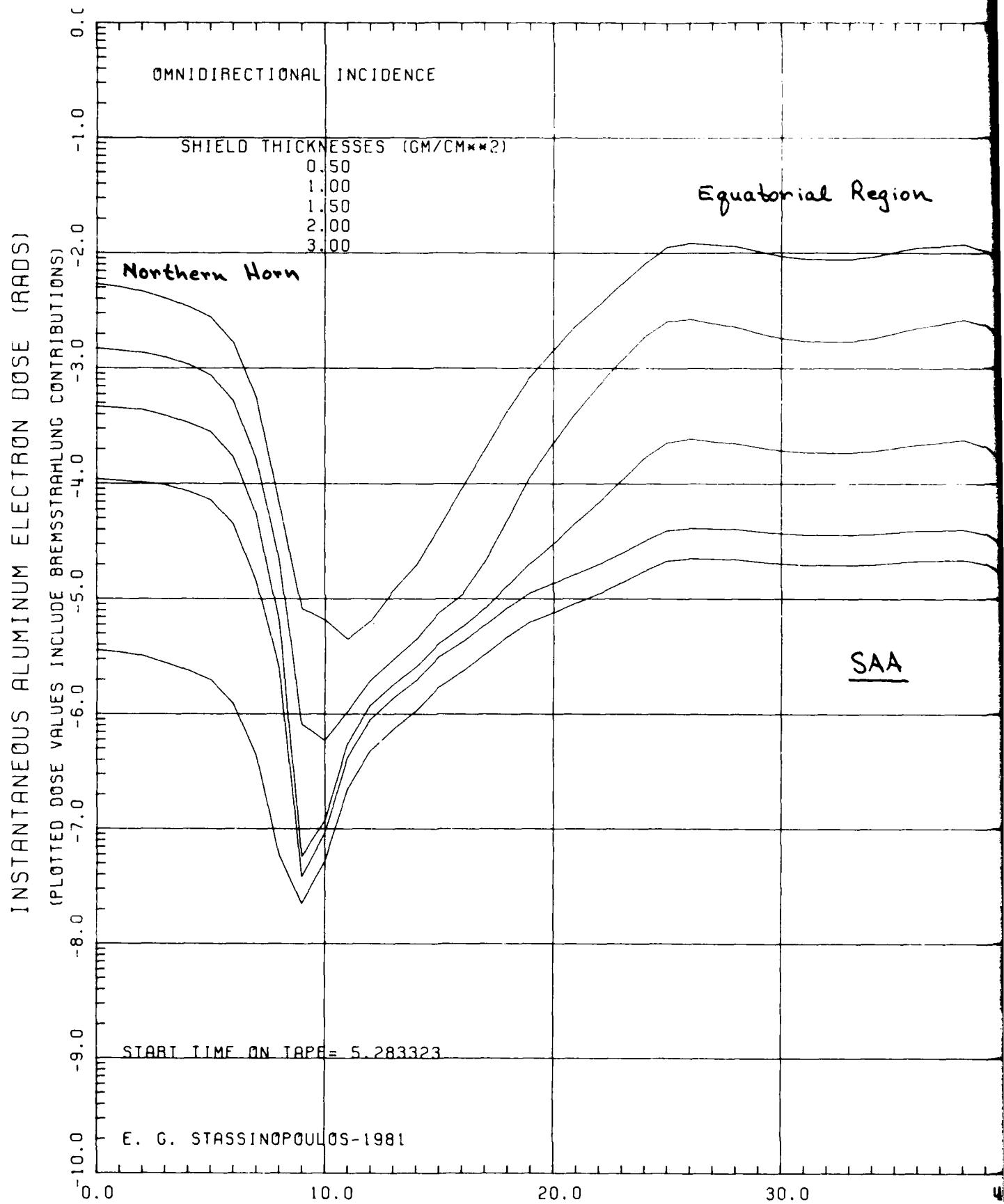
NASA-GSFC

110.0

120.0

130.0

140.0



DOSE AT CENTER OF ALUMINUM SPH

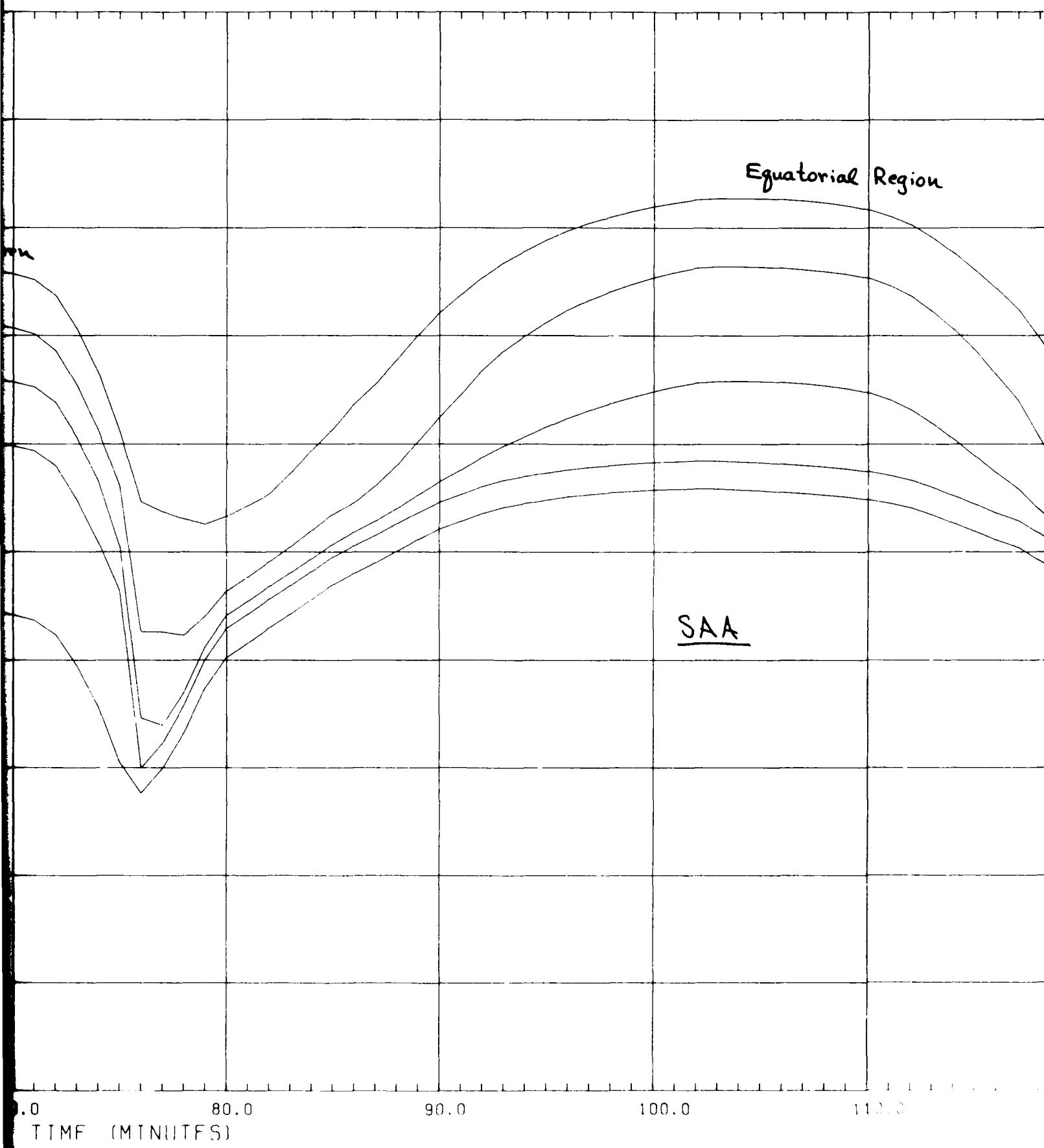
Region

Southern Horn

SAA

40.0 50.0 60.0 70.0 80.0
RELATIVE ORBIT TIME (MINUTES)

OF ALUMINUM SPHERES

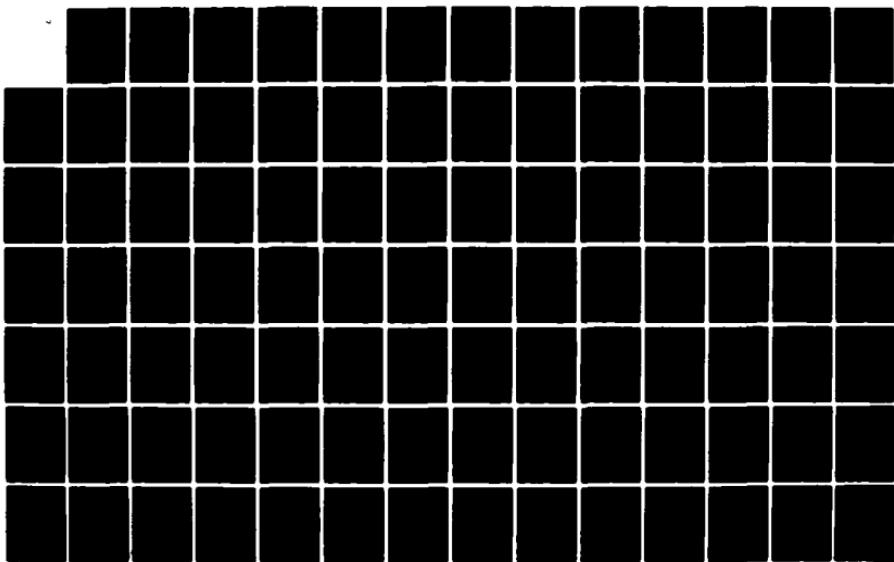


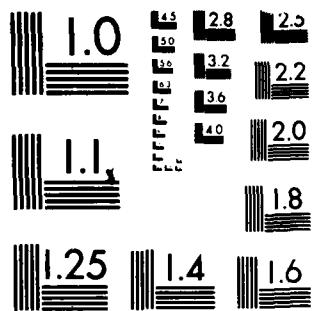
AD-A141 849 ORBITAL RADIATION STUDY FOR INCLINED CIRCULAR
UNCLASSIFIED TRAJECTORIES(U) NATIONAL AERONAUTICS AND SPACE
NOV 81 NASA-GSFC-X-601-81-28 ADMINISTRATION GREENBELT MD GO.. E G STASSINOPoulos

F/G 2273

4/5

NL





MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS 1963-A

4

Figure 129

ORBIT: NAVELEX 2
60 DGR/2593-2593 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-L8

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern Horn

STOP TIME ON TAPE = 7.616656

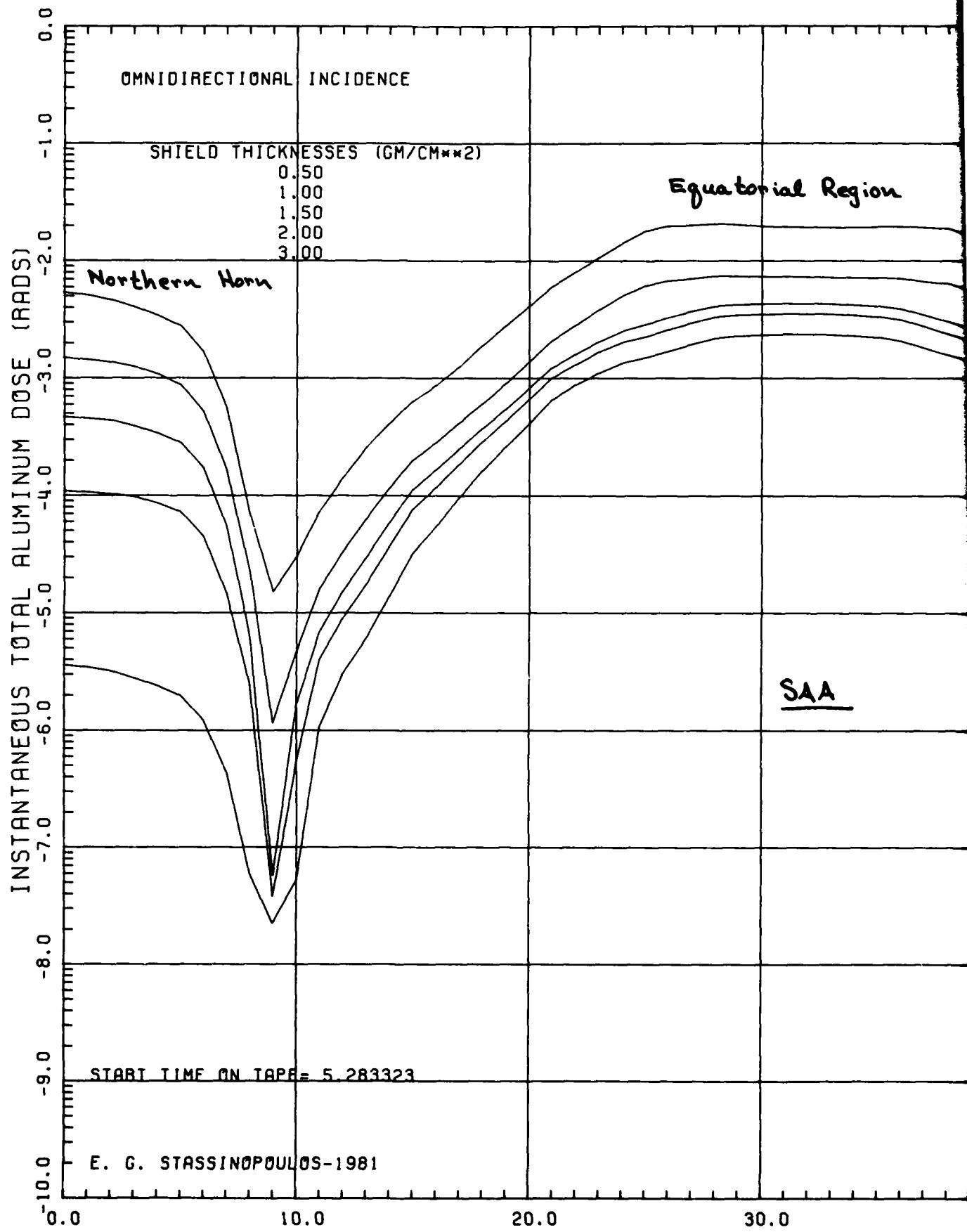
NASA-GSFC

0.0

120.0

130.0

140.0



2
DOSE AT CENTER OF ALUMINUM S

Region

Southern Horn

AA



13

ALUMINUM SPHERES

Equatorial Region

SAA

80.0

90.0

100.0

110.0

TIME (MINUTES)

4

Figure 130

ORBIT: NAVELEX 2
60 DGR/2593-2593 KM

EPOCH: 1989.5

atorial Region

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 LO

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern
Horn

STOP TIME ON TAPE = 7.616656

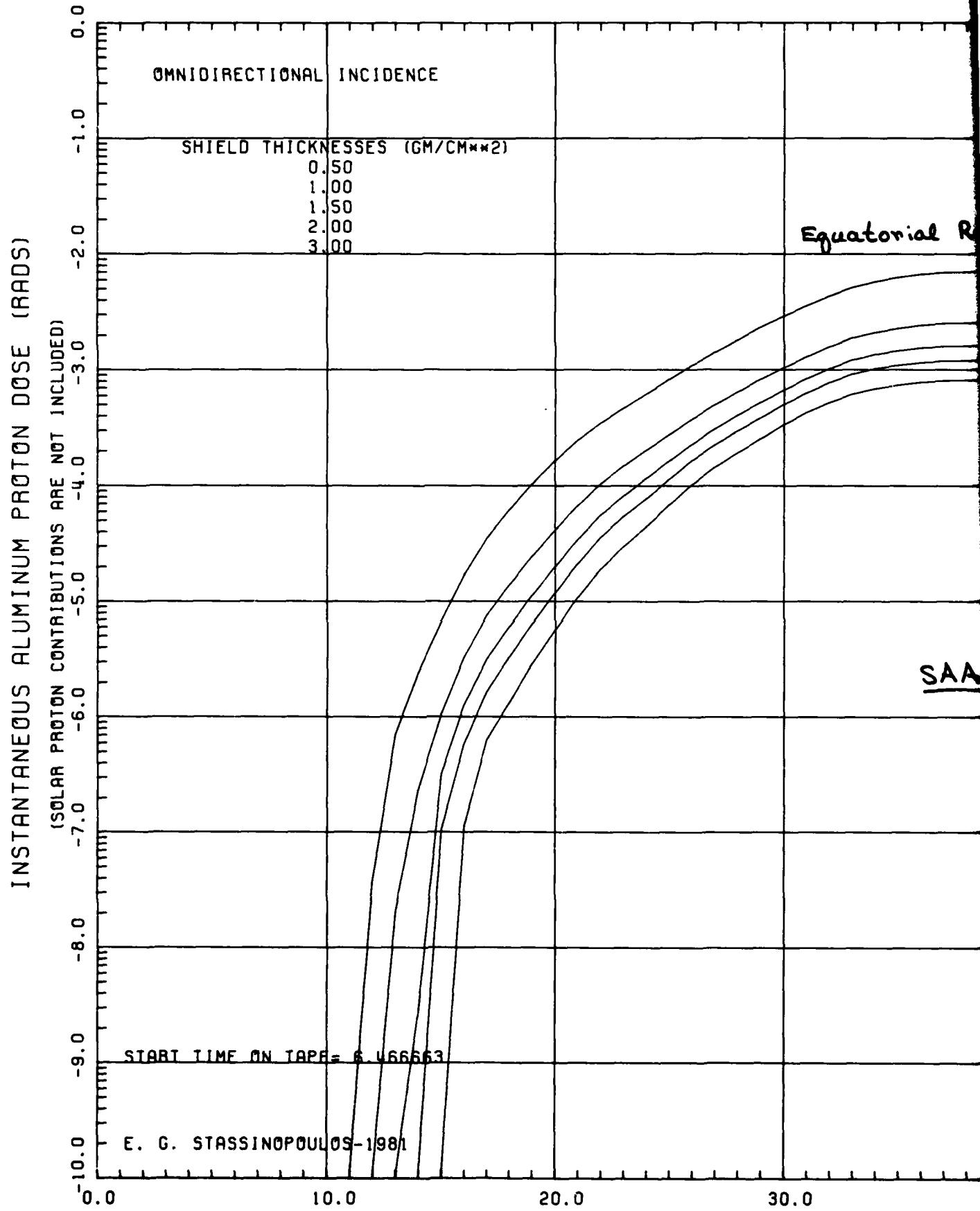
NASA-GSFC

110.0

120.0

130.0

140.0



2

DOSE AT T

(=

Equatorial Regions

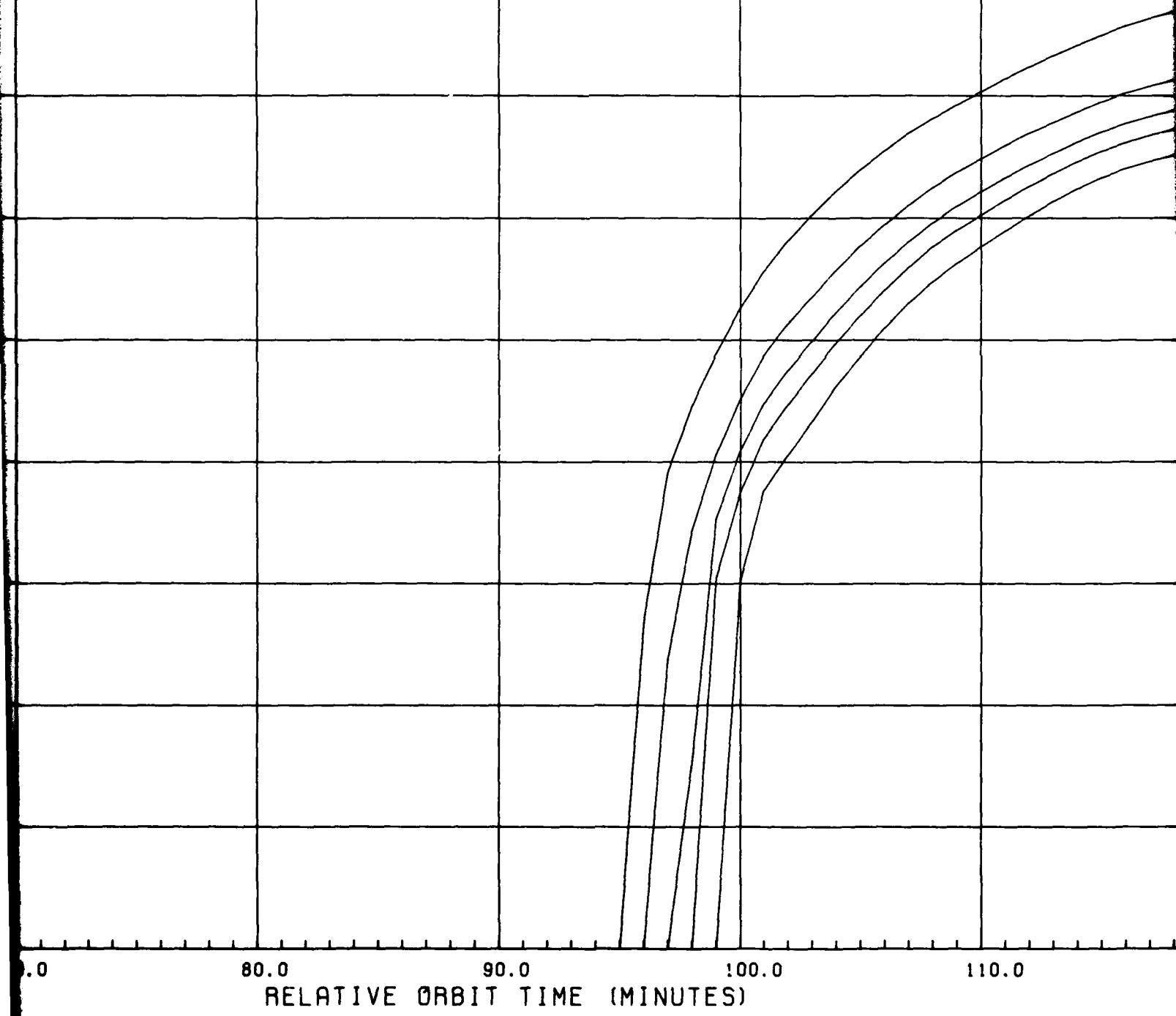
SAA



13

DOSE AT TRANSMISSION SURFACE OF FINITE ALUMINUM SLAB SHIELDS

(= DOSE IN SEMI-INFINITE ALUMINUM MEDIUM)



HIELDS

14

Equatorial Region

SAA

0.0

120.0

130.0

140.0

150.0

5

Figure 131

ORBIT: NAVELEX 3
60 DGR/3889-3889 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

STOP TIME ON TAPF = 9.316662

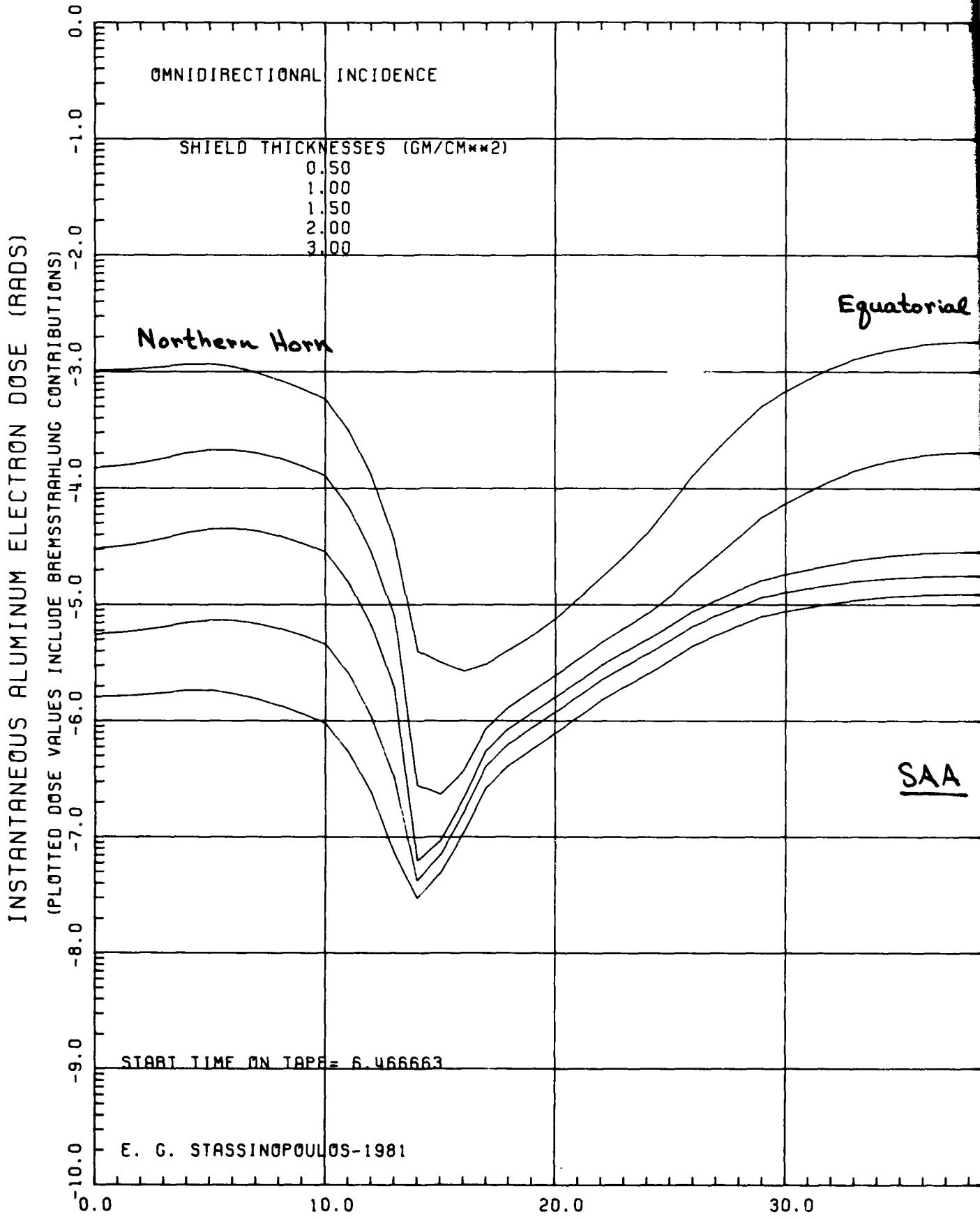
NASA-GSFC

150.0

160.0

170.0

180.0



DOSE AT TRA

Equatorial Region

Southern Horn

SAA

40.0

50.0

60.0

70.0

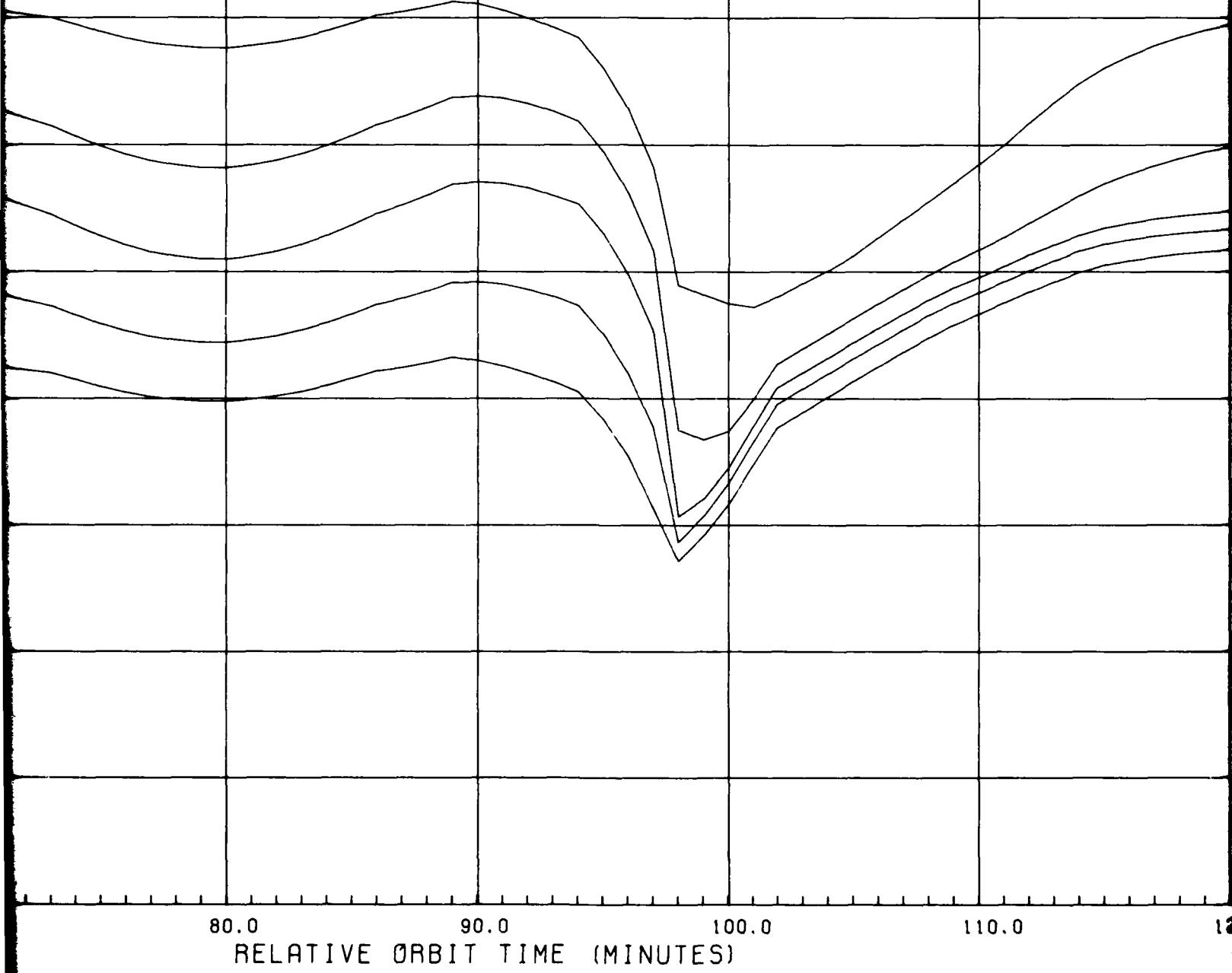
80

13

DOSE AT TRANSMISSION SURFACE OF FINITE ALUMINUM SLAB SHIELDS

Southern Horn

Southern Horn



4

S

Equatorial Region

Northern
Horn

SAA

120.0

130.0

140.0

150.0

160.0

5

Figure 132

ORBIT: NAVELEX B
60 DGR/3889-3889 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AE17 LO

MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern Horn

STOP TIME ON TAPE = 9.316662

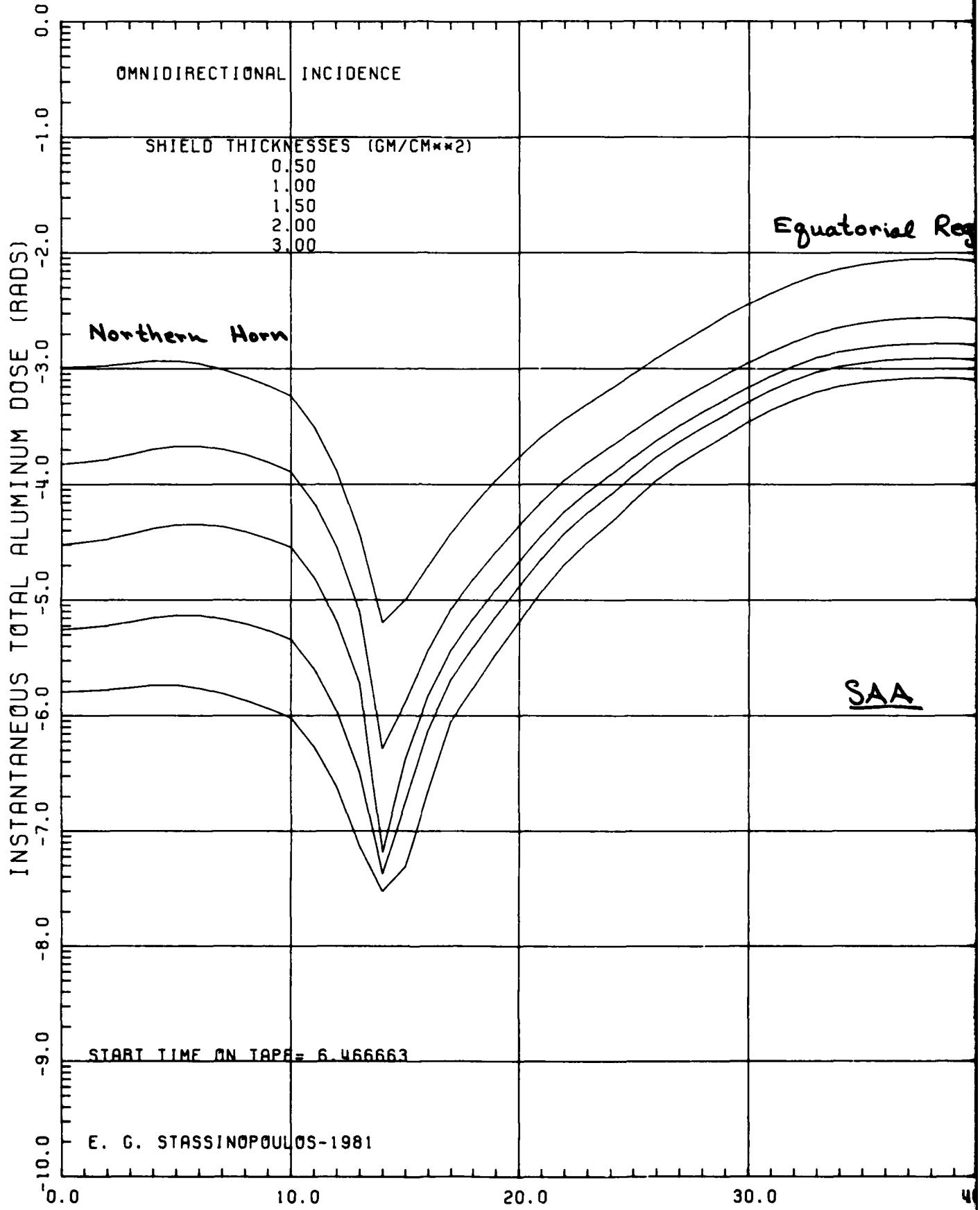
NASA-GSFC

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160.0

170.0

180.0



DOSE AT TR

2

Equatorial Region

Southern Horn

SAA

40.0

50.0

60.0

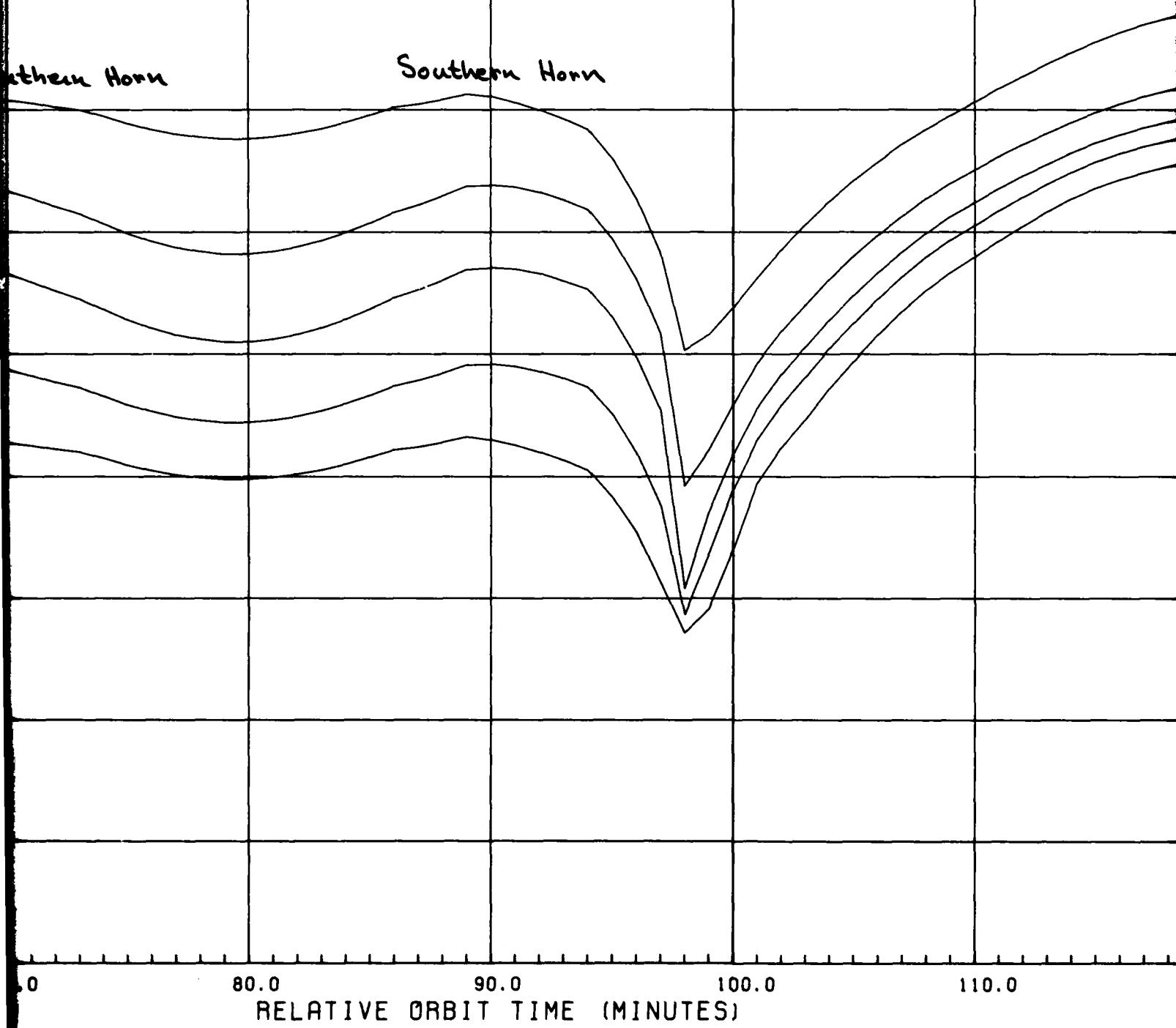
70.0

13

DOSE AT TRANSMISSION SURFACE OF FINITE ALUMINUM SLAB SHIELDS

Northern Horn

Southern Horn



IELDS

'4

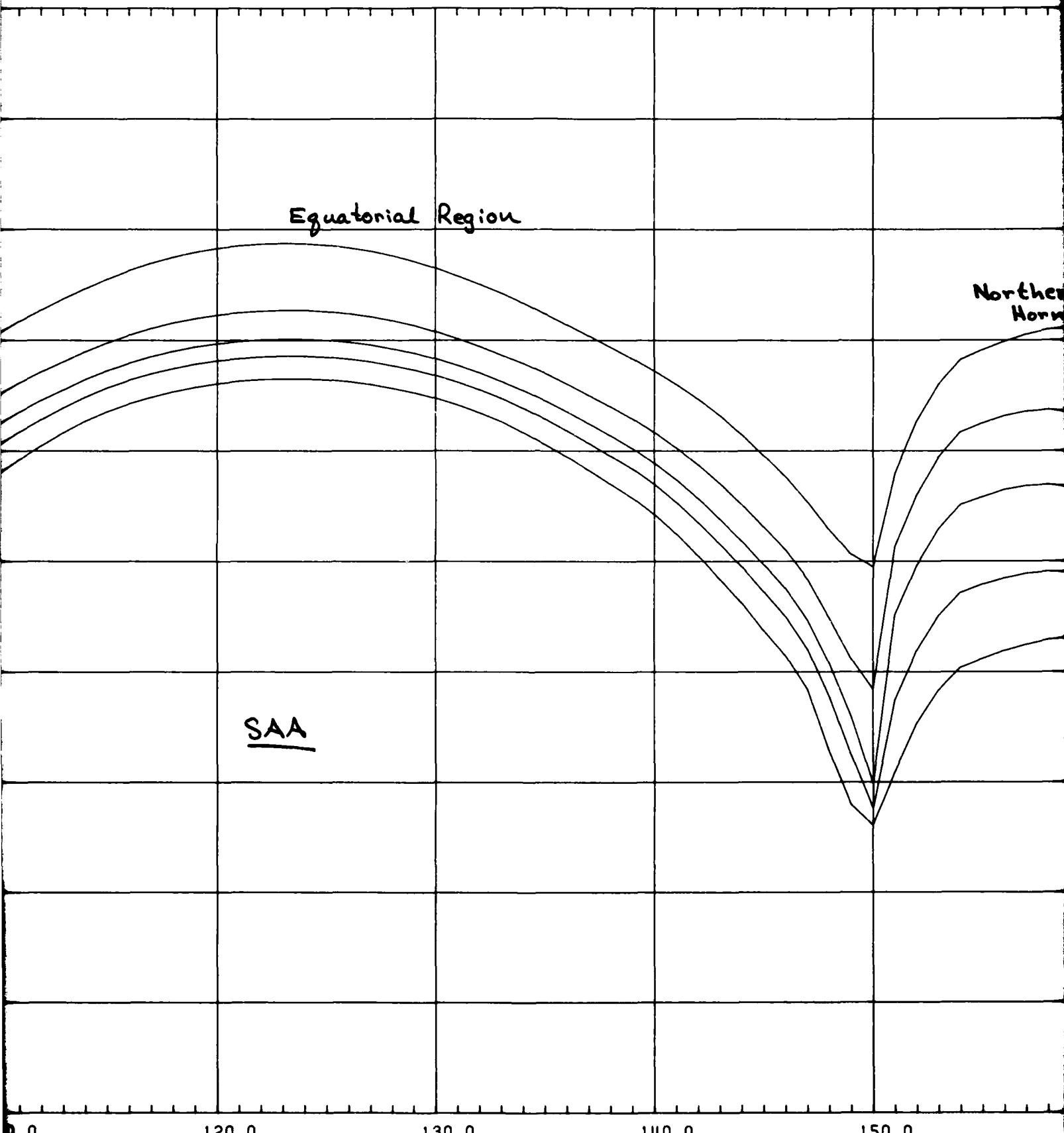


Figure 133

ORBIT: NAVELEX 3
60 DGR/3889-3889 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 LO

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

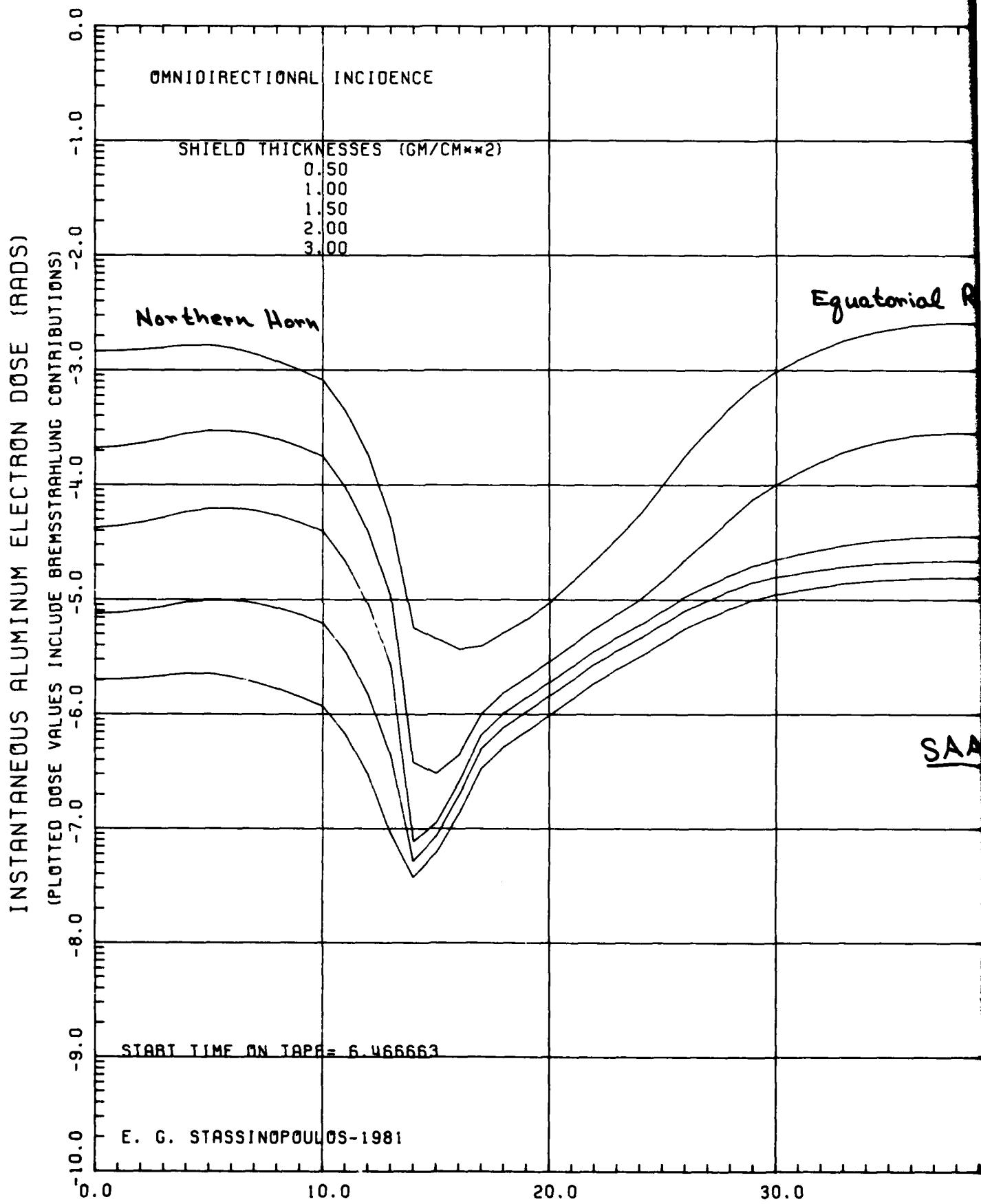
UN FACTORS: NOT APPLIED

Northern
Horn

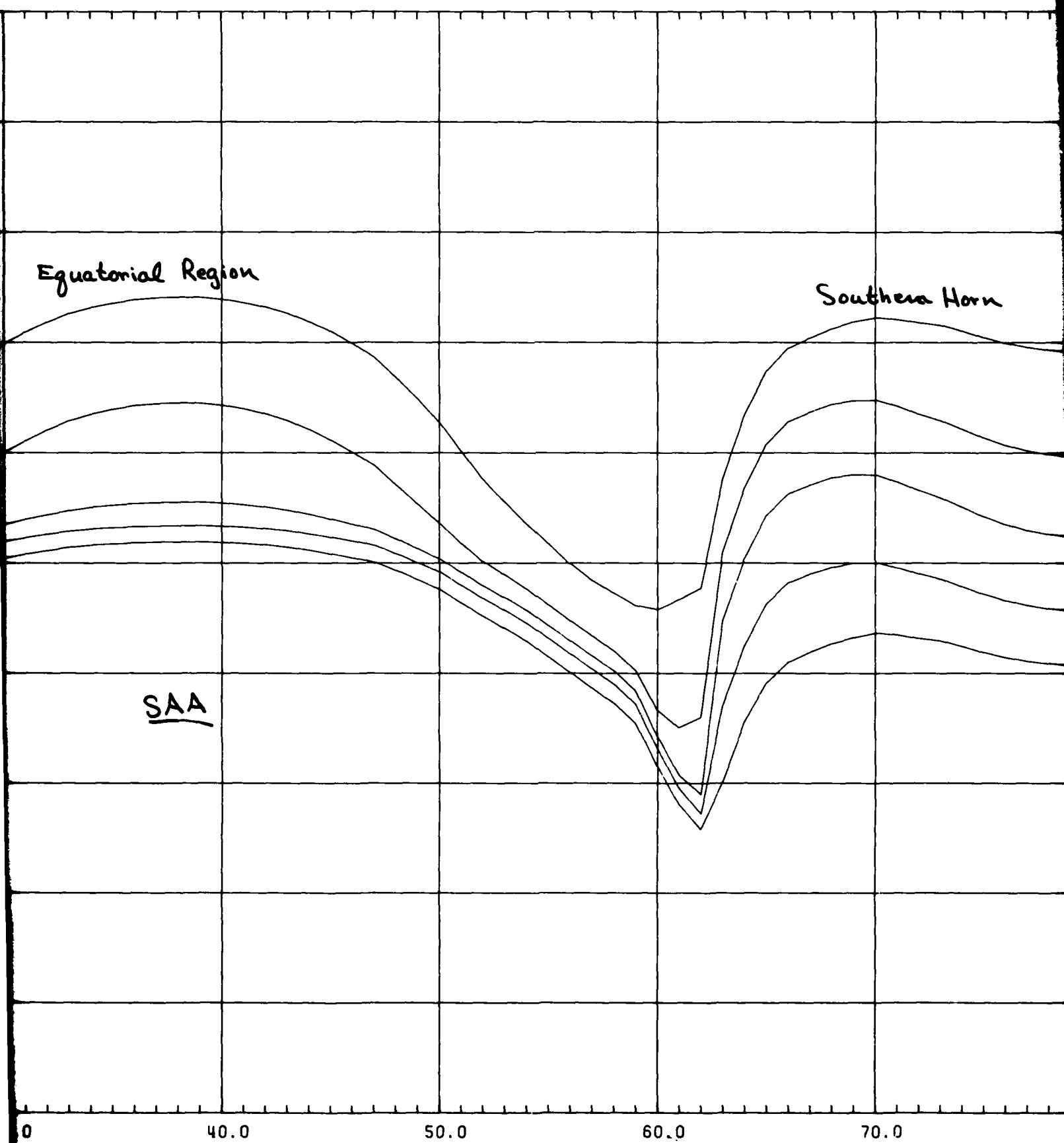
STOP TIME ON TAPF = 9.316662

NASA-GSFC

0.0 160.0 170.0 180.0



2'

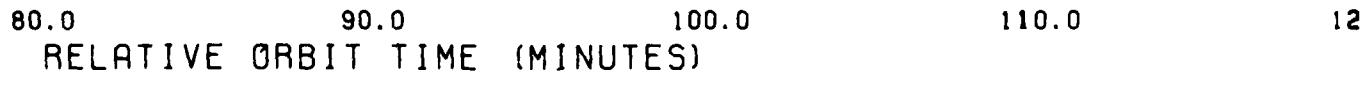


3

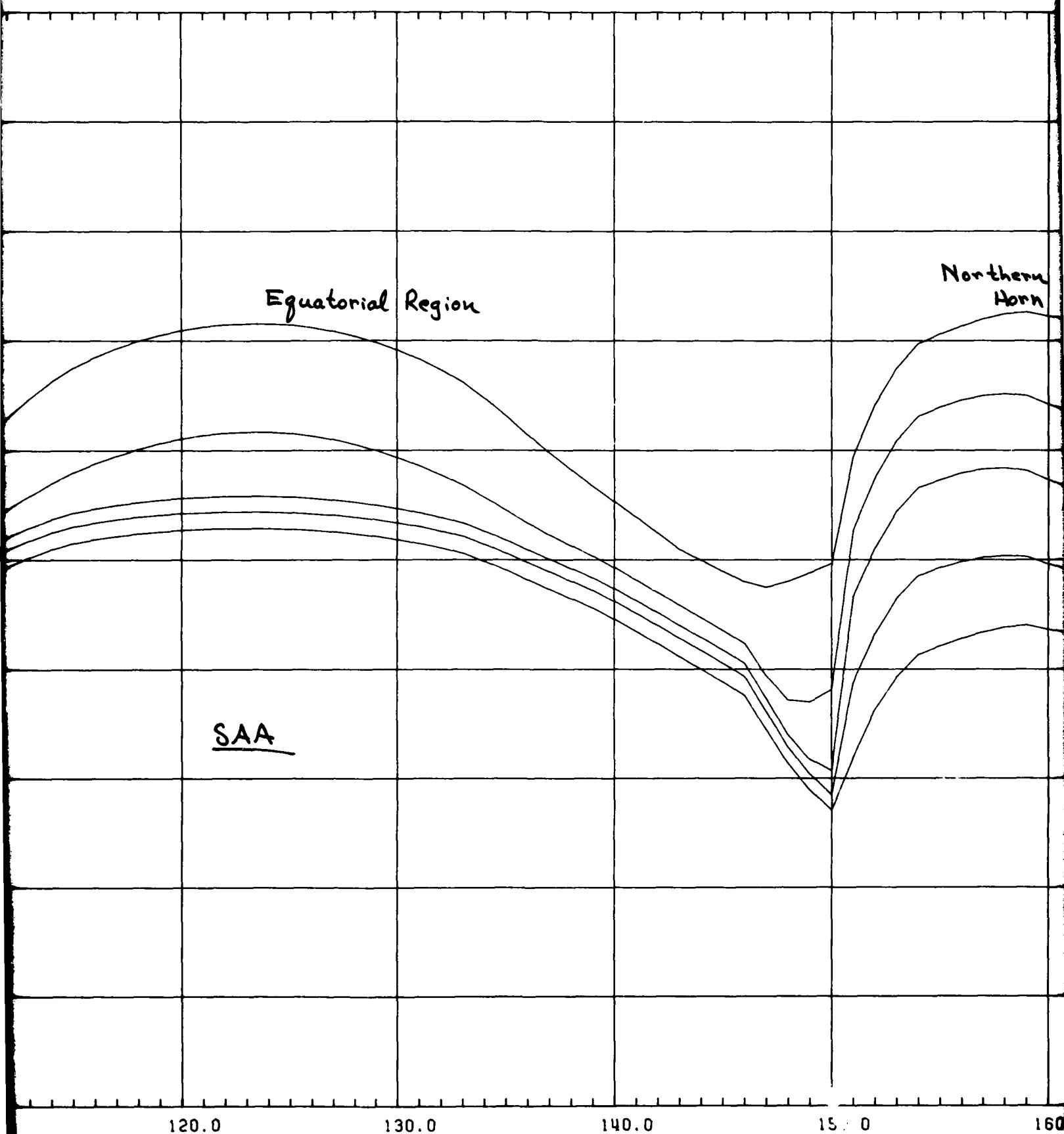
DOSE IN SEMI-INFINITE ALUMINUM MEDIUM

ma Horn

Southern Horn



14



120.0

130.0

140.0

15.0

160

Figure 134

ORBIT: NAVELEX 8
60 DGR/3889-3889 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 LO

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern Horn

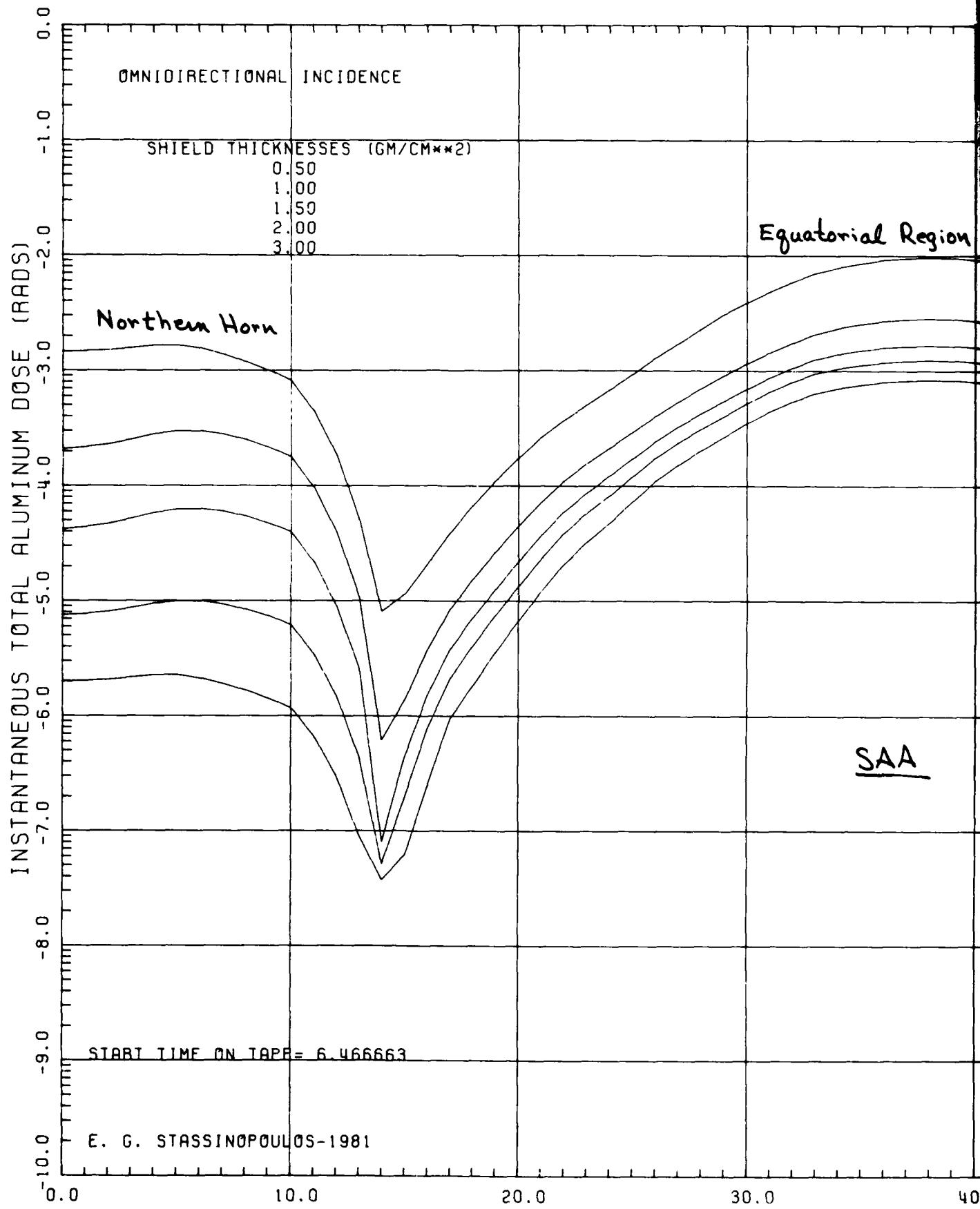
STOP TIME ON TAPE = 9.316662

NASA-GSFC

160.0

170.0

180.0



Equatorial Region

Southern Horn

SAA

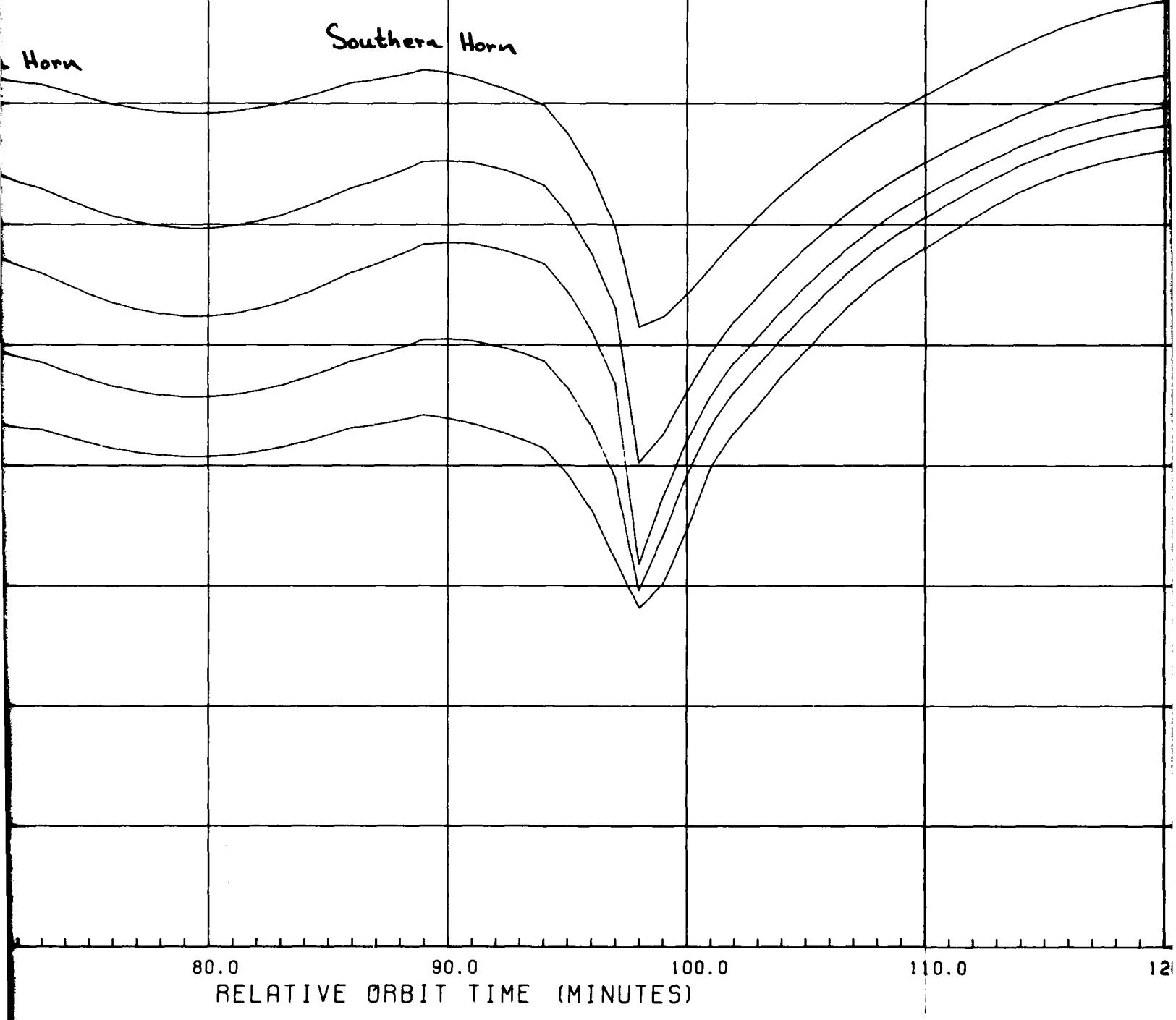
40.0

50.0

60.0

70.0

13
DOSE IN SEMI-INFINITE ALUMINUM MEDIUM



4

Equatorial Region

Northern Horn

SAA

120.0

130.0

140.0

150.0

160

Figure 135

ORBIT: NAVELEX 8
60 DGR/3889-3889 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 LO

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern
Horn

STOP TIME ON TAPE = 9.316662

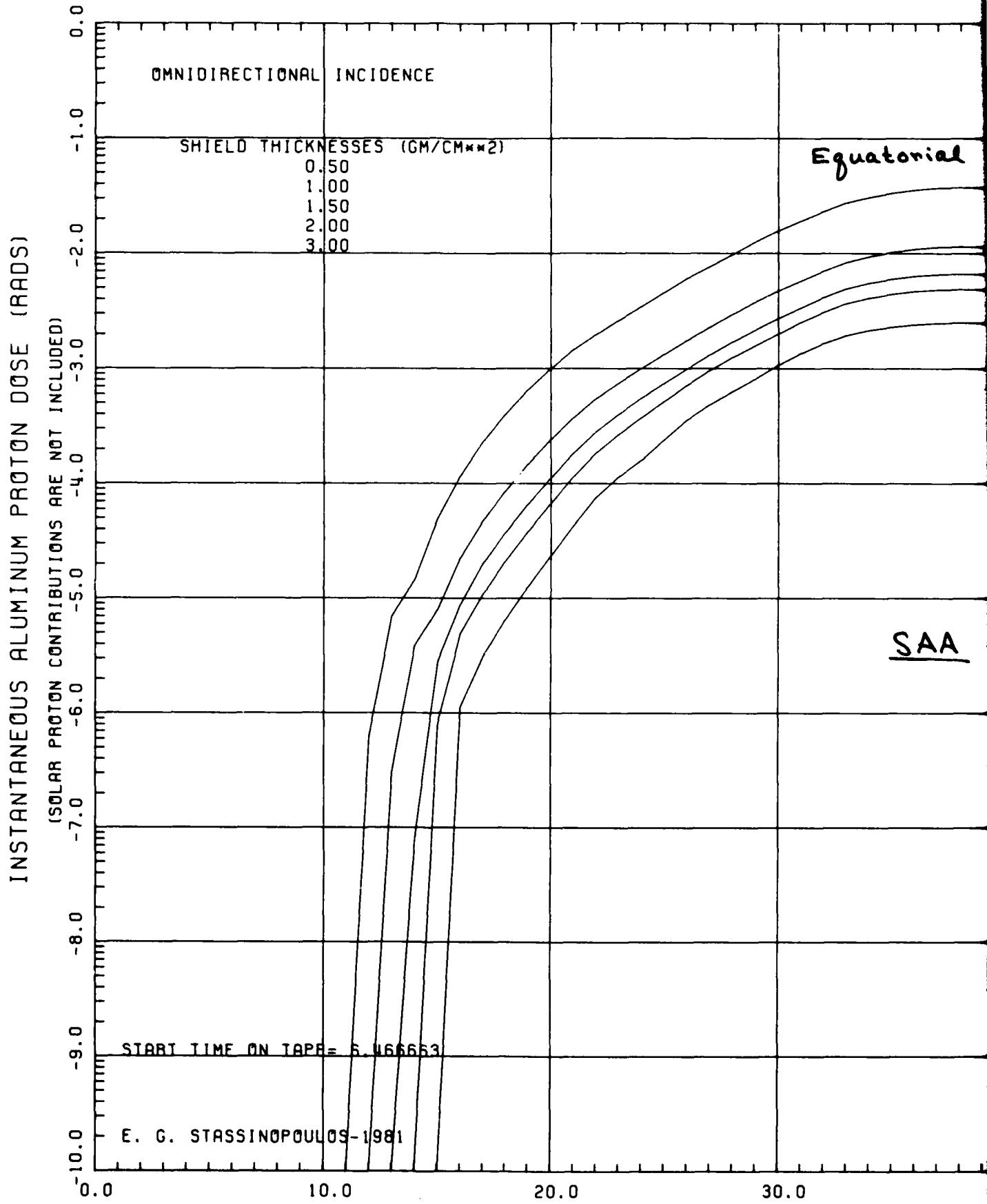
NASA-GSFC

150.0

160.0

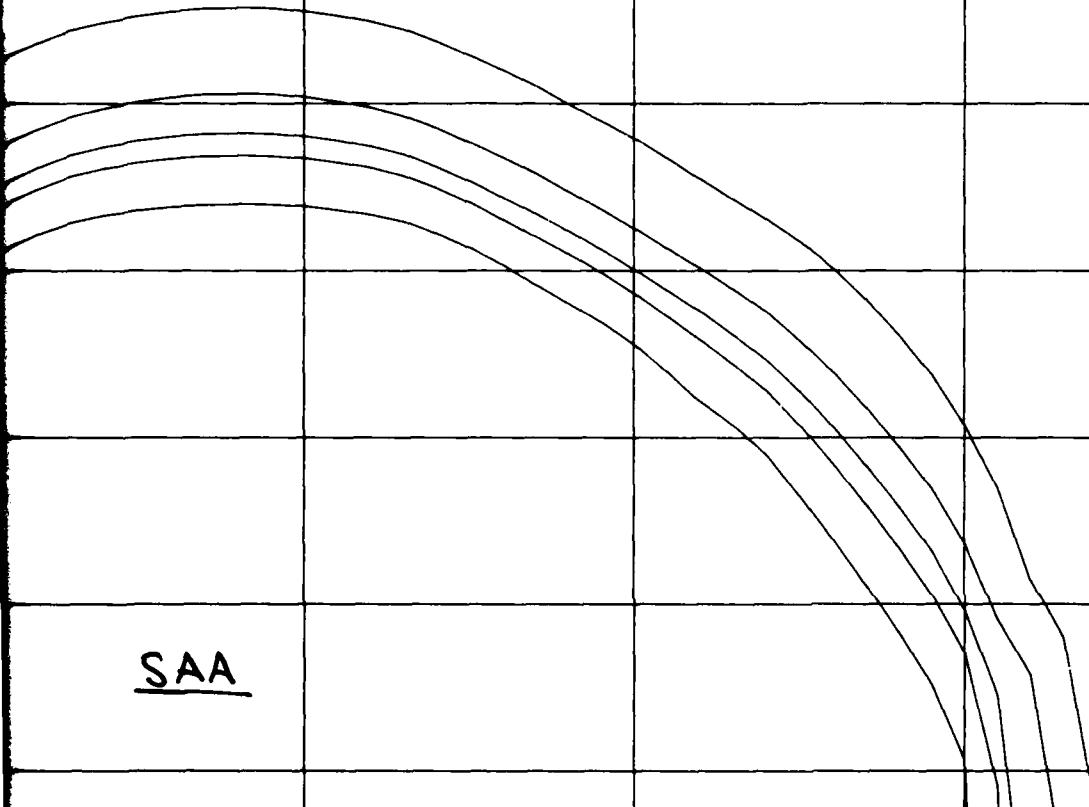
170.0

180.0



2

Equatorial Region



SAA

40.0

50.0

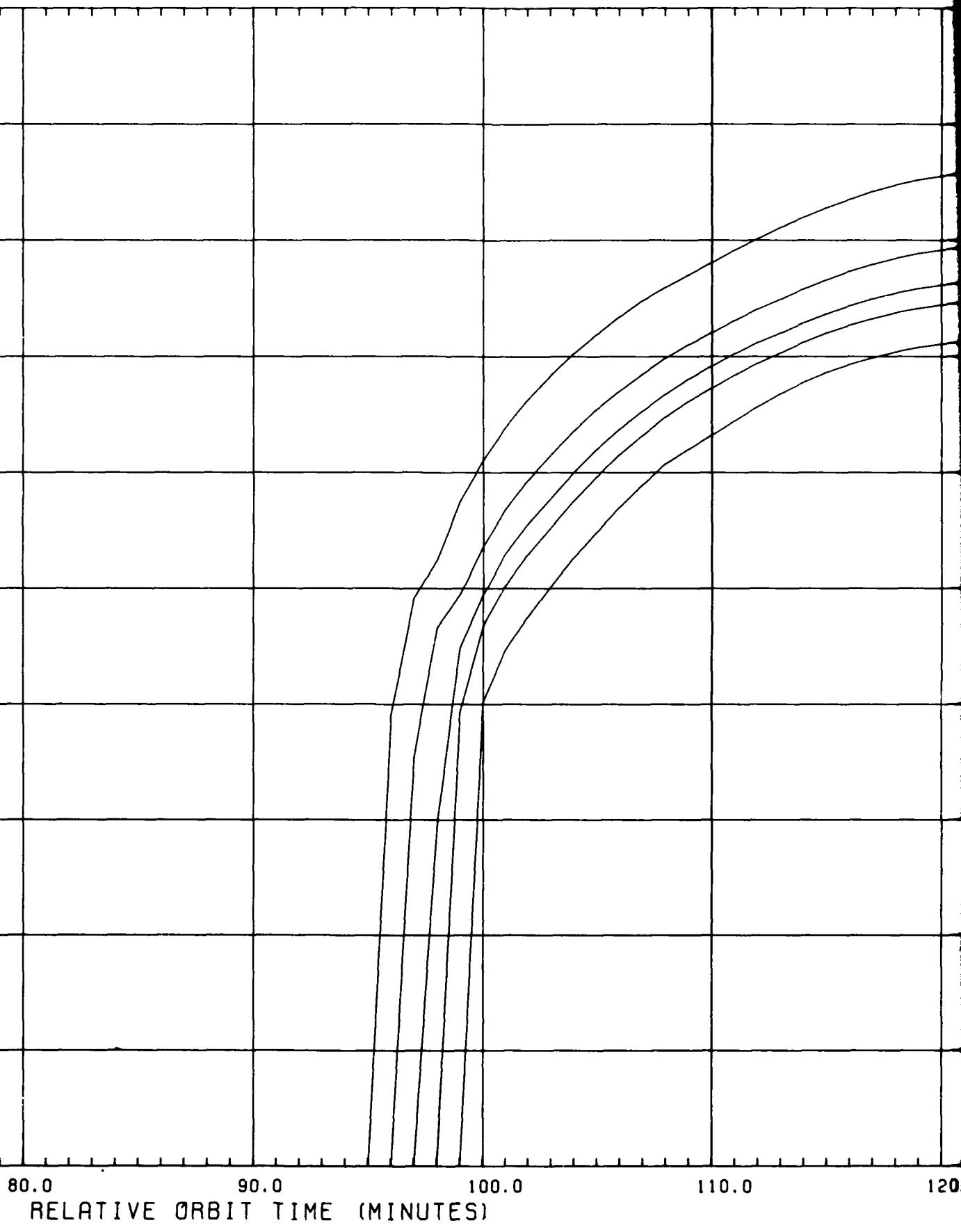
60.0

70.0

80

3

DOSE AT CENTER OF ALUMINUM SICKLES



4

Equatorial Region

SAA

120.0

130.0

140.0

150.0

160.0

Figure 13b

5

ORBIT: NAVELEX 3
60 OGR/3889-3889 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

STOP TIME ON TAPF = 9.316662

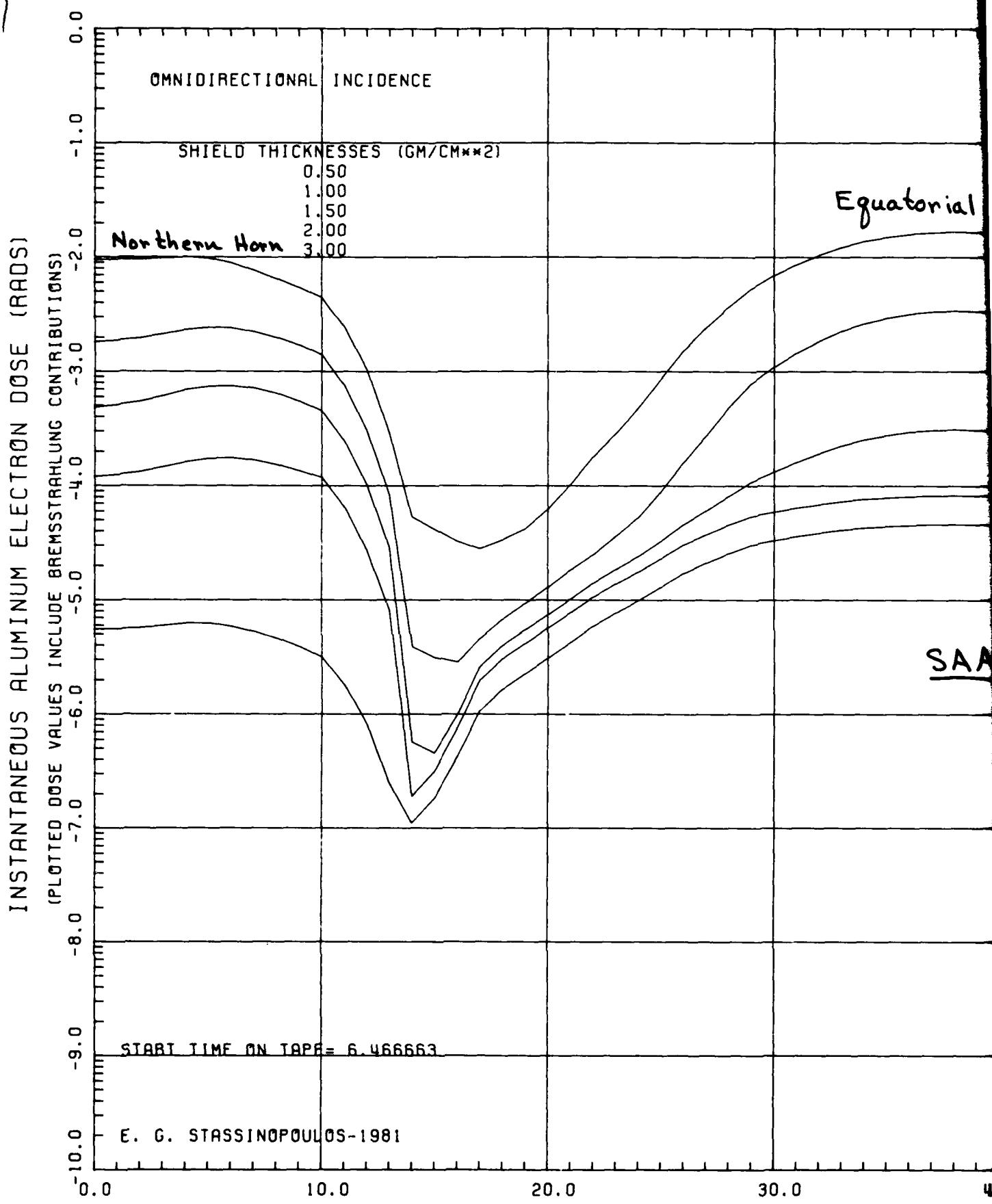
NASA-GSFC

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170.0

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Equatorial Region

Southern Horn

SAA

40.0

50.0

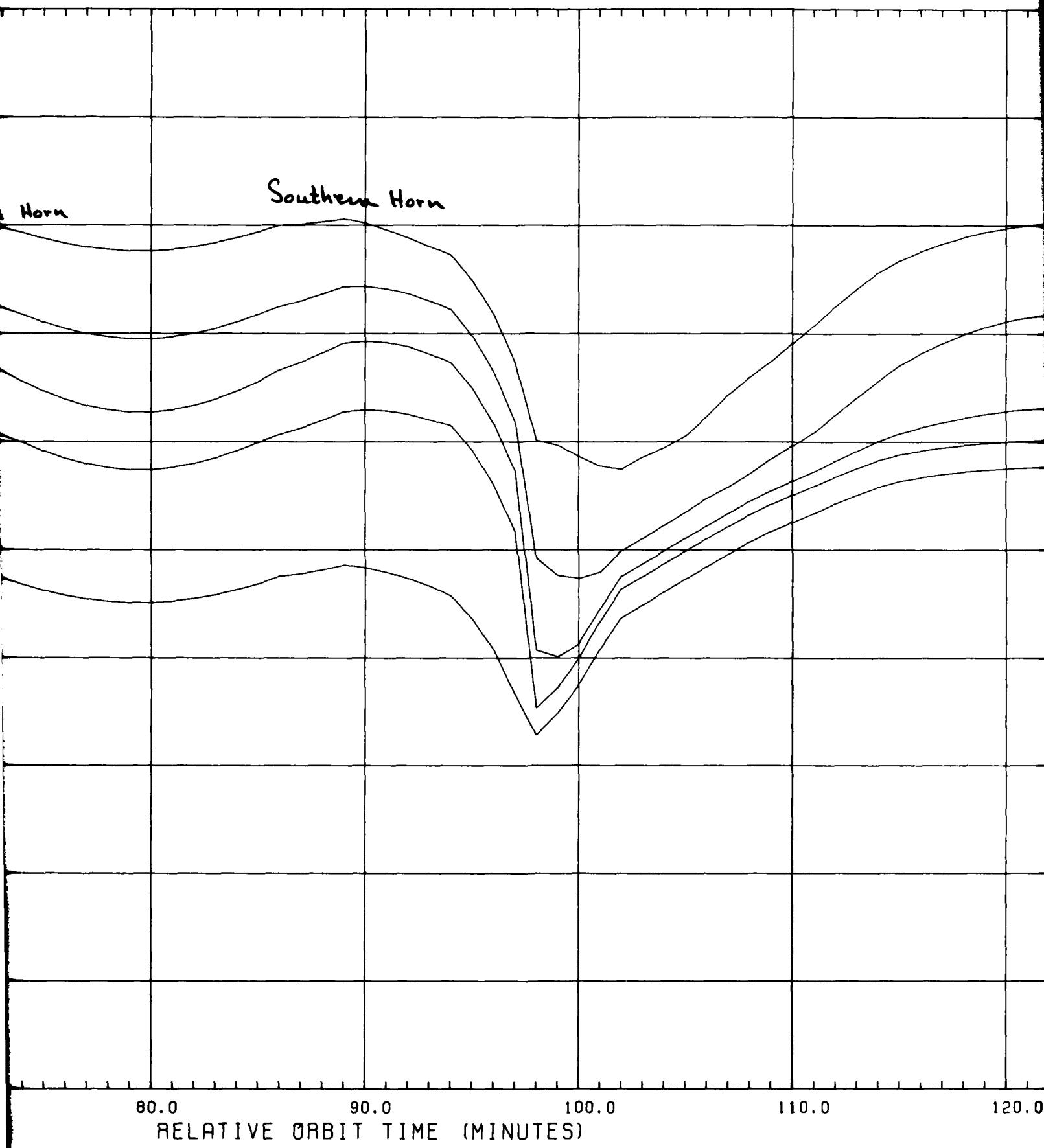
60.0

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REI

3
DOSE AT CENTER OF ALUMINUM SPHERES



'U

Equatorial Region

Northern Horn

SAA

120.0

130.0

140.0

150.0

160.0

Figure 137

ORBIT: NAVELEX 3
60 DGR/3889-3889 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: RP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

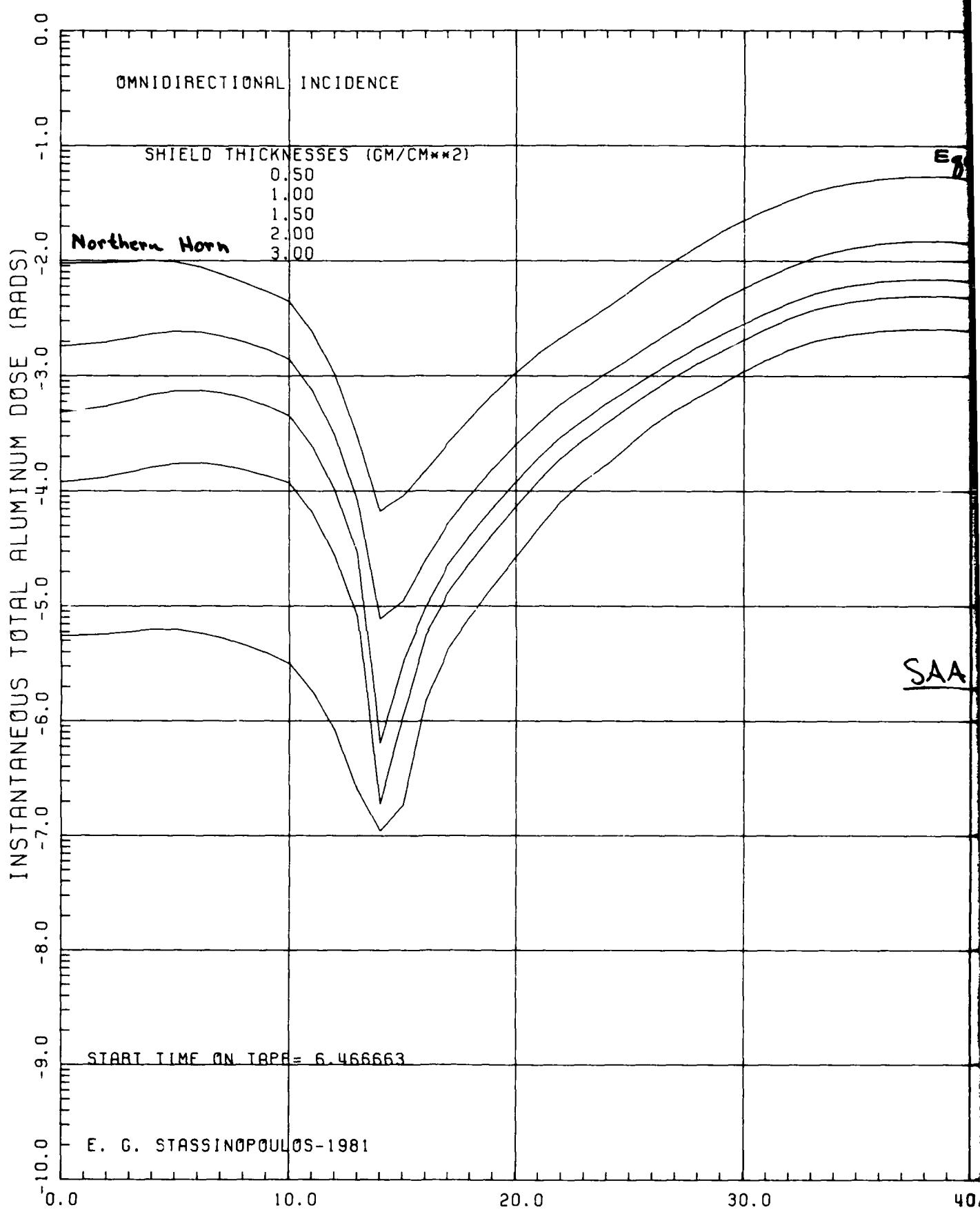
UN FACTORS: NOT APPLIED

Northern Horn

STOP TIME ON TAPE = 9.316662

NASA-GSFC

0 160.0 170.0 180.0



2

Equatorial Region

Southern Hor

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50.0

60.0

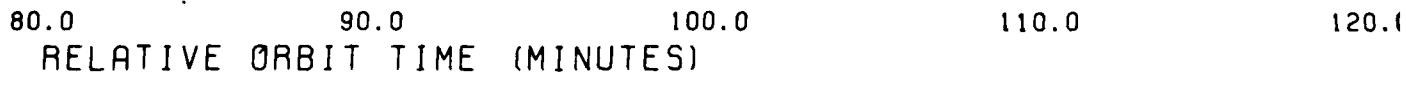
70.0

80

DOSE AT CENTER OF ALUMINUM SPHERES

Southern Horn

Southern Horn



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6

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Equatorial Region

Northern Horn

SAA

120.0

130.0

140.0

150.0

160.0

Figure 138

ORBIT: NAVELEX 3
60 DGR/3889-3889 KM

EPOCH: 1989.5

Northern
Horn

MODELS:
FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AEI7-L8
MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

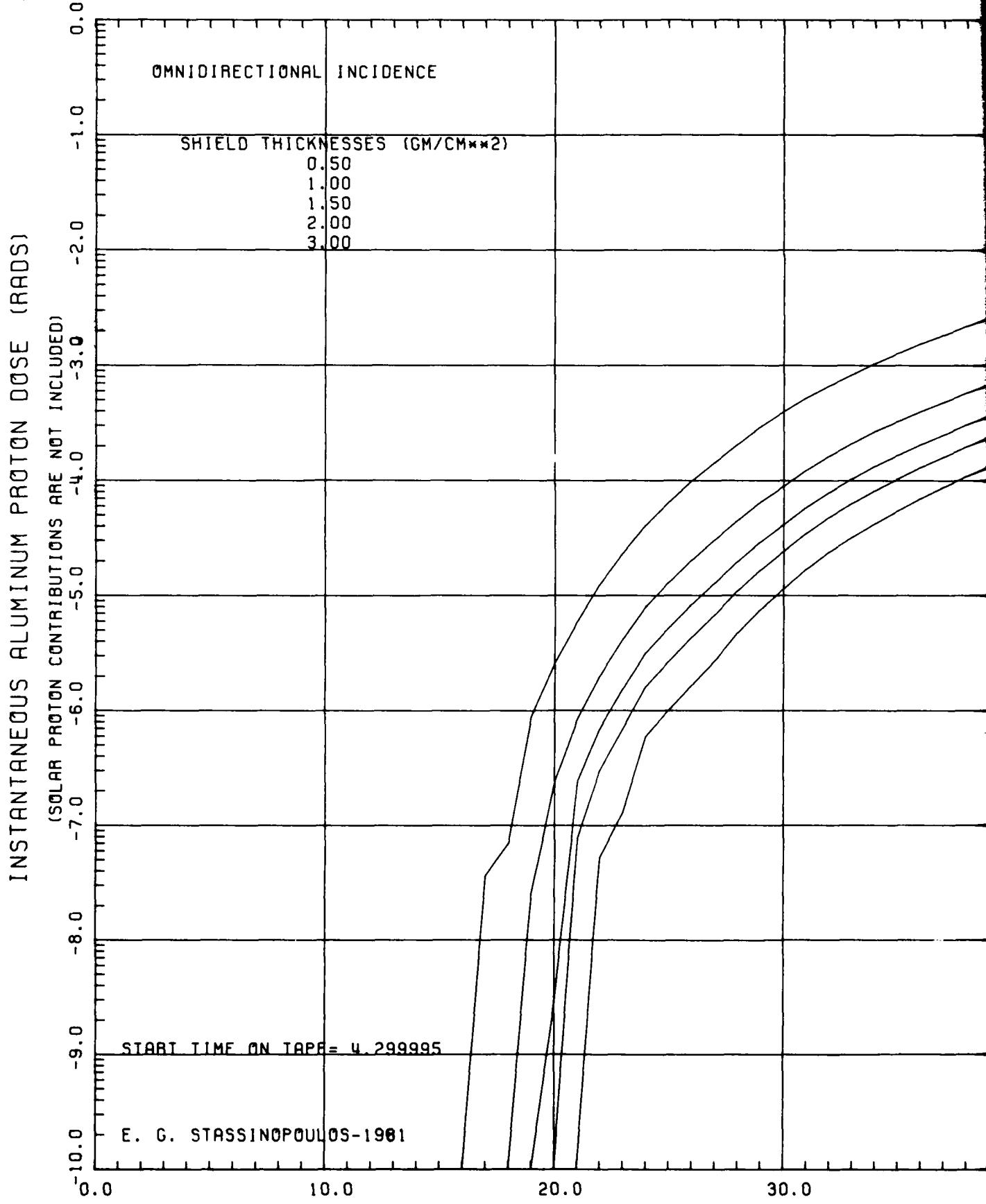
STOP TIME ON TAPF = 9.316662

NASA-GSFC

160.0

170.0

180.0



Equatorial Region

SAA

40.0

50.0

60.0

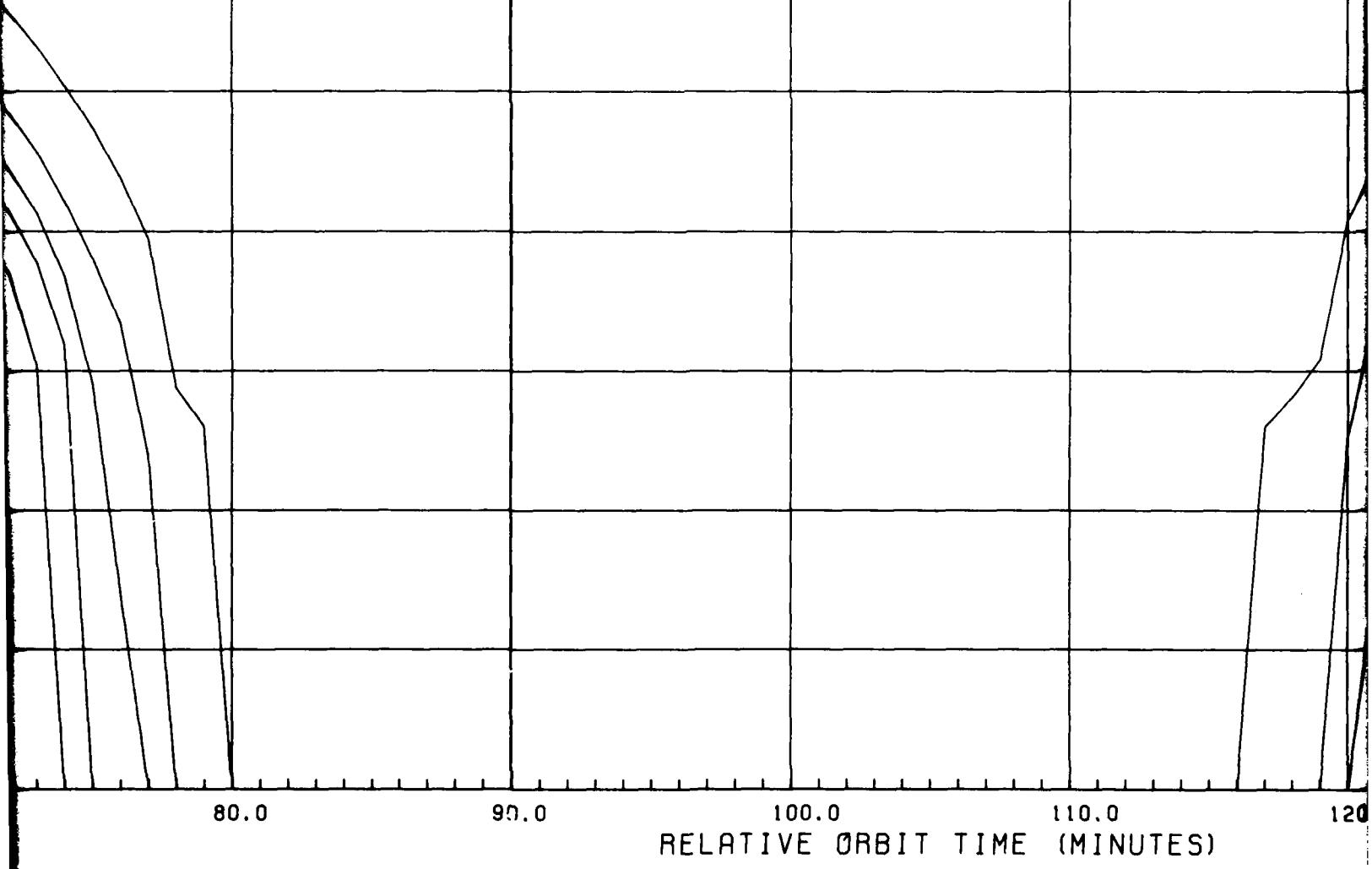
70.0

8

3

DOSE AT TRANSMISSION SURFACE OF FINITE ALUMINUM

ζ = DOSE IN SEMI-INFINITE ALUMINUM MEDIUM



4

TE ALUMINUM SLAB SHIELDS

UMINUM MEDIUM)

Equatorial Re

SAA

(TES)

120.0

130.0

140.0

150.0

160.

5

ORBIT: NAVELE
60 DGR/5186

EPOCH: 1989.5

MODELS:
FIELD: BARR/
TRAPPED PROT
INNER ZN ELE
OUTER ZN ELE
MISSION DURAT
EVALUATION PHA

UN FACTORS: NO

Equatorial Region

SAA

STOP TIME ON T

0

160.0

170.0

180.0

190.0

Figure 139

ORBIT: NAVELEX 4
60 DGR/5186-5186 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

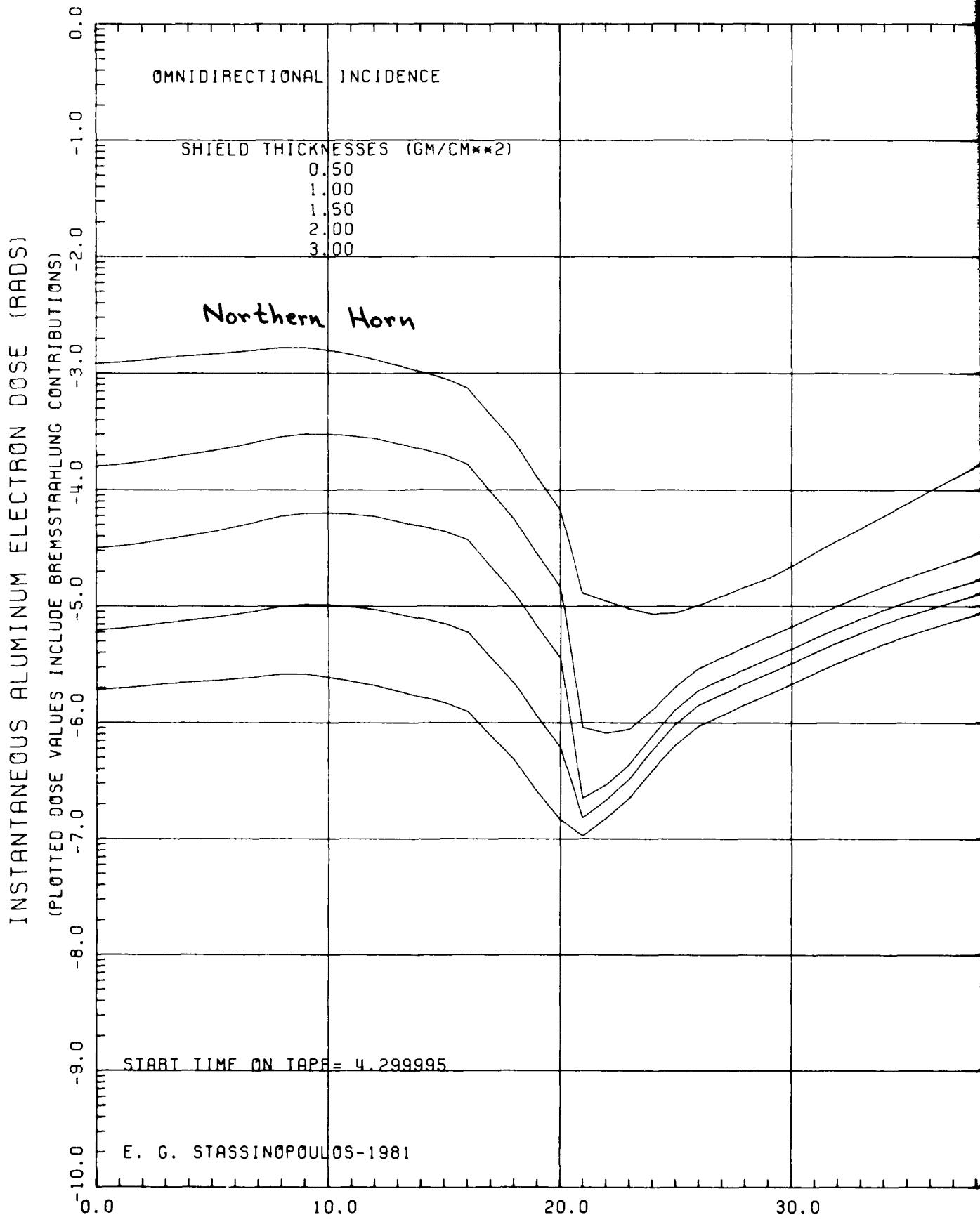
STOP TIME ON TAPF = 7.716662

NASA-GSFC

190.0

200.0

210.0



Equatorial Region

SAA

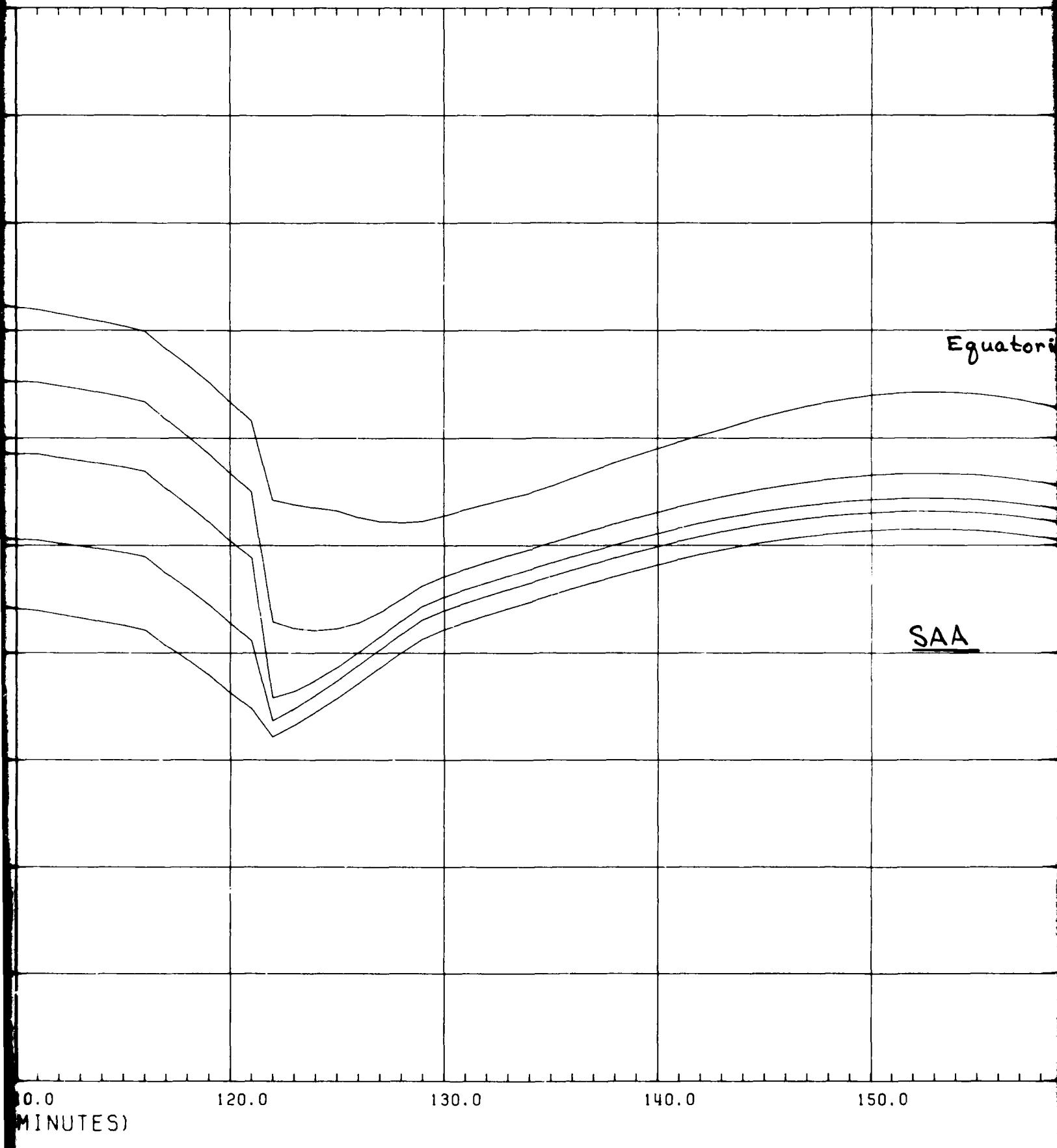
0 40.0 50.0 60.0 70.0

DOSE AT TRANSMISSION SURFACE OF FINITE ALUMINU

Southern Horn



FINITE ALUMINUM SLAB SHIELDS



5

ORBIT: NA
60 DGR/

EPOCH: 19

MODELS:
FIELD: B
TRAPPED
INNER ZN
OUTER ZN
MISSION D
EVALUATION
UN FACTORS

Equatorial Region

Northern
Horn

SAA

STOP TIME

150.0

160.0

170.0

180.0

190.0

Figure 140

ORBIT: NAVELEX
60 DGR/5186-5186 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern
Horn

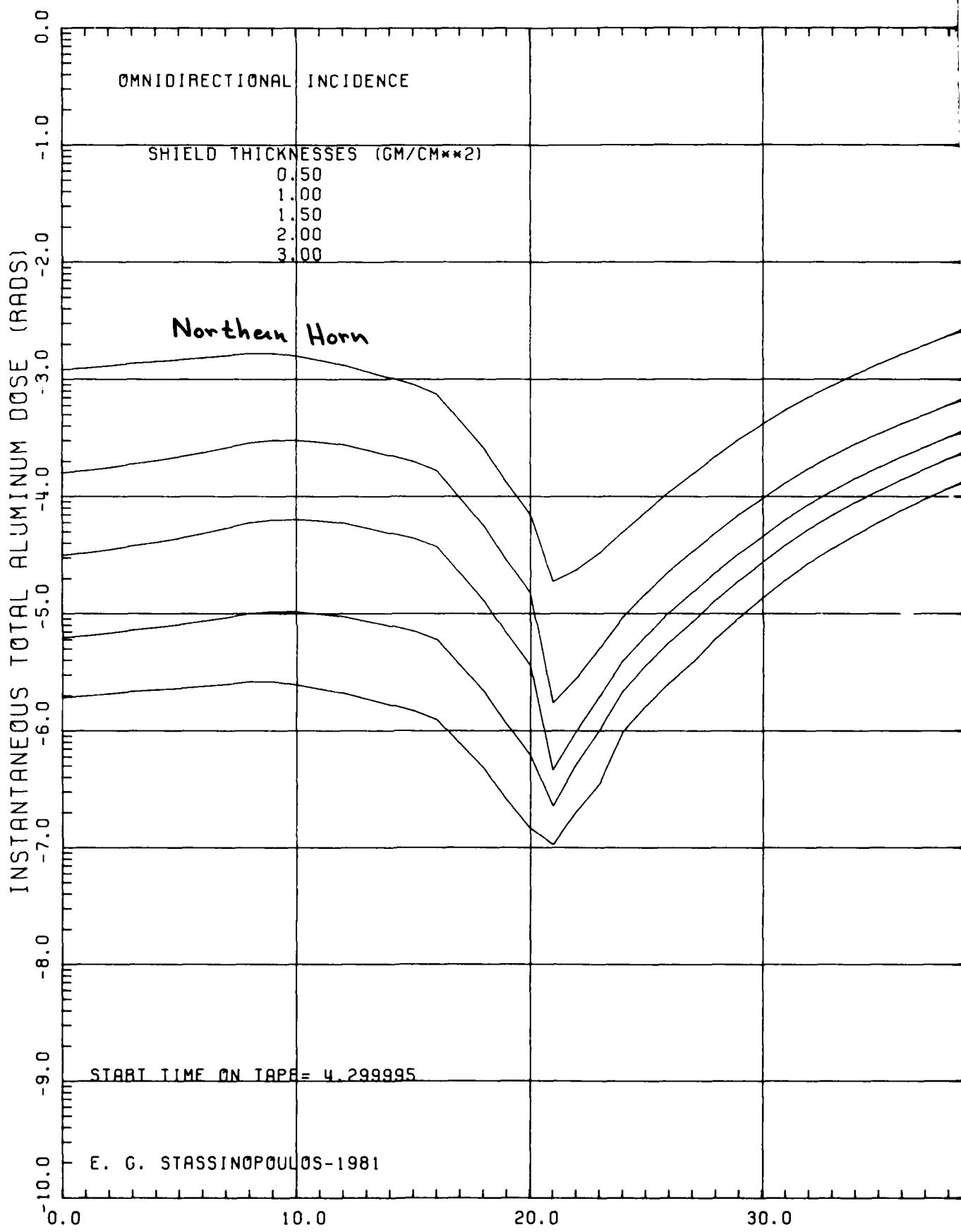
STOP TIME ON TAPF = 7.716662

NASA-GSFC

190.0

200.0

210.0



Equatorial Region

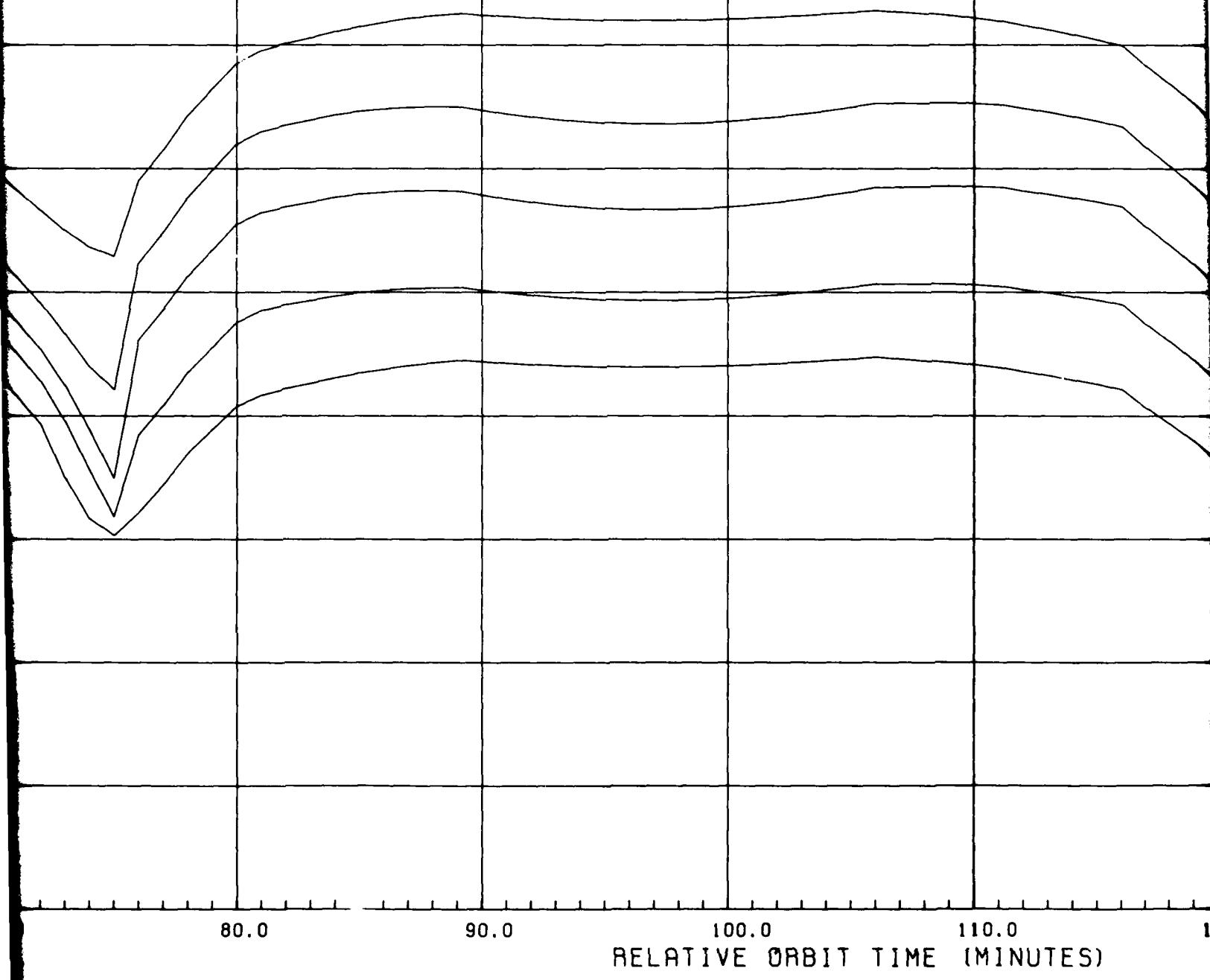
SAA

40.0 50.0 60.0 70.0

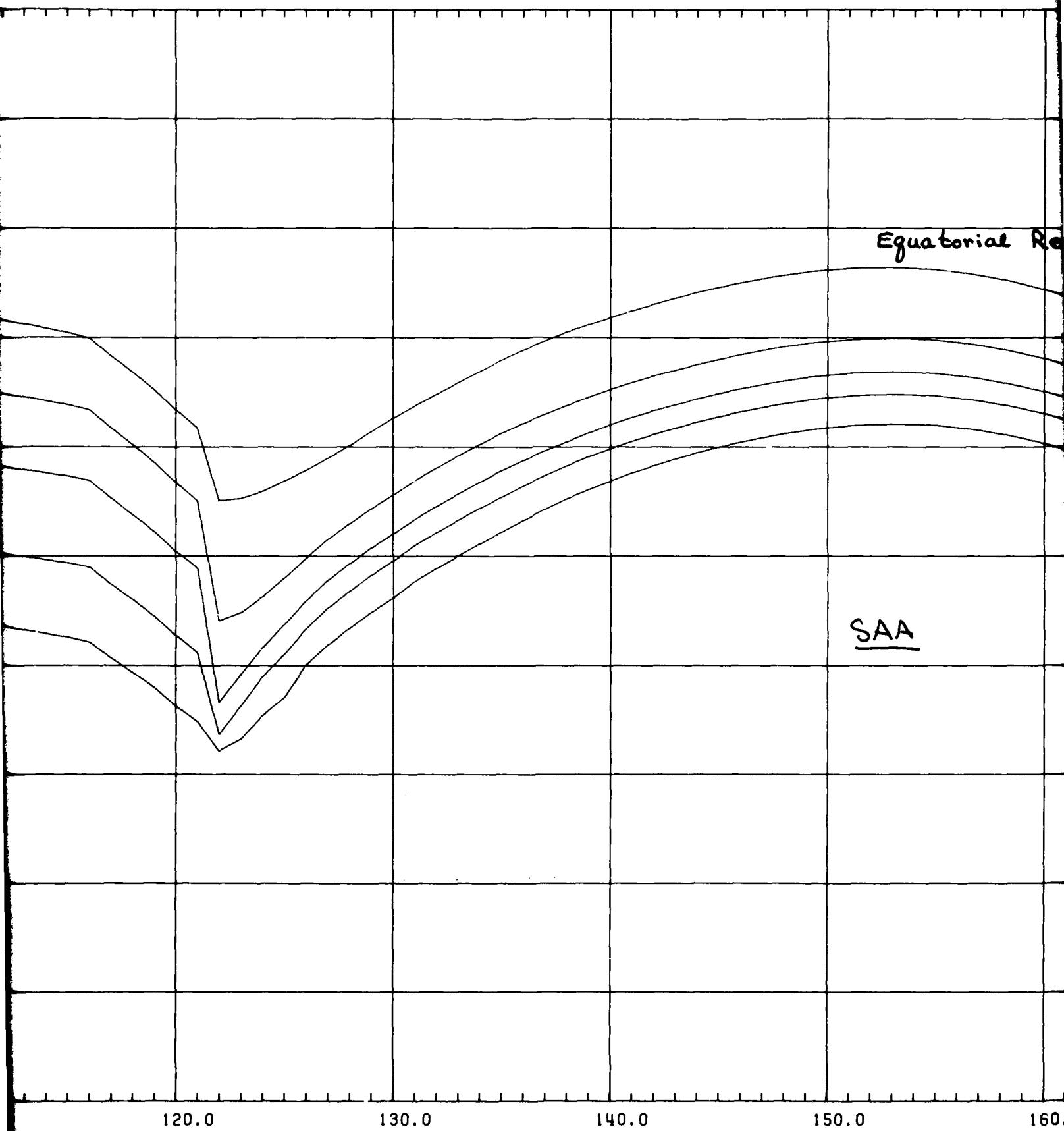
3

DOSAGE AT TRANSMISSION SURFACE OF FINITE ALUMINU

Southern Horn



4
TE ALUMINUM SLAB SHIELDS



5
ORBIT: NAVELEX
60 DGR/5186-

EPOCH: 1989.5

MODELS:
FIELD: BARR/7
TRAPPED PROTO
INNER ZN ELEC
OUTER ZN ELEC

MISSION DURATI
EVALUATION PHA

UN FACTORS: NO

Equatorial Region

Northern
Horn

SAA

STOP TIME ON T

0 160.0 170.0 180.0 190.0

Figure 141

ORBIT: NAVELEX
60 DGR/5186-5186 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 LG

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

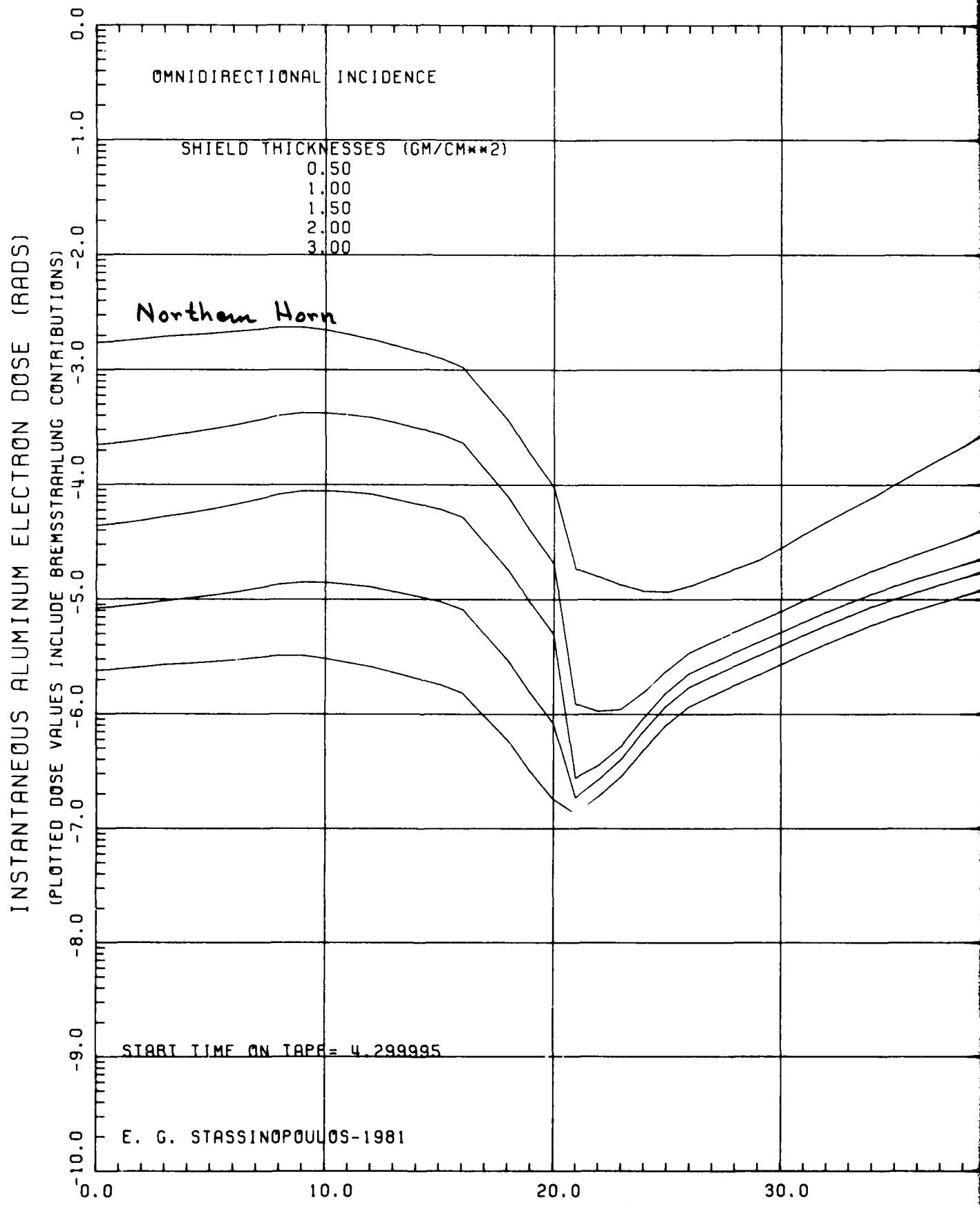
STOP TIME ON TAPF = 7.716662

NASA-GSFC

190.0

200.0

210.0



Equatorial Region

SAA

40.0 50.0 60.0 70.0 80.0

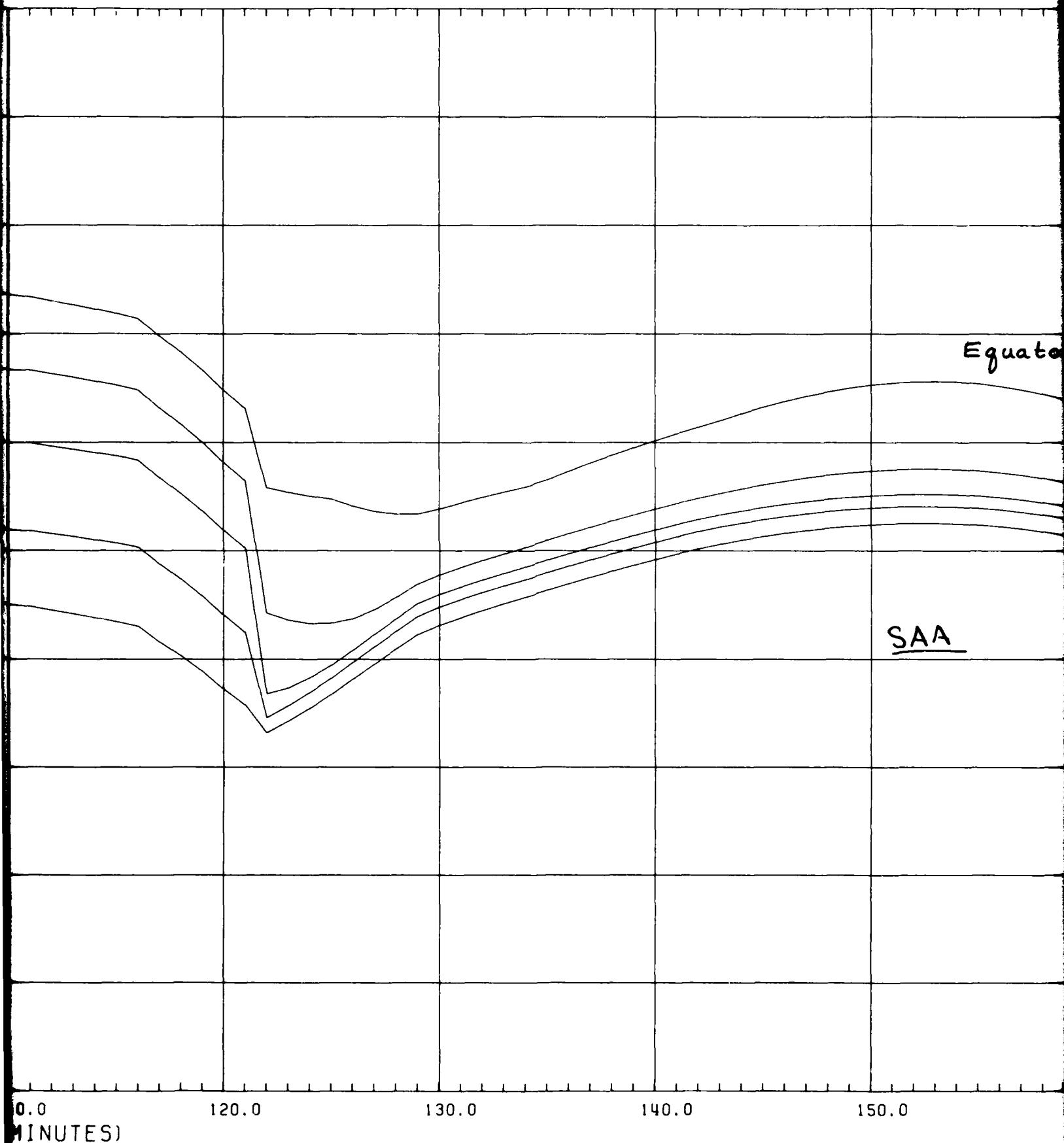
3

DOSE IN SEMI-INFINITE ALUMINUM MEDIUM

Southern Horn

80.0 90.0 100.0 110.0 120
RELATIVE ORBIT TIME (MINUTES)

LUMINUM MEDIUM



0.0
(MINUTES)

ORBIT: NAVELEX
60 DGR/5186

EPOCH: 1989.5

MODELS:
FIELD: BARR/T
TRAPPED PROTO
INNER ZN ELEC
OUTER ZN ELEG
MISSION DURATI
EVALUATION PHA

UN FACTORS: NO

Northern
Horn

Equatorial Region

SAA

STOP TIME ON I

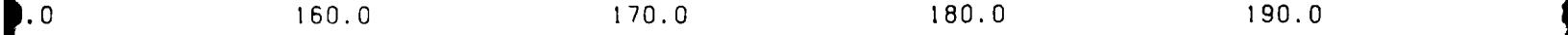


Figure 142

ORBIT: NAVELEX 4
60 DGR/5186-5186 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN-FACTORS: NOT APPLIED

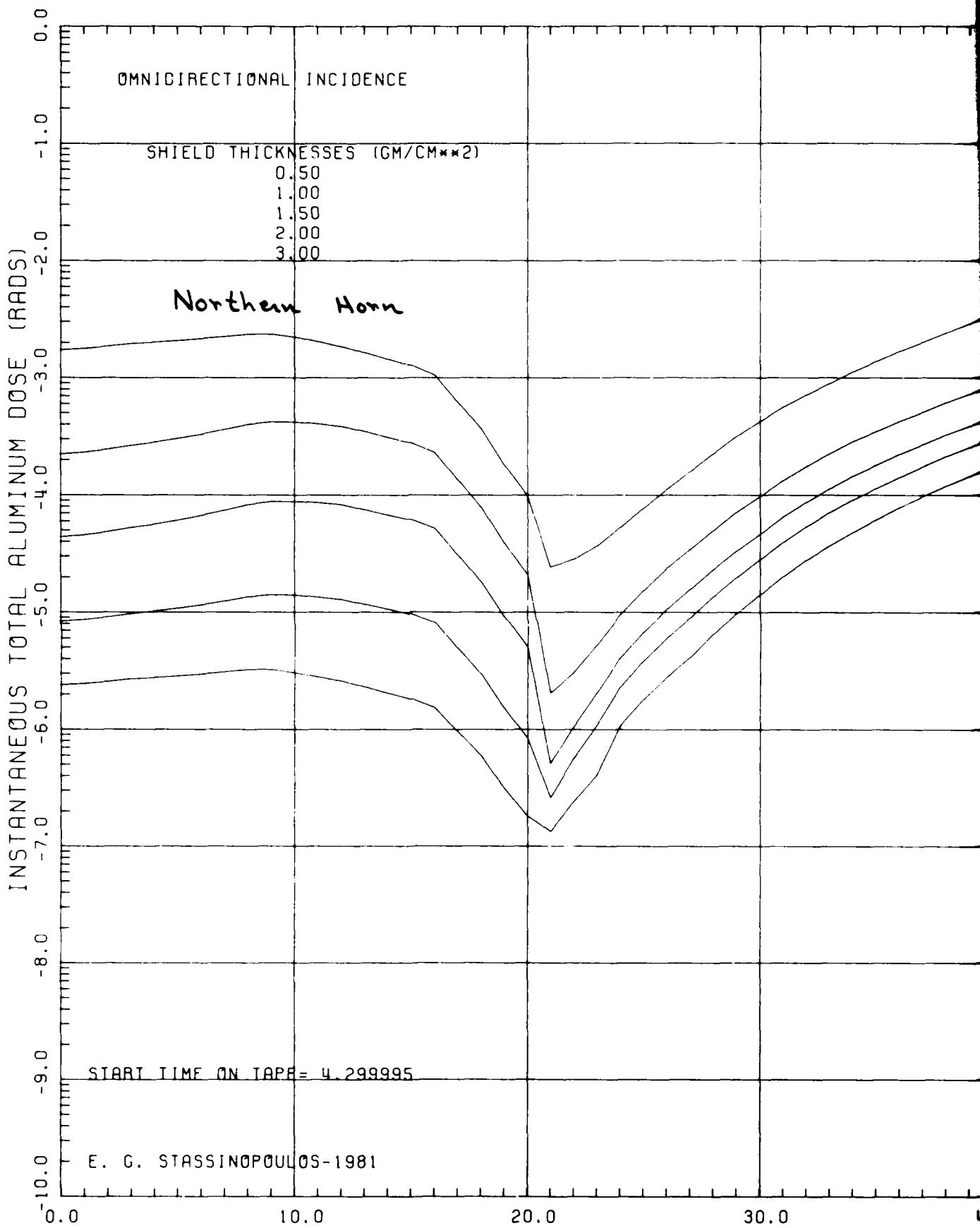
STOP TIME ON TAPE = 7.716662

NASA-GSFC

190.0

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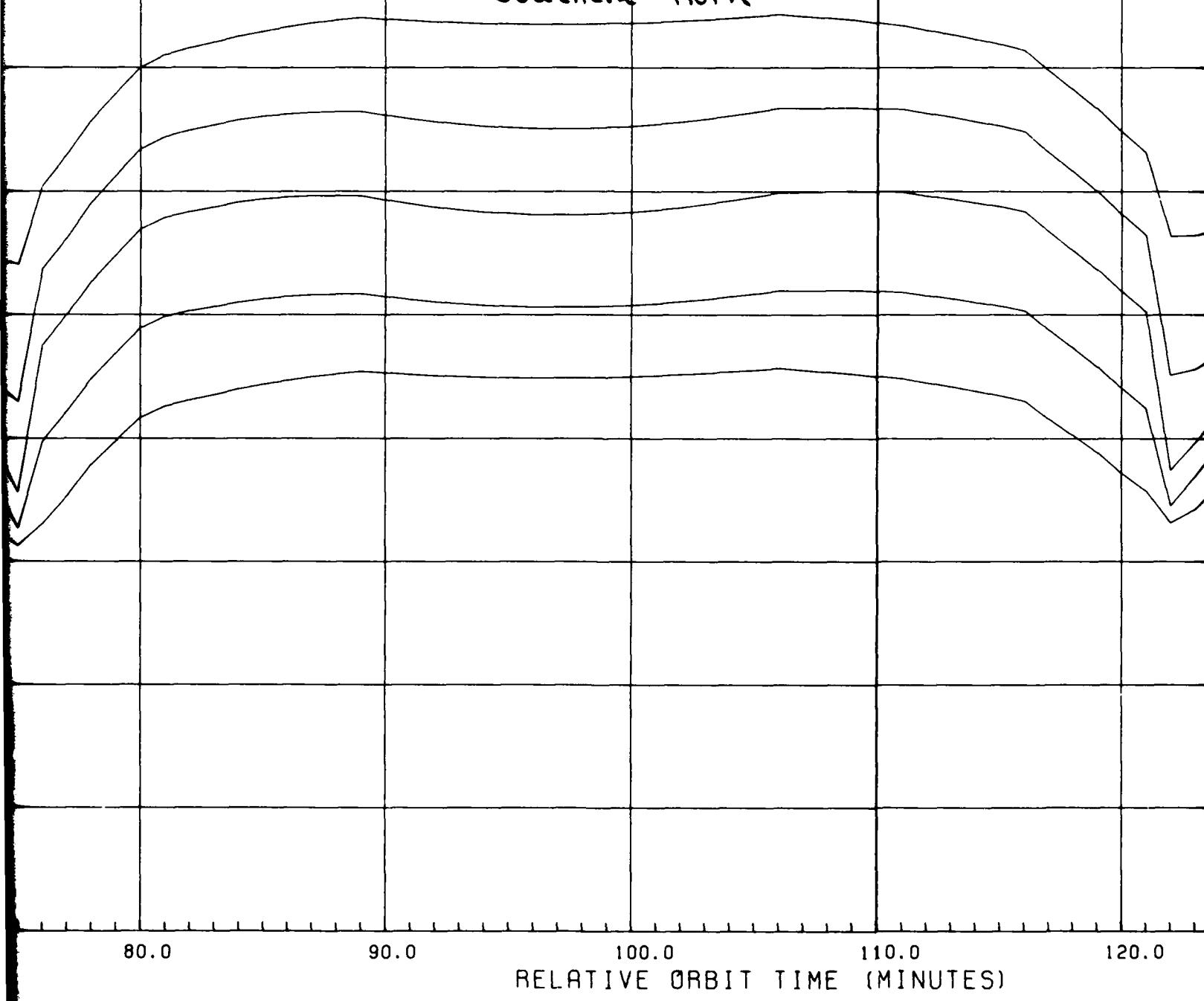
Equatorial Region

SAA

40.0 50.0 60.0 70.0 80.0

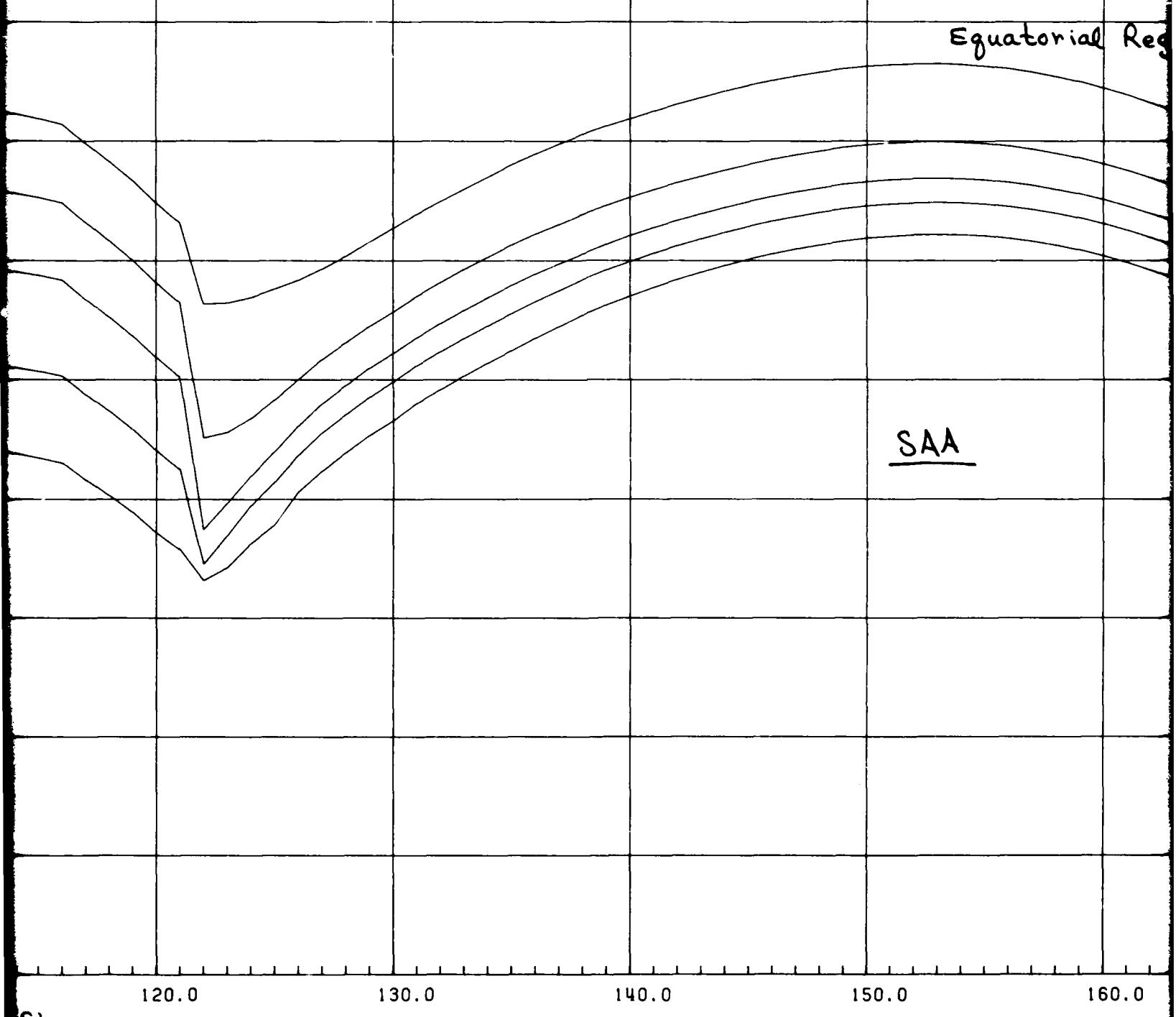
DOSE IN SEMI-INFINITE ALUMINUM MEDIUM

Southern Horn



UM MEDIUM

4



S)

5.

ORBIT: NAVELEX
60 DGR/5186-51

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS:

INNER ZN ELEC: R

OUTER ZN ELEC: R

MISSION DURATION:

EVALUATION PHASE:

UN FACTORS: NOT A

Equatorial Region

Northern Horn

AA

STOP TIME ON TAPE

160.0

170.0

180.0

190.0

200.

Figure 143

ORBIT: NAVELEX
60 DGR/5186-5186 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

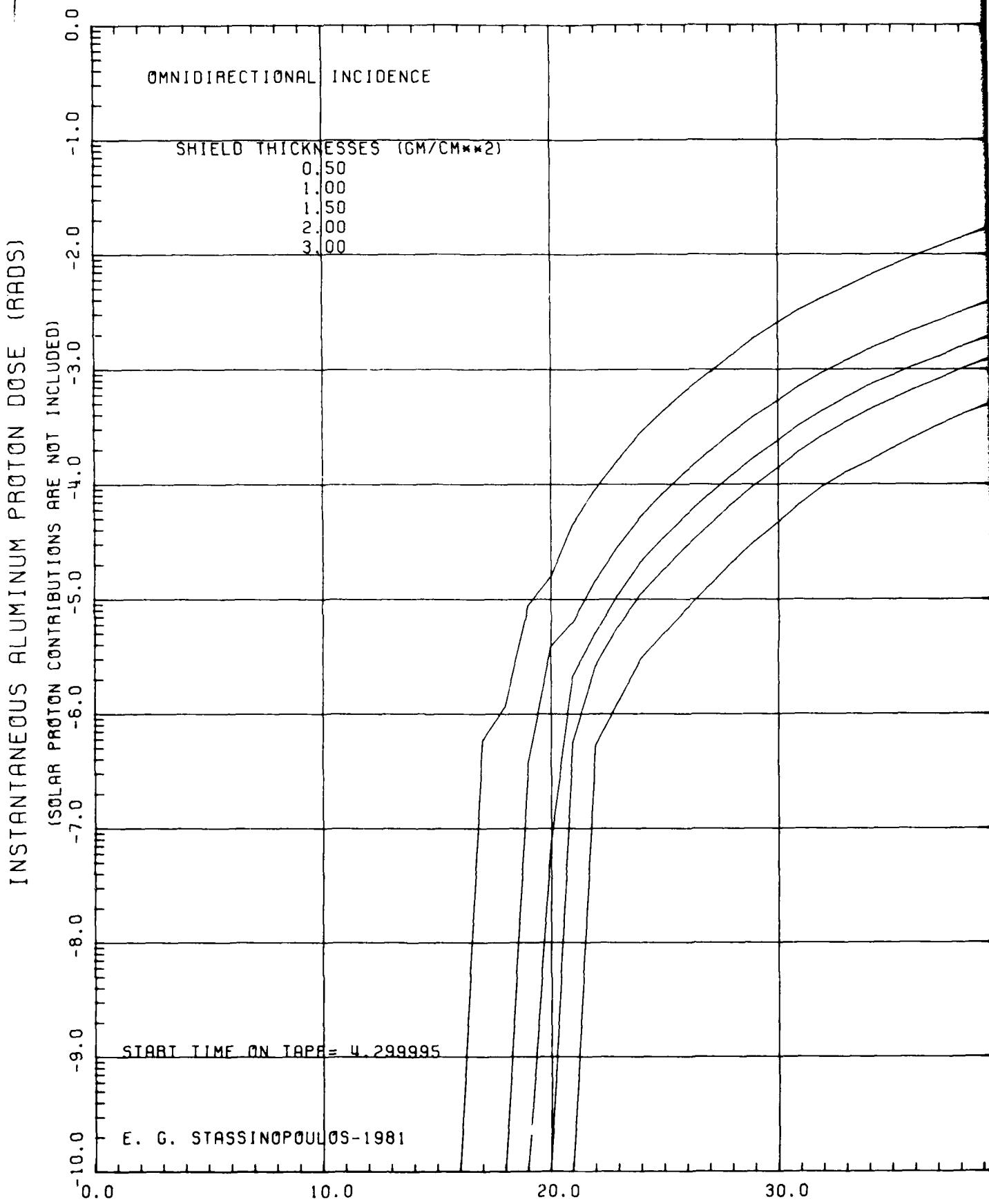
STOP TIME ON TAPF = 7.716662

NASA-GSFC

190.0

200.0

210.0



12

Equatorial Region

SAA

40.0

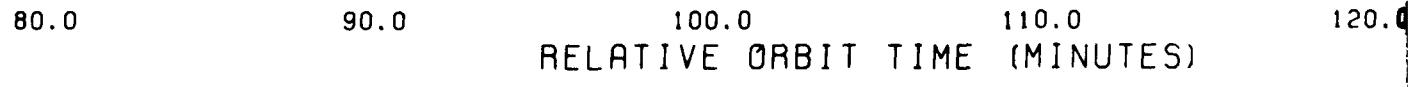
50.0

60.0

70.0

80.

DOSE AT CENTER OF ALUMINUM SPHERES



ERES

Li

Equatorial Region

SAA

120.0

130.0

140.0

150.0

160.0

Figure

ORBIT: NAVELEX H
60 DGR/5186-5186 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

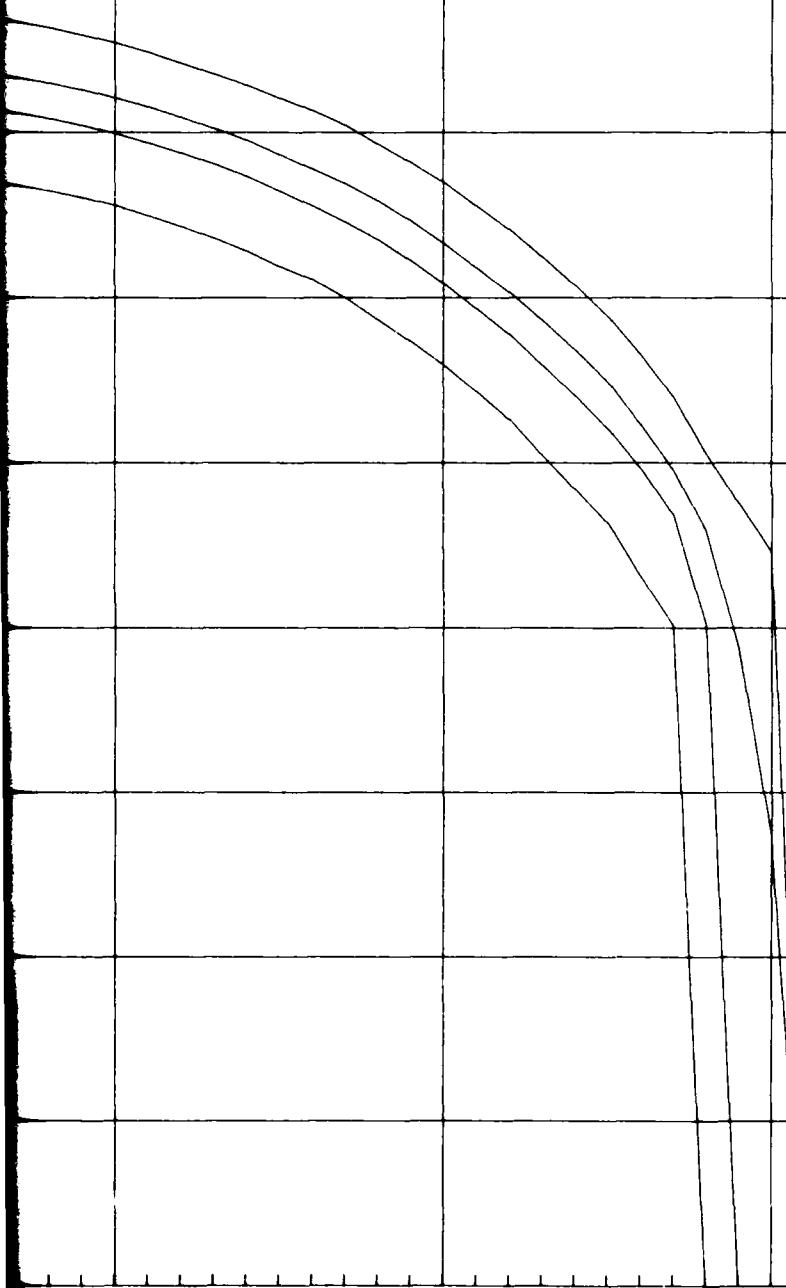
OUTER ZN ELEC: AE17 L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Region



STOP TIME ON TAPE = 7.716662

NASA-GSFC

160.0

170.0

180.0

190.0

200.0

Figure 144

ORBIT: NAVELEX 4
60 DGR/5186-5186 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-L0

MISSION DURATION: 60.00 M0

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

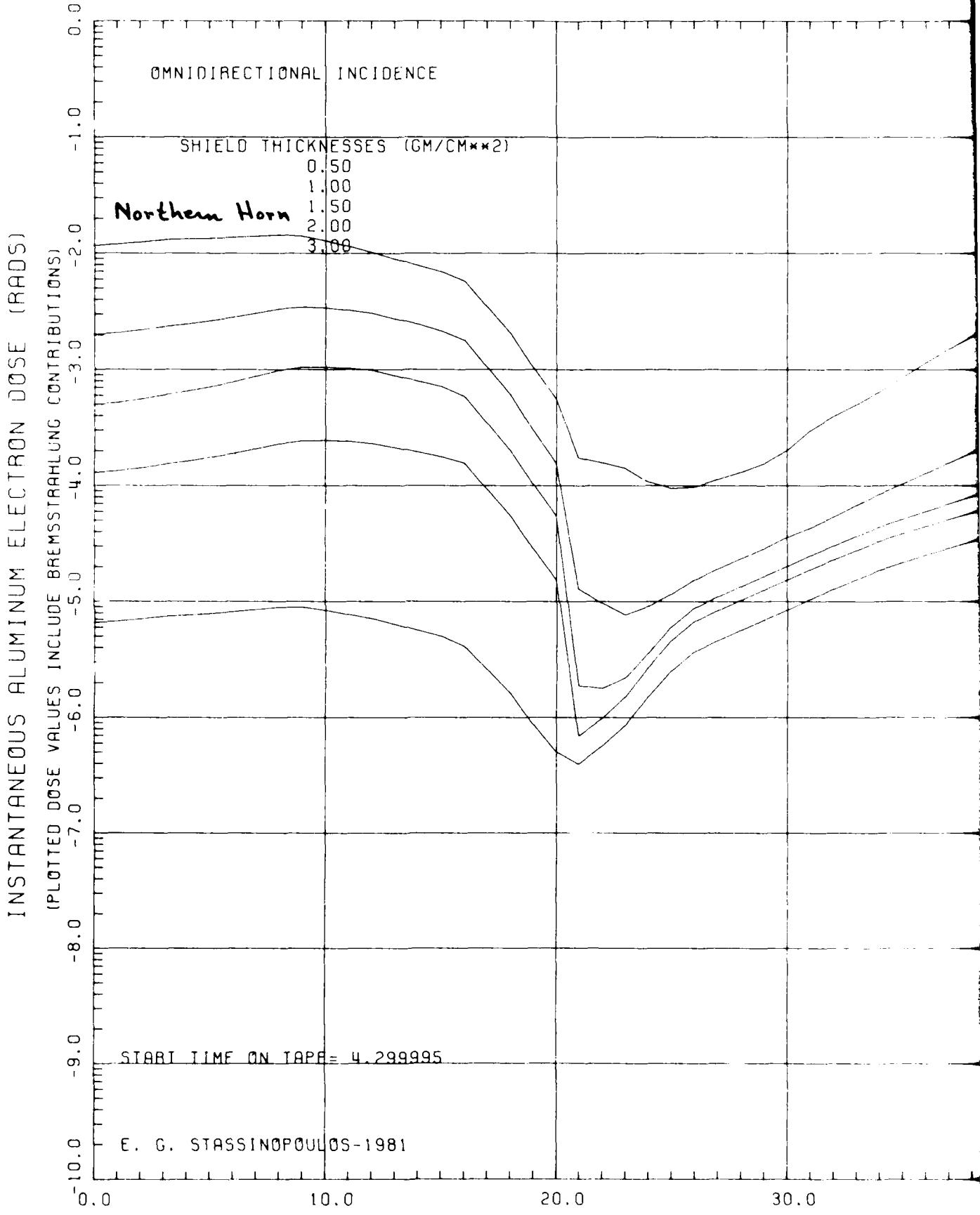
STOP TIME ON TAPE = 7.716662

NASA-GSFC

190.0

200.0

210.0



Equatorial Region

SAA

40.0

50.0

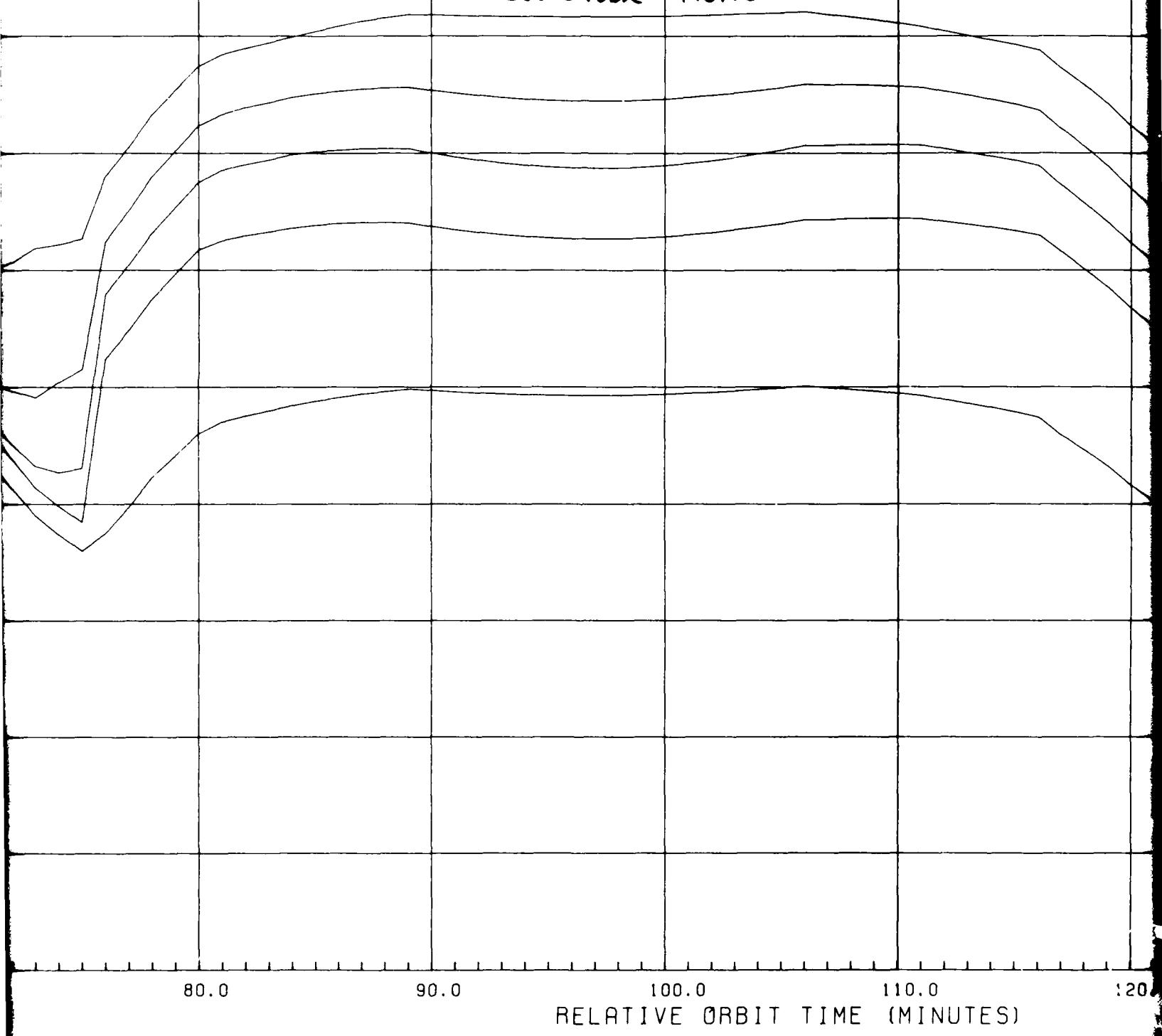
60.0

70.0

80

DOSE AT CENTER OF ALUMINUM SPHERES

Southern Horn



NUM SPHERES

4

Equatorial

SAA

120.0

130.0

140.0

150.0

MINUTES)

ORBIT: NA
60 DGR/

EPOCH: 19

MODELS:

FIELD: B

TRAPPED

INNER ZN

OUTER ZN

MISSION DU

EVALUATION

UN FACTORS

Equatorial Region

Northern Horn

SAA

STOP TIME

150.0

160.0

170.0

180.0

190.0

Figure 145

ORBIT: NAVELEX 4
60 DGR/5186-5186 KM

EPOCH: 1989.5

Northern Horn

MODELS:
FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AE17-L0
MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX
UN FACTORS: NOT APPLIED

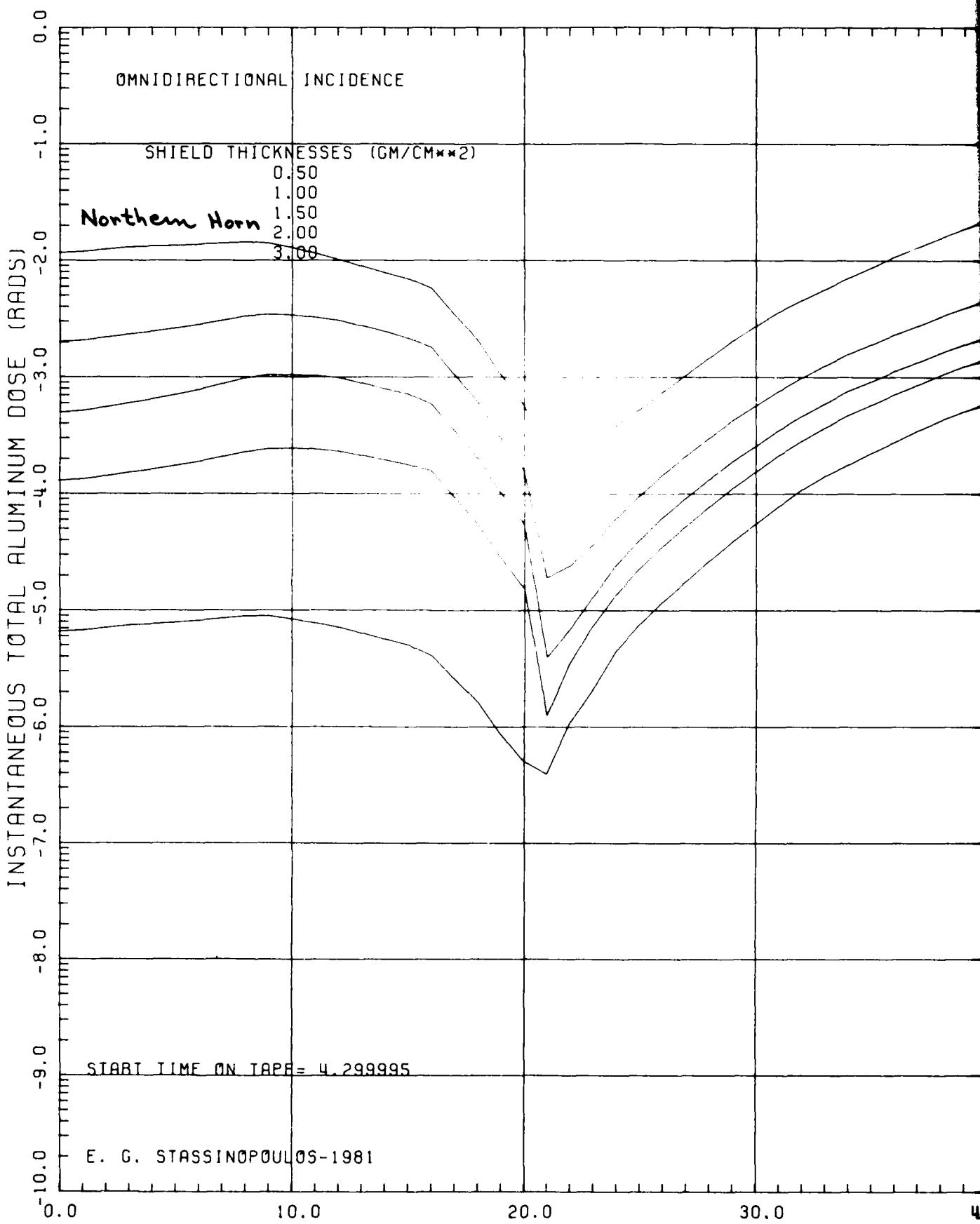
STOP TIME ON TAPE = 7.716662

NASA-GSFC

190.0

200.0

210.0



Equatorial Region

SAA

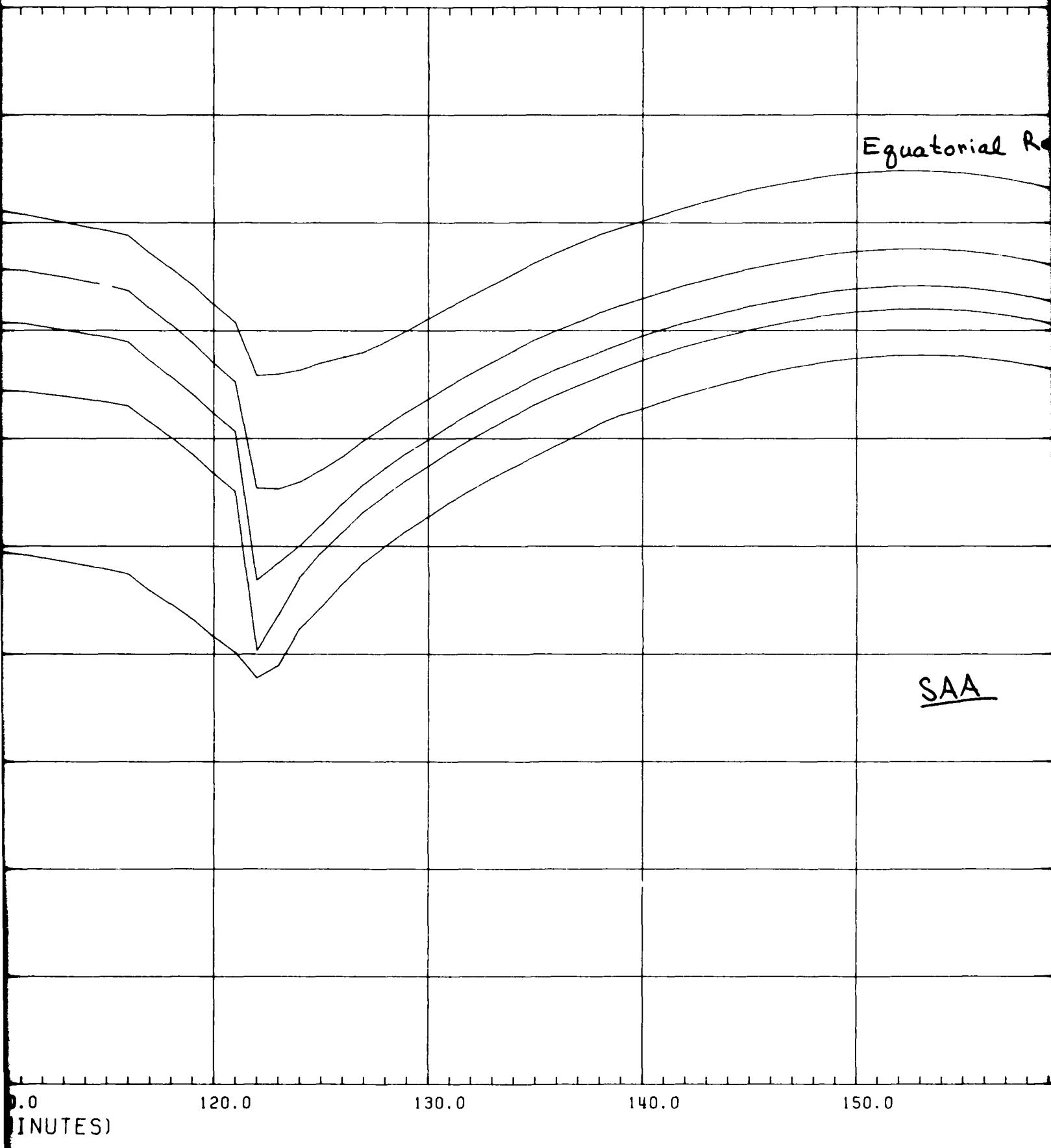
0 40.0 50.0 60.0 70.0

DOSE AT CENTER OF ALUMINUM SPHERES

Southern Horn

80.0 90.0 100.0 110.0
RELATIVE ORBIT TIME (MINUTES)

INUM SPHERES



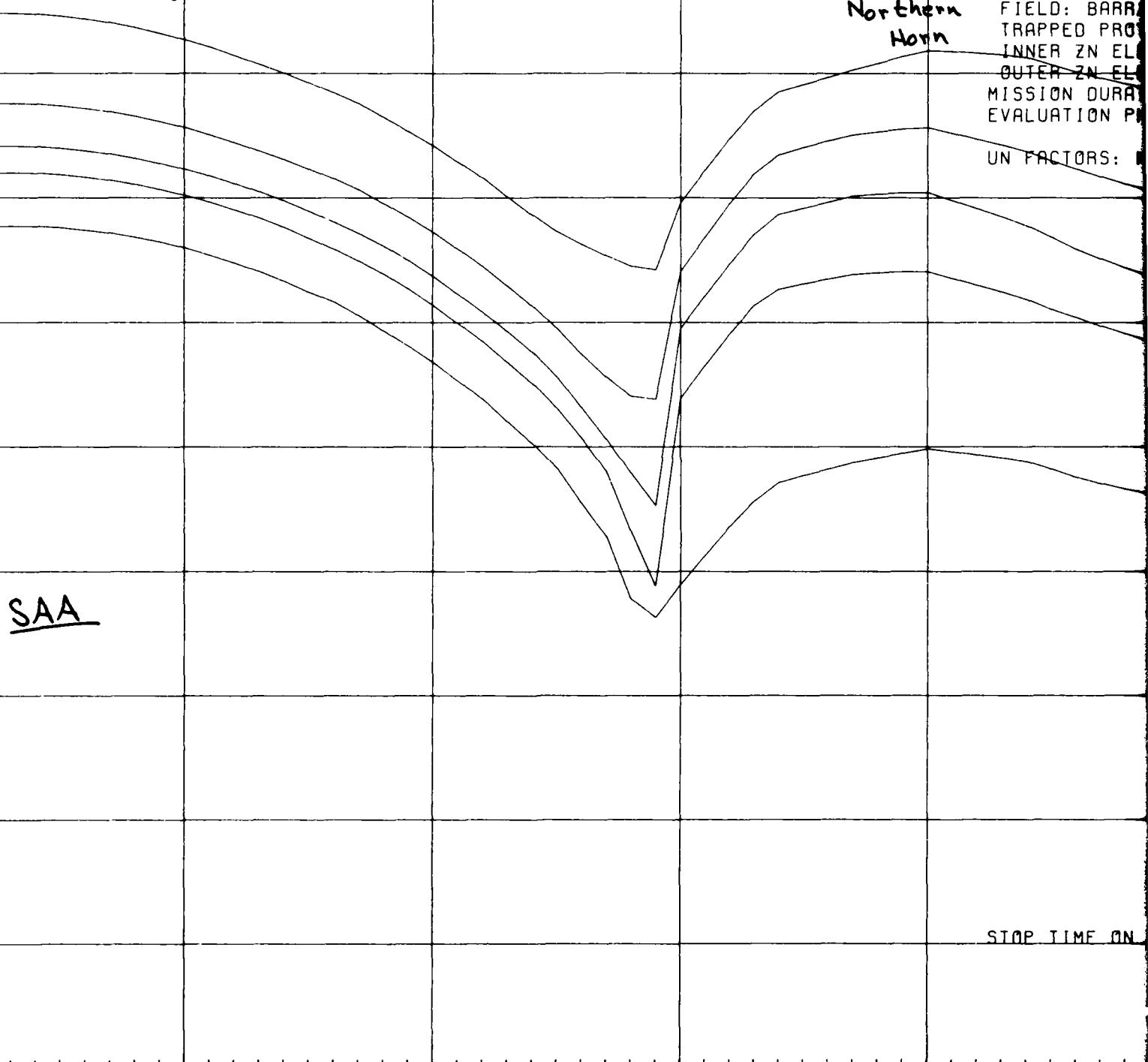
ORBIT: NAVEL
60 DGR/518

EPOCH: 1989.

MODELS:
FIELD: BARR
TRAPPED PRO
INNER ZN EL
OUTER ZN EL
MISSION DURAT
EVALUATION P

UN FACTORS:

Northern
Horn



Equatorial Region

SAA

STOP TIME ON

0.0

160.0

170.0

180.0

190.0

Figure 146

ORBIT: NAVELEX 4
60 DGR/5186-5186 KM

EPOCH: 1989.5

Northern
Horn

MODELS:
FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AE17 L0
MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

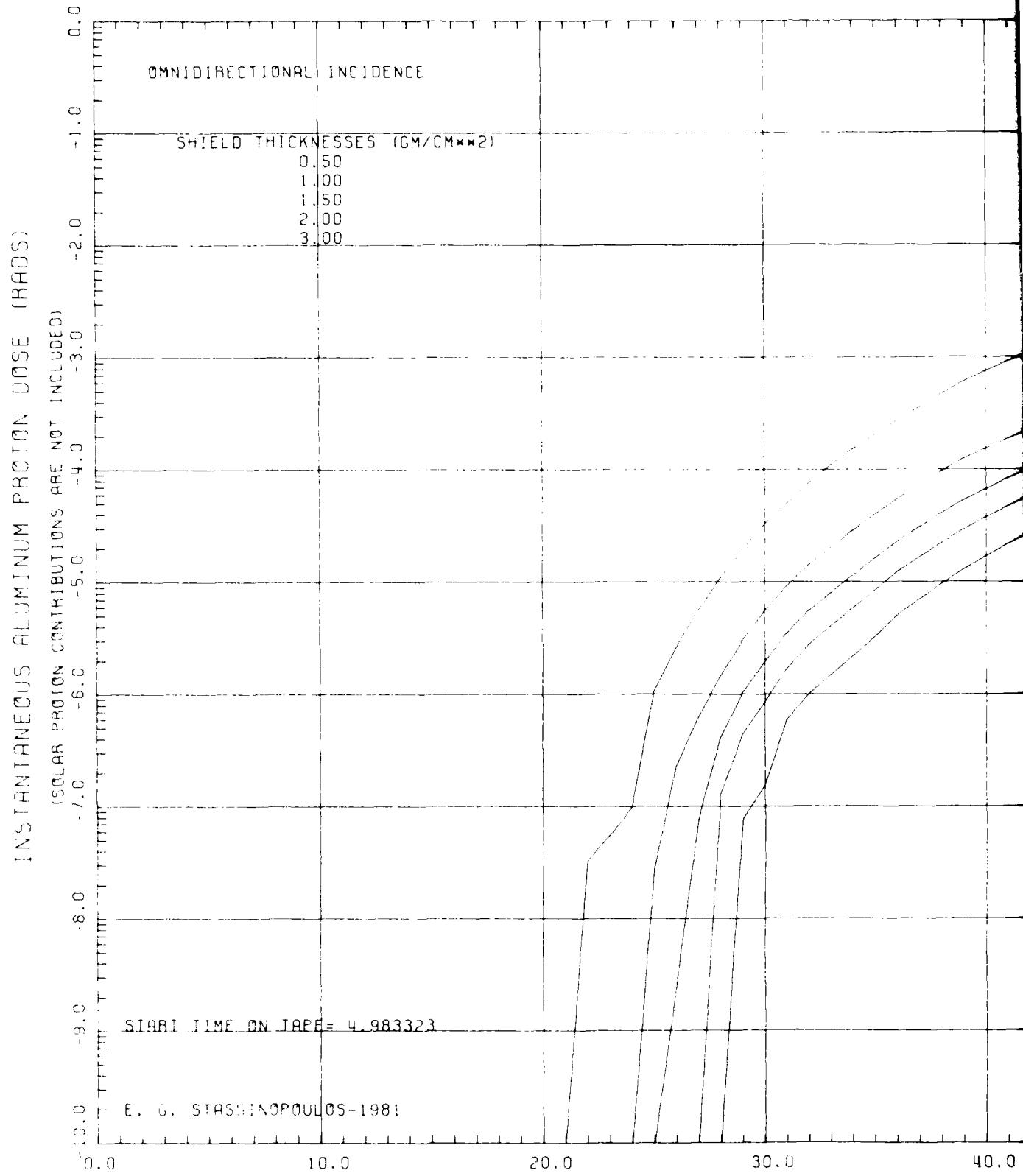
STOP TIME ON TAPE = 7.716662

NASA-GSFC

190.0

200.0

210.0



Equatorial Region

SAA

40.0

50.0

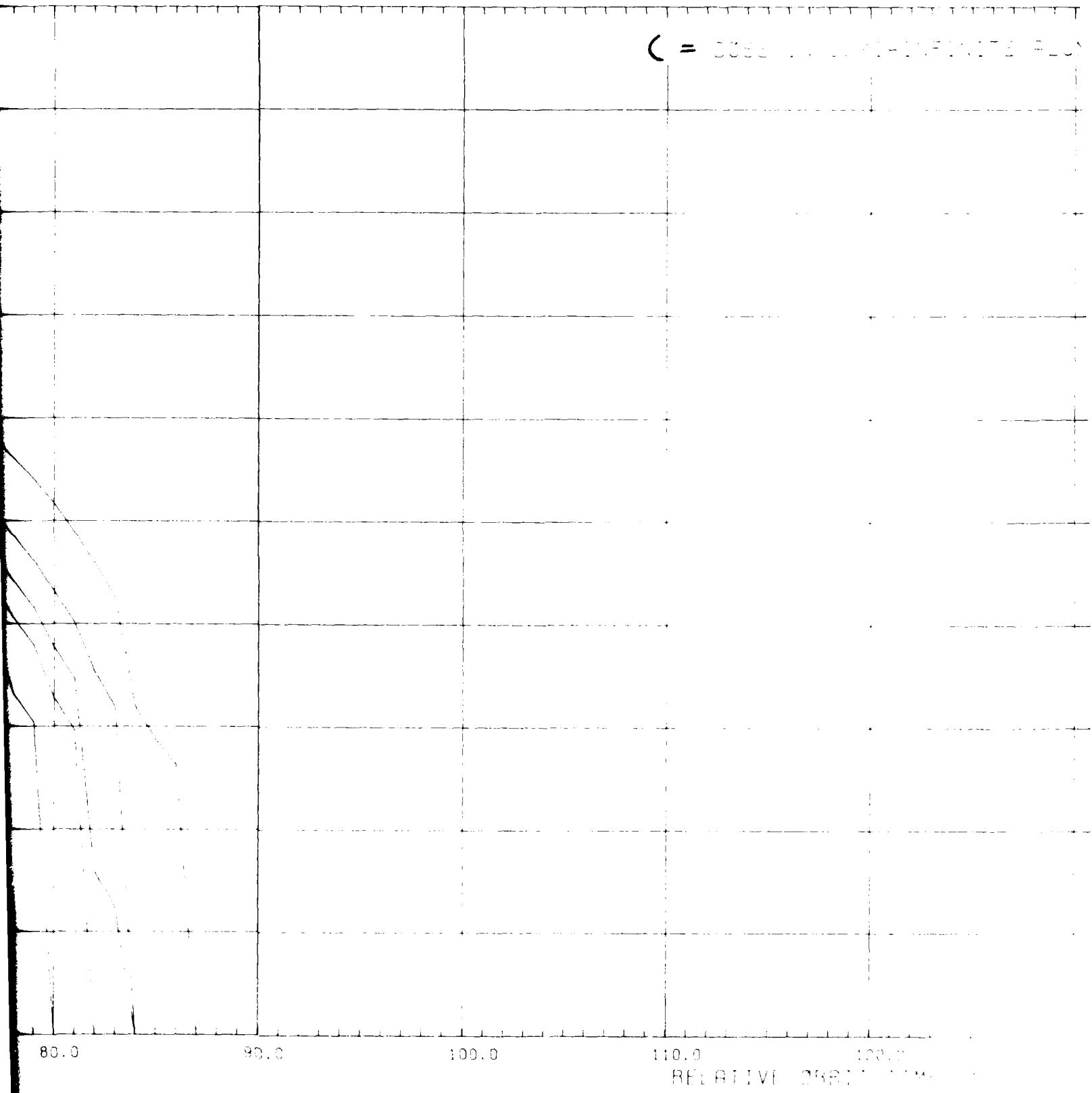
60.0

70.0

80.0

DOSE AT TRANSMISSION SURFACE OF FINITE AL

C = DOSE AT TRANSMISSION SURFACE OF FINITE AL



AD-A141 849 ORBITAL RADIATION STUDY FOR INCLINED CIRCULAR
TRAJECTORIES(U) NATIONAL AERONAUTICS AND SPACE
ADMINISTRATION GREENBELT MD GO.. E G STASSINOPoulos
NOV 81 NASA-GSFC-X-601-81-28

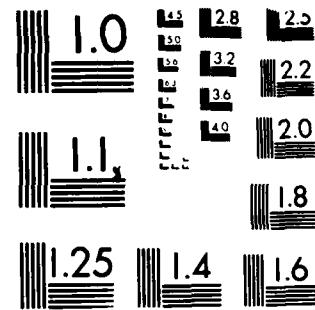
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F/G 22/3

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5/5

END
DATE 7-84
DHC



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS 1963 A

4

FINITE ALUMINUM SLAB SHIELDS

FINITE ALUMINUM MEDIUM)

Equator

SAA

130.0

140.0

150.0

160.0

170.0

(MINUTES)

5

Equatorial Region

SAA

170.0

180.0

190.0

200.0

210.0

6

Figure 147

ORBIT: NAVELEX 5
60 OGR/6389-6389 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AE17 L0
MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

STOP TIME ON TAPE = 8.933318

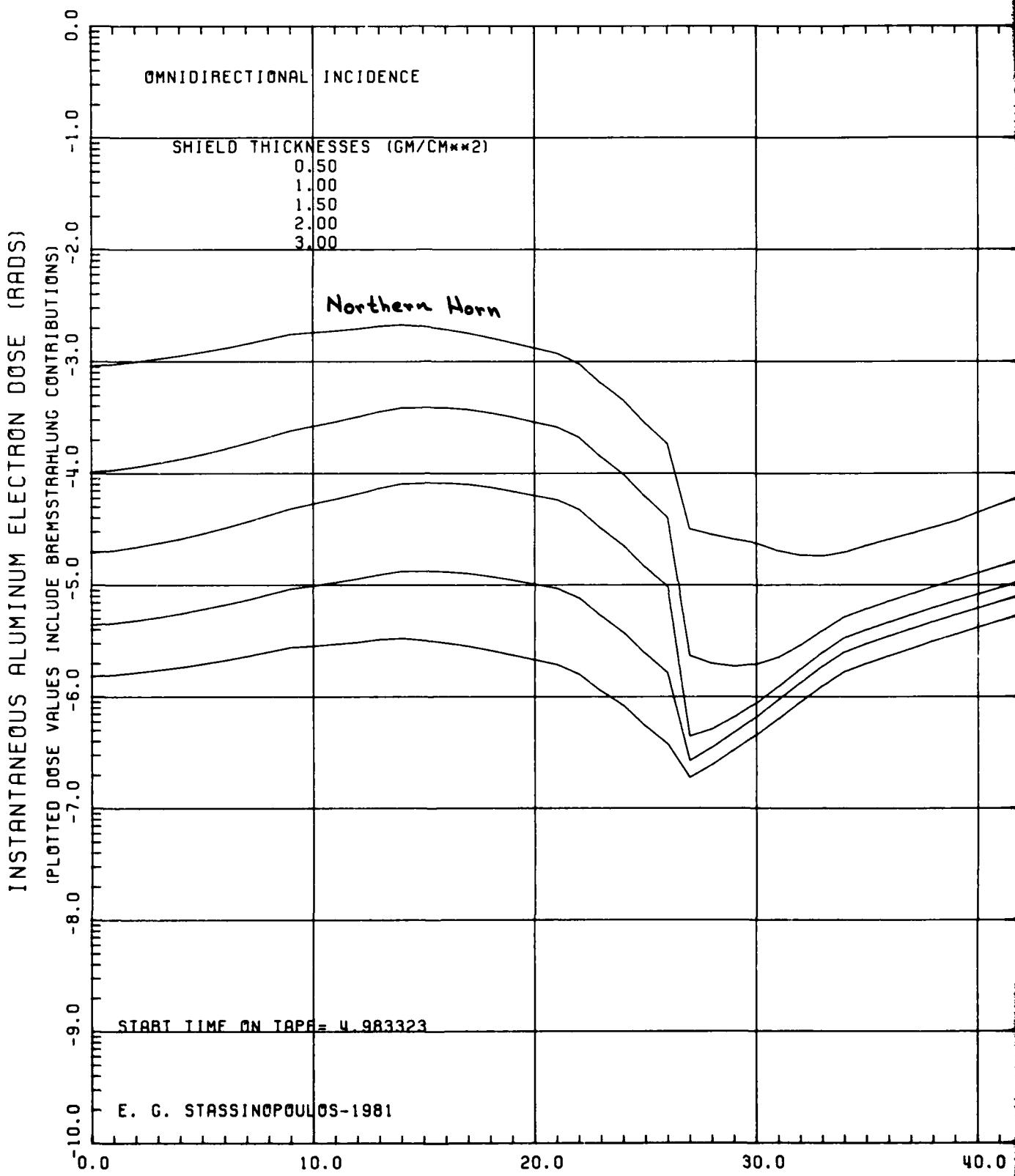
NASA-GSFC

210.0

220.0

230.0

240.0



'2

Equatorial Region

SAA

40.0

50.0

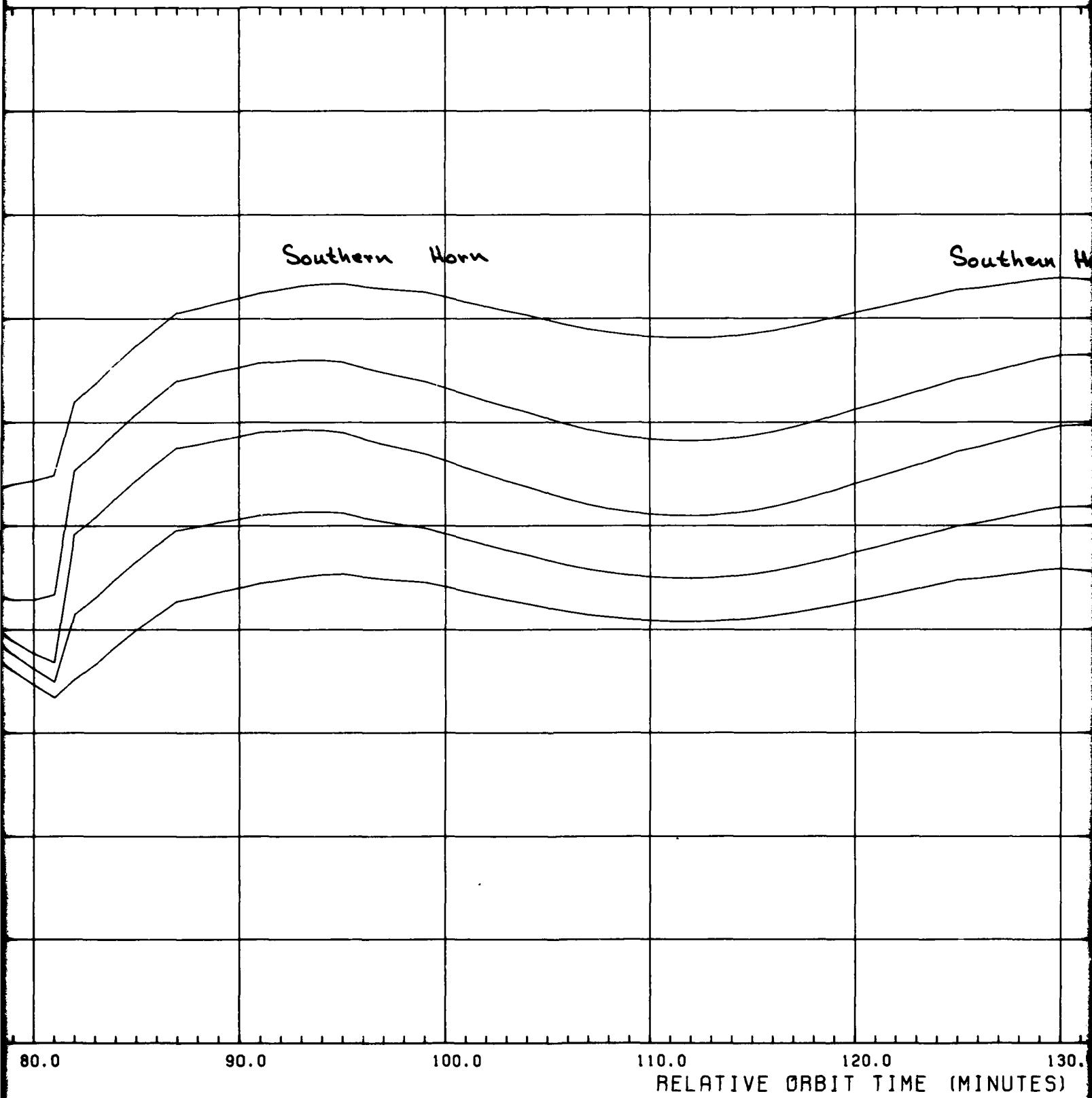
60.0

70.0

80.0

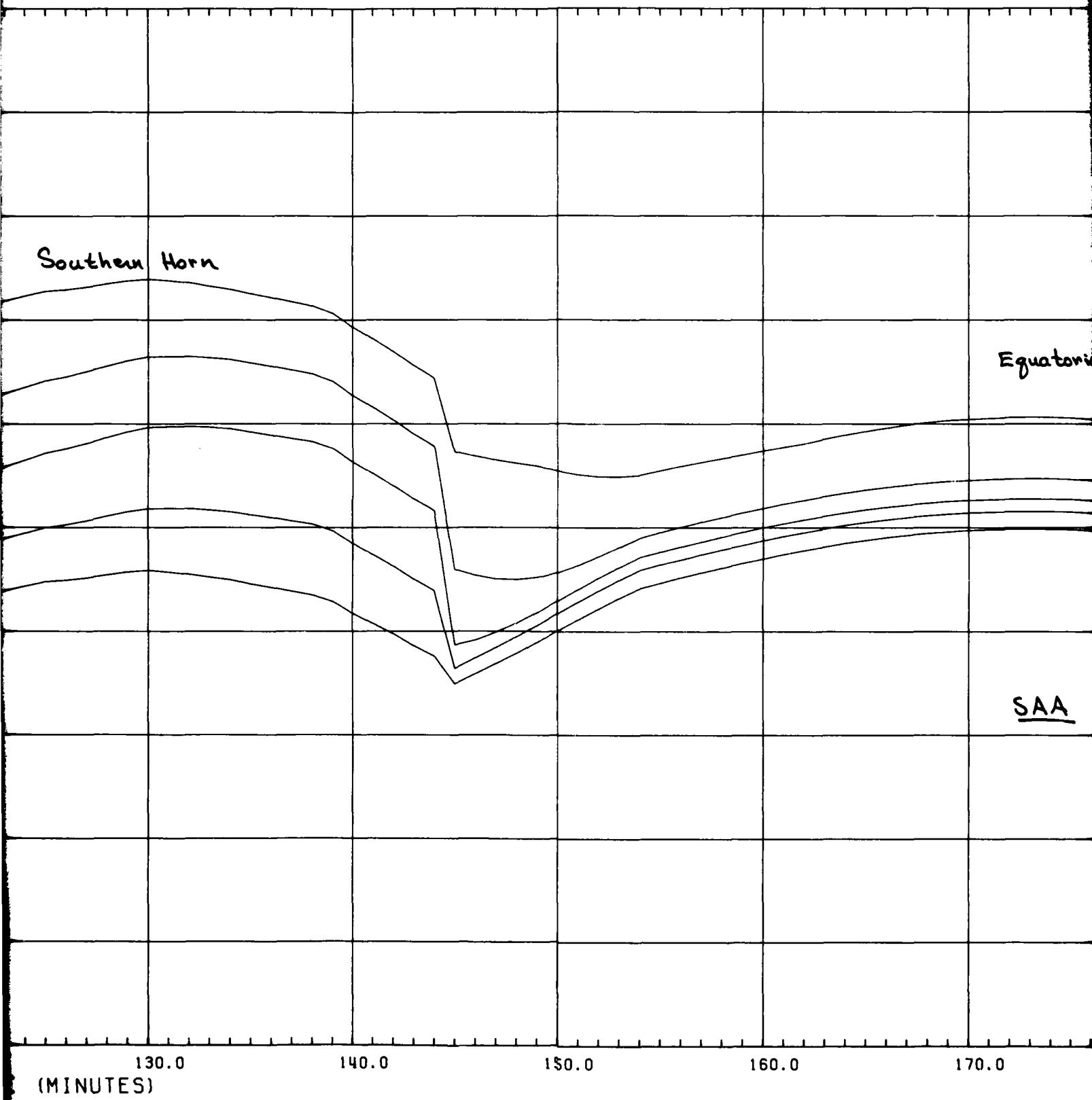
3

DOSE AT TRANSMISSION SURFACE OF FINITE ALU



'4

FINITE ALUMINUM SLAB SHIELDS



15

Equatorial Region

Northern Hemisphere

SAA

170.0

180.0

190.0

200.0

210.0

2

D-3

6

Figure 148

ORBIT: NAVELEX 5
60 DGR/6389-6389 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AE17-L0
MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern Horn

STOP TIME ON TAPF = 8.933318

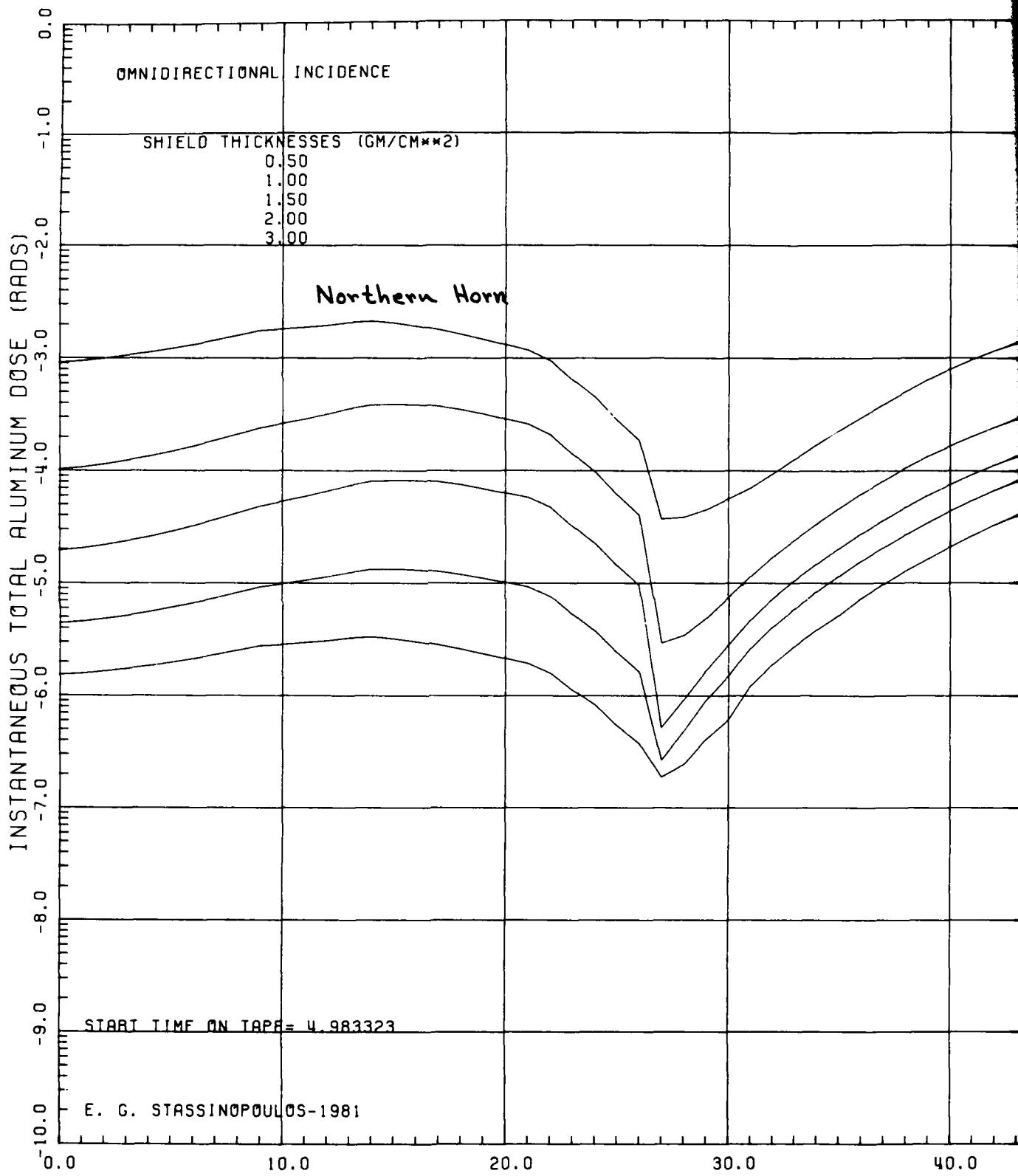
NASA-GSFC

210.0

220.0

230.0

240.0



2

Equatorial Region

SAA

40.0

50.0

60.0

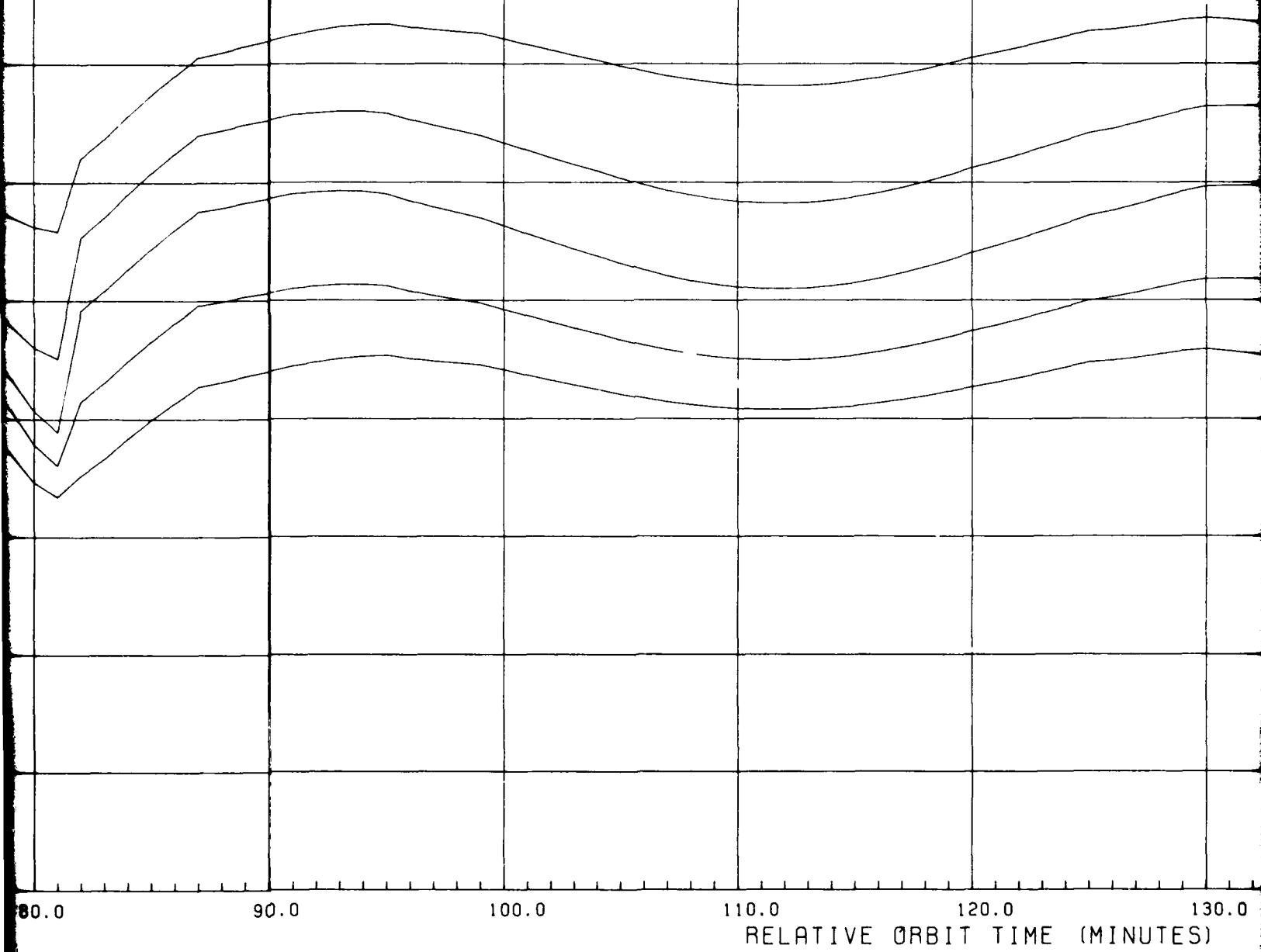
70.0

80.0

3
DOSE AT TRANSMISSION SURFACE OF FINITE ALUM

Southern Horn

Southern



'4

F FINITE ALUMINUM SLAB SHIELDS

Southern Horn

Equat

SAA

130.0

140.0

150.0

160.0

170.0

E (MINUTES)

5

Equatorial Region

Northern Horn

SAA

170.0

180.0

190.0

200.0

210.0

Figure 149

ORBIT: NAVELEX 5
60 DGR/6389-6389 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AEG

OUTER ZN ELEC: AEI7-L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern Horn

STOP TIME ON TAPE = 8.933318

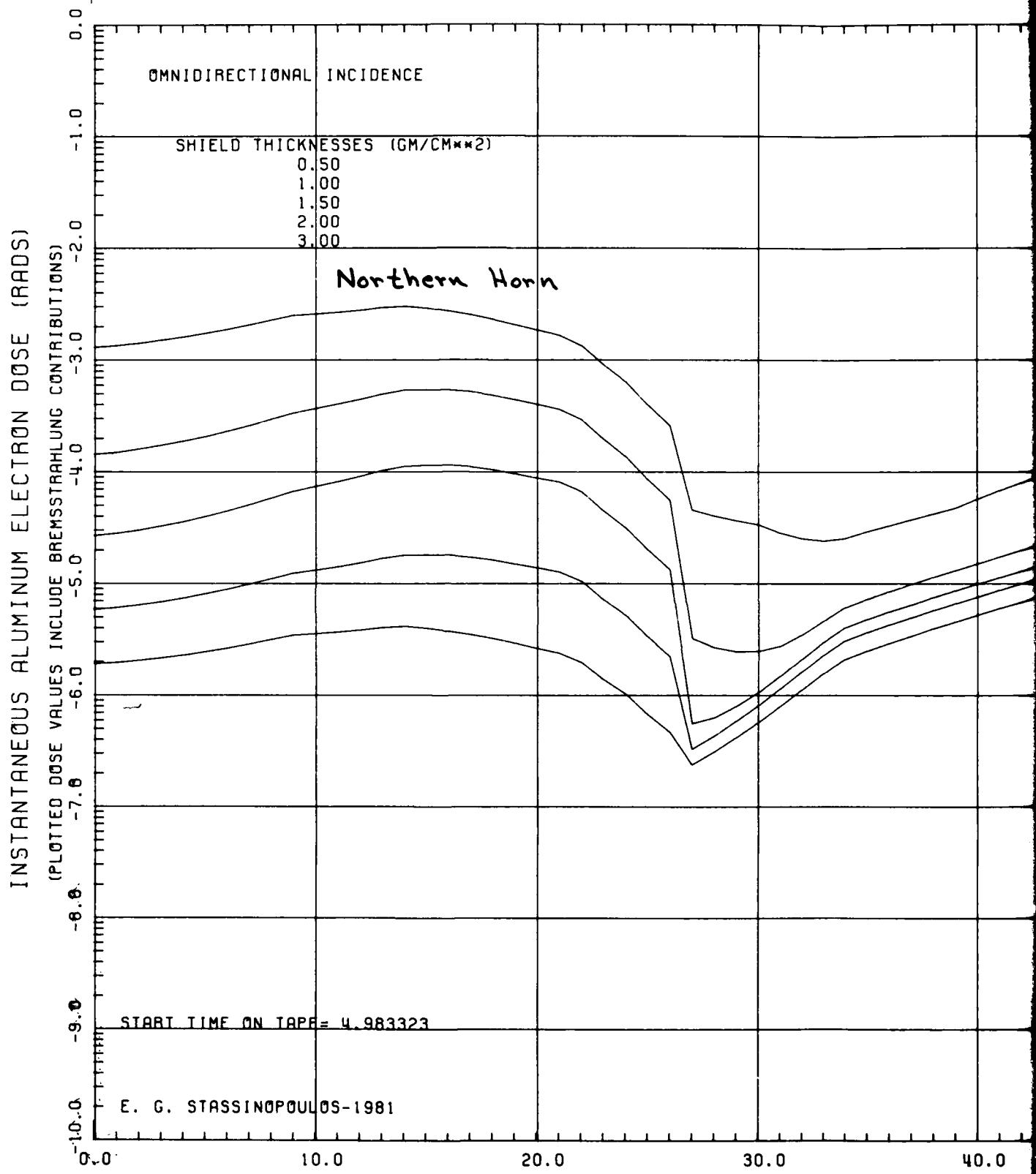
NASA-GSFC

210.0

220.0

230.0

240.0



2

Equatorial Region

SAA

40.0

50.0

60.0

70.0

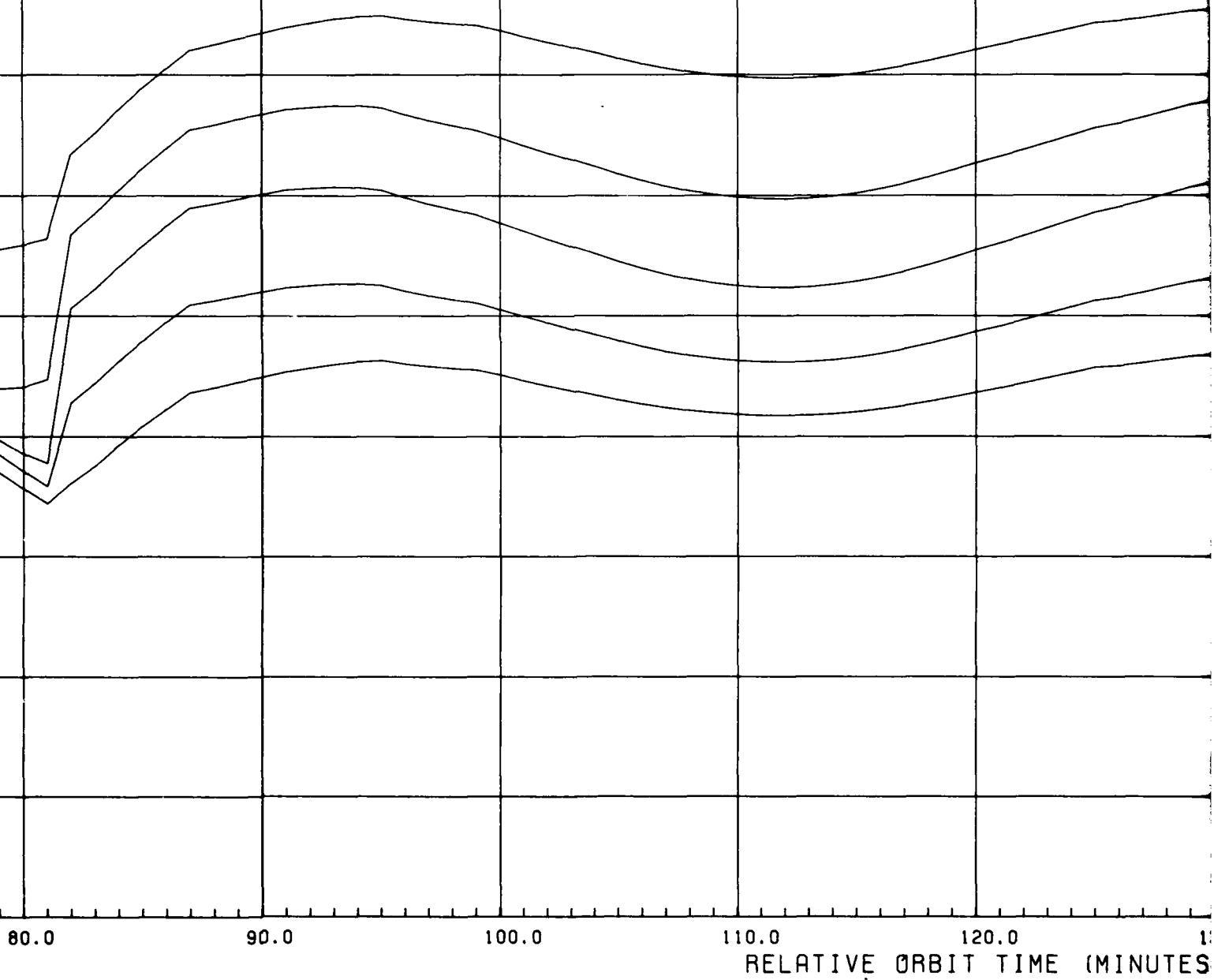
80.0

3

DOSE IN SEMI-INFINITE ALUMINUM

Southern Horn

Sout



4

ITE ALUMINUM MEDIUM

Southern Horn

Equator

SA

130.0

140.0

150.0

160.0

170.0

ME (MINUTES)

5

Equatorial Region

Northern

SAA

170.0

180.0

190.0

200.0

210.0

6

Figure 150

ORBIT: NAVELEX 5
60 DGR/6389-6389 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AE17 LO
MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern Horn

STOP TIME ON TAPE = 8.933318

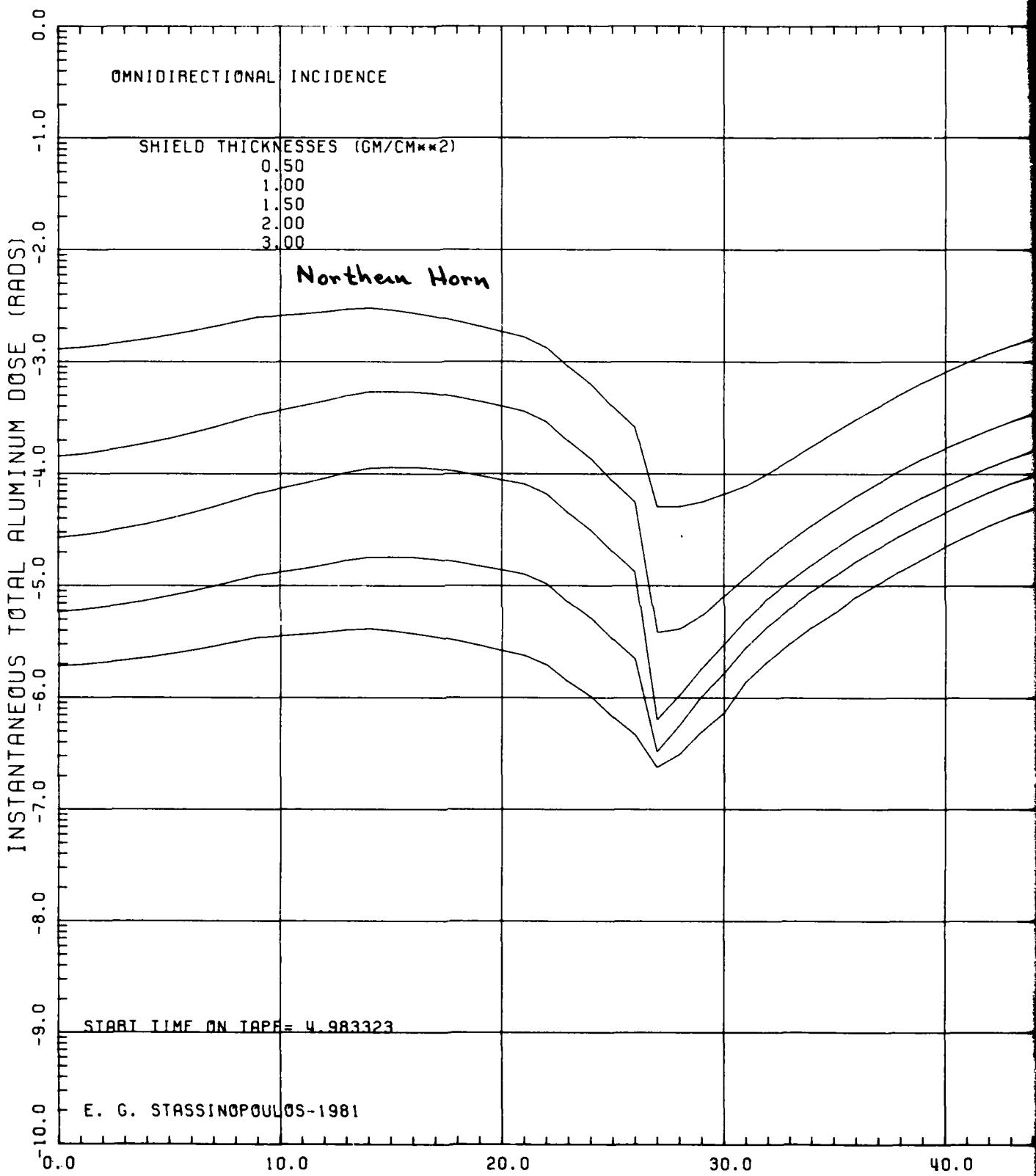
NASA-GSFC

210.0

220.0

230.0

240.0



2'

Equatorial Region

SAA

40.0

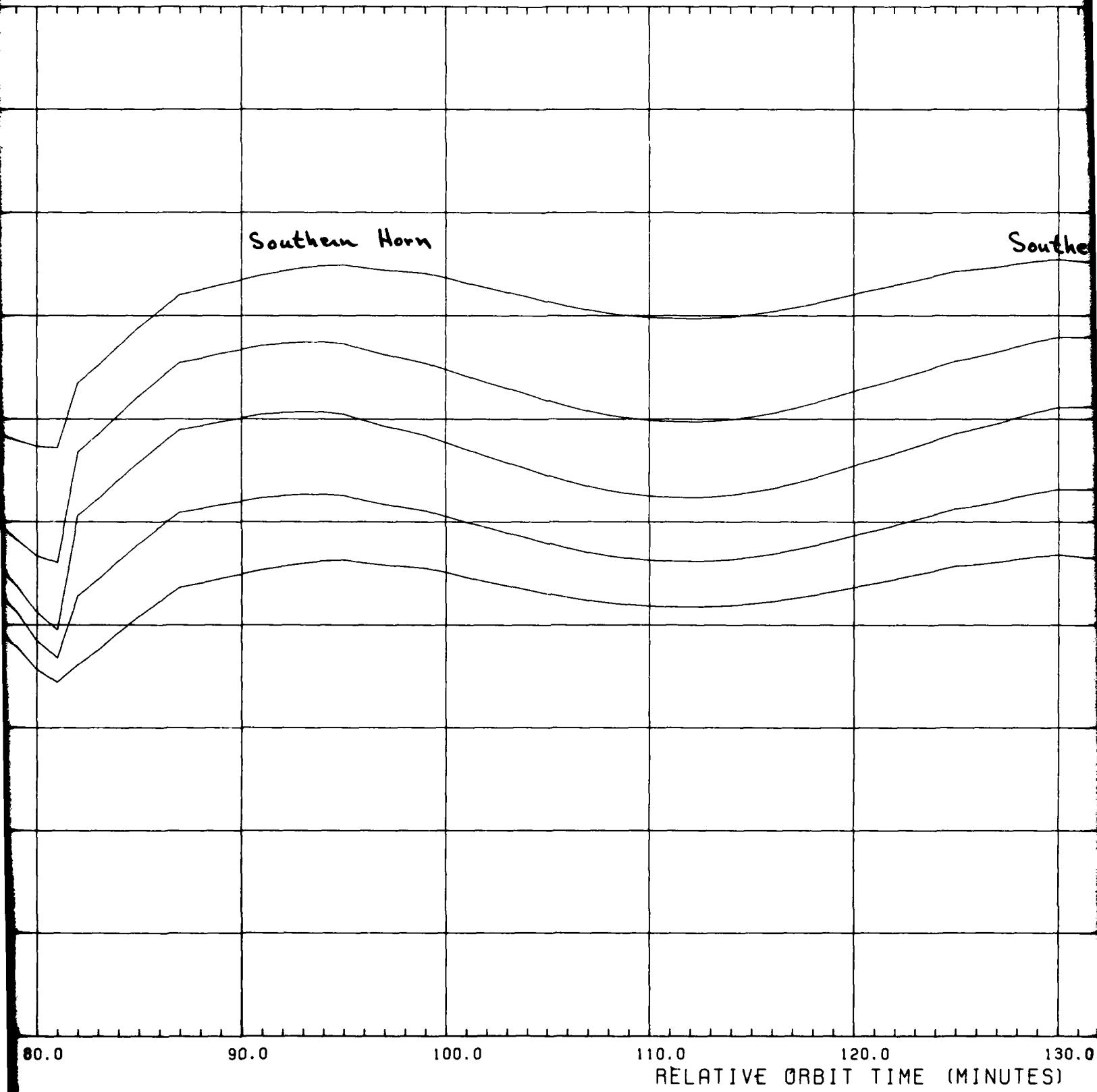
50.0

60.0

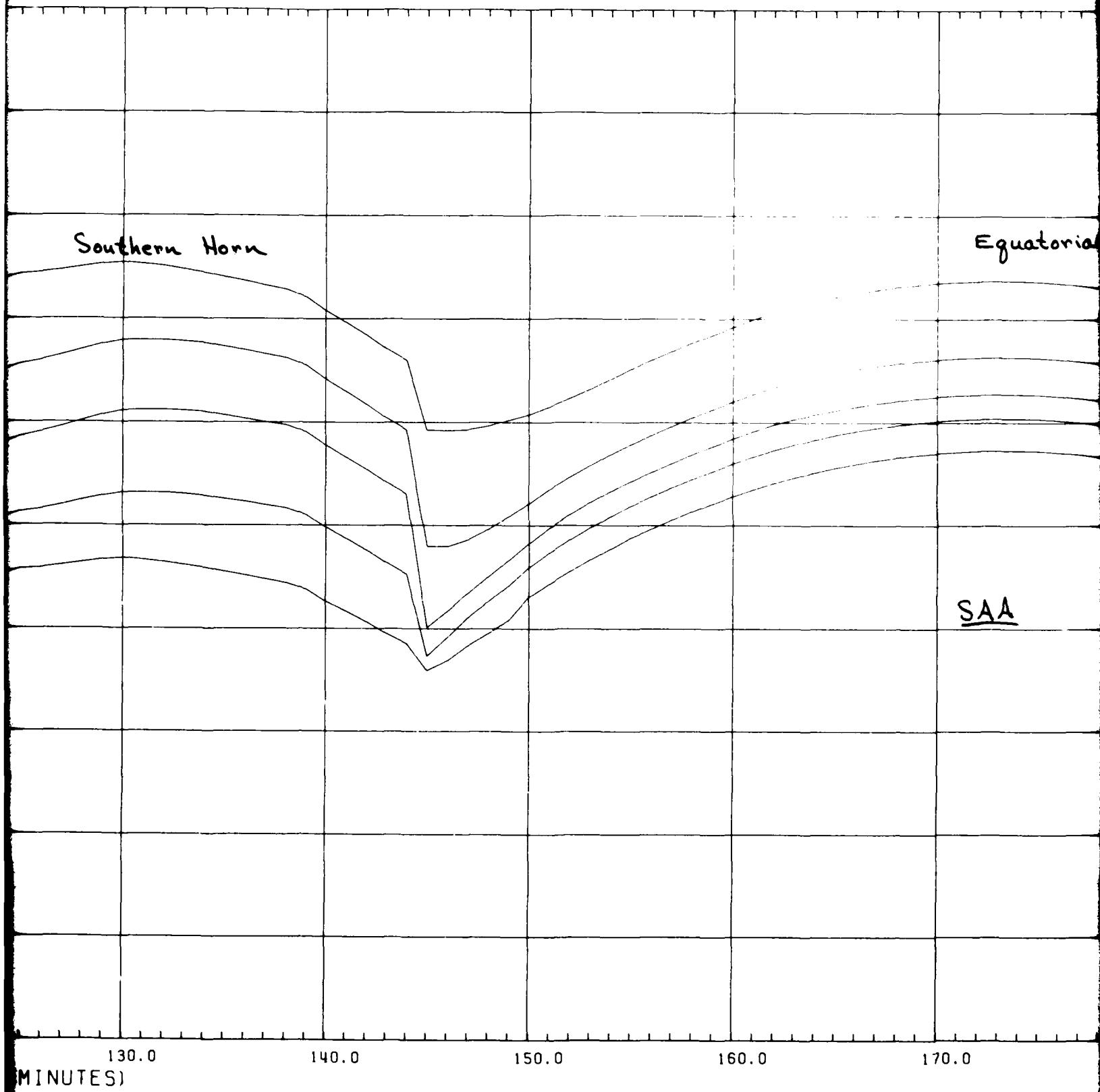
70.0

80.0

DOSE IN SEMI-INFINITE ALUMINUM M



ALUMINUM MEDIUM



Equatorial Region

Northern Horn

SAA

170.0

180.0

190.0

200.0

210.0

220.0

Figure 151

ORBIT: NAVELEX 5
60 DGR/6389-6389 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 LO

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

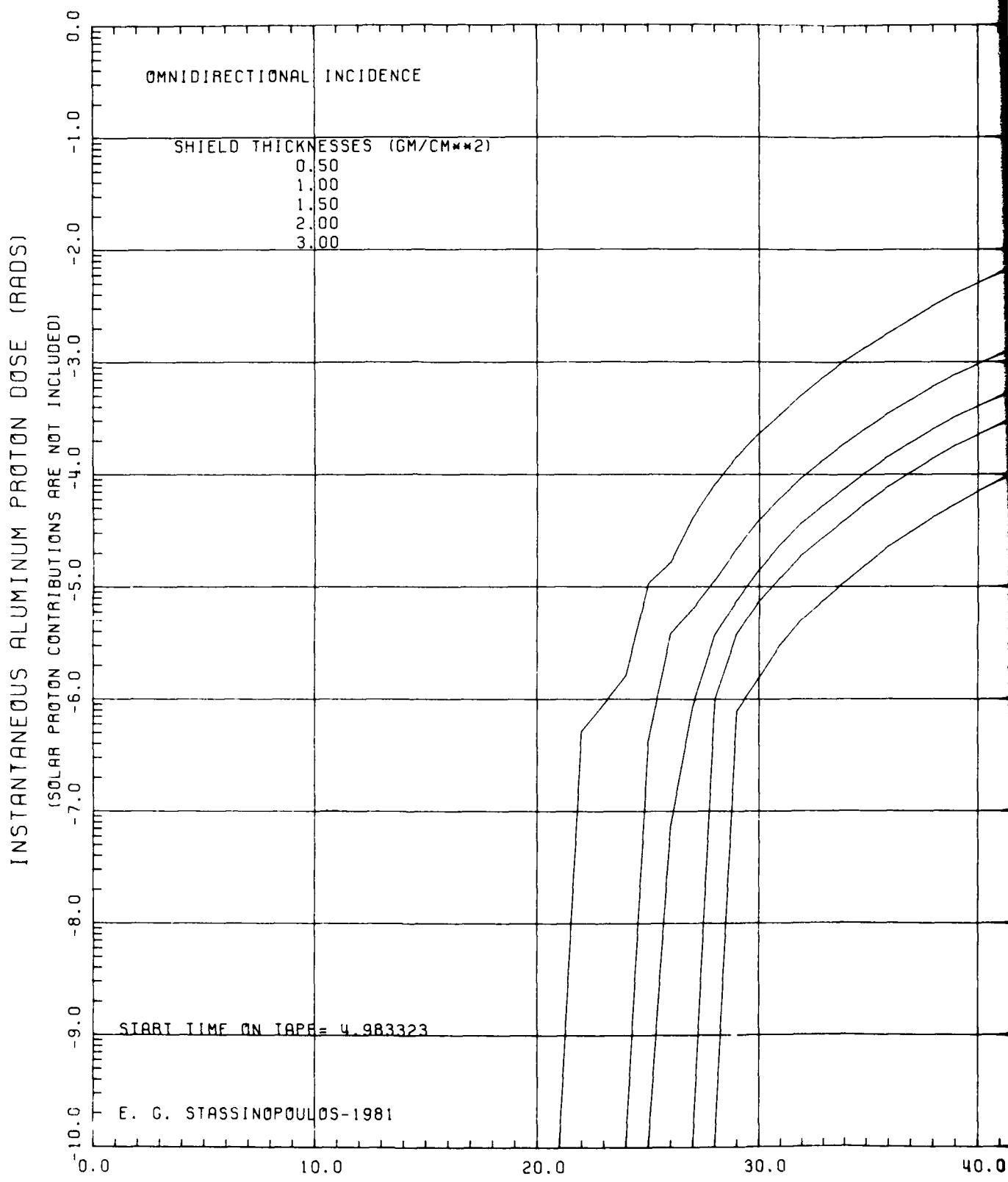
UN FACTORS: NOT APPLIED

Northern Horn

STOP TIME ON TAPF = 8.933318

NASA-GSFC

210.0 220.0 230.0 240.0



1
2

Equatorial Region

SAA

40.0

50.0

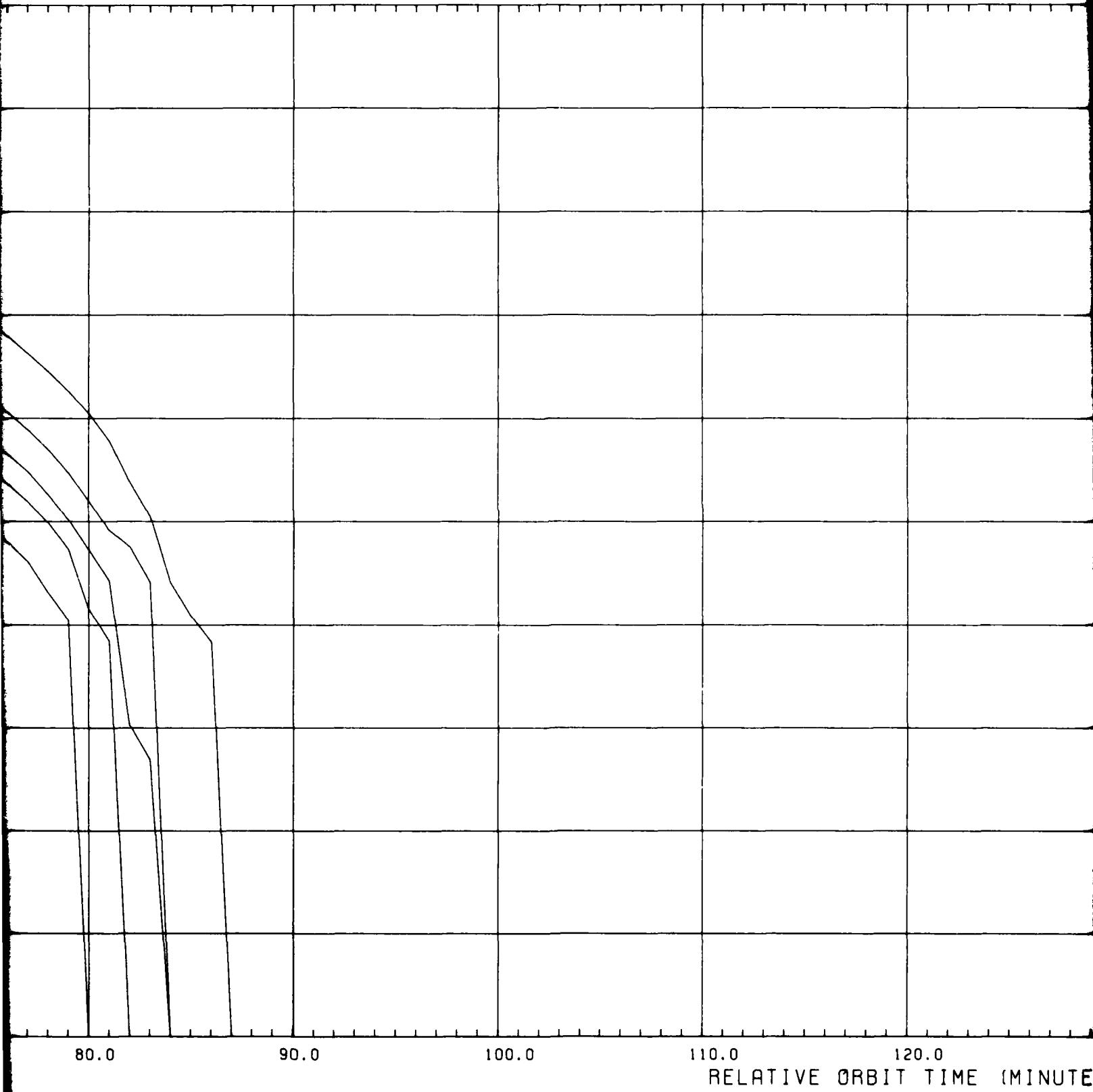
60.0

70.0

80.0

3

DOSE AT CENTER OF ALUMINUM



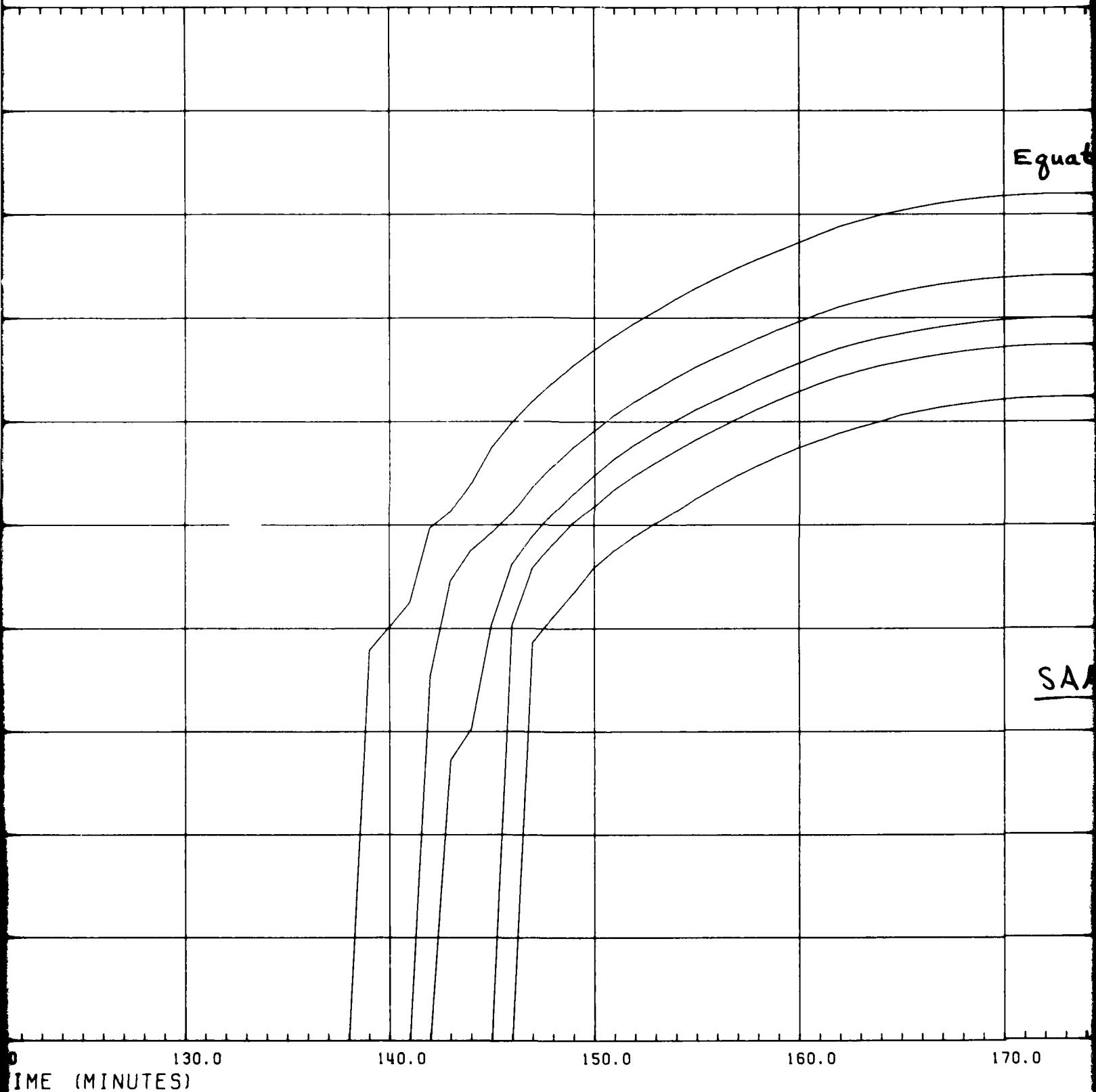
RELATIVE ORBIT TIME (MINUTE)

4

ALUMINUM SPHERES

Equat

SAA



TIME (MINUTES)

5

Equatorial Region

SAA

170.0

180.0

190.0

200.0

210.0

6

Figure 152

ORBIT: NAVELEX 5
60 OGR/6389-6389 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
~~OUTER ZN ELEC: AE17 L0~~
MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

STOP TIME ON TAPF = 8.933318

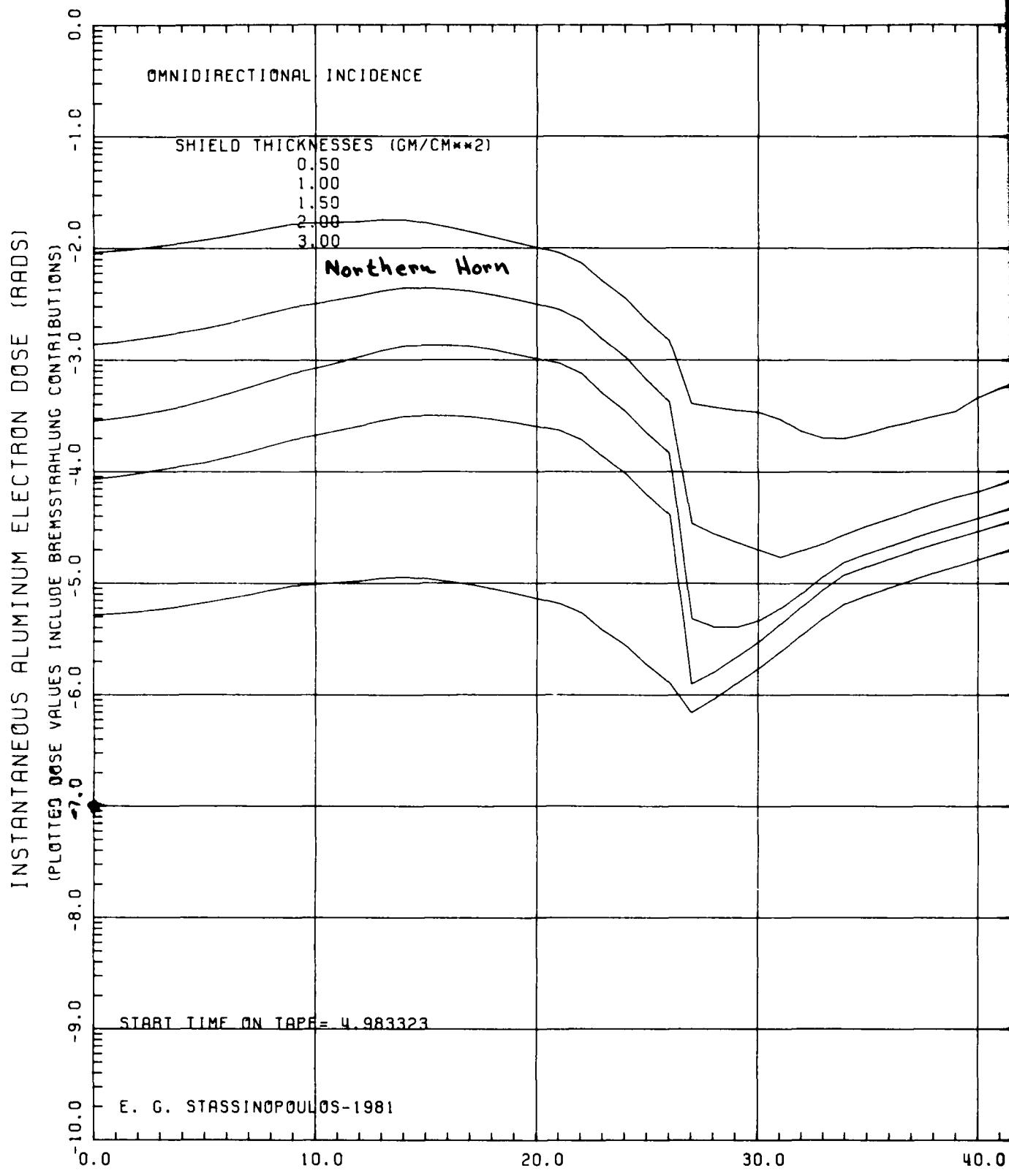
NASA-GSFC

210.0

220.0

230.0

240.0



2

Equatorial Region

SAA

40.0

50.0

60.0

70.0

80.0

3 1
DOSE AT CENTER OF ALUMINUM

Southern Horn

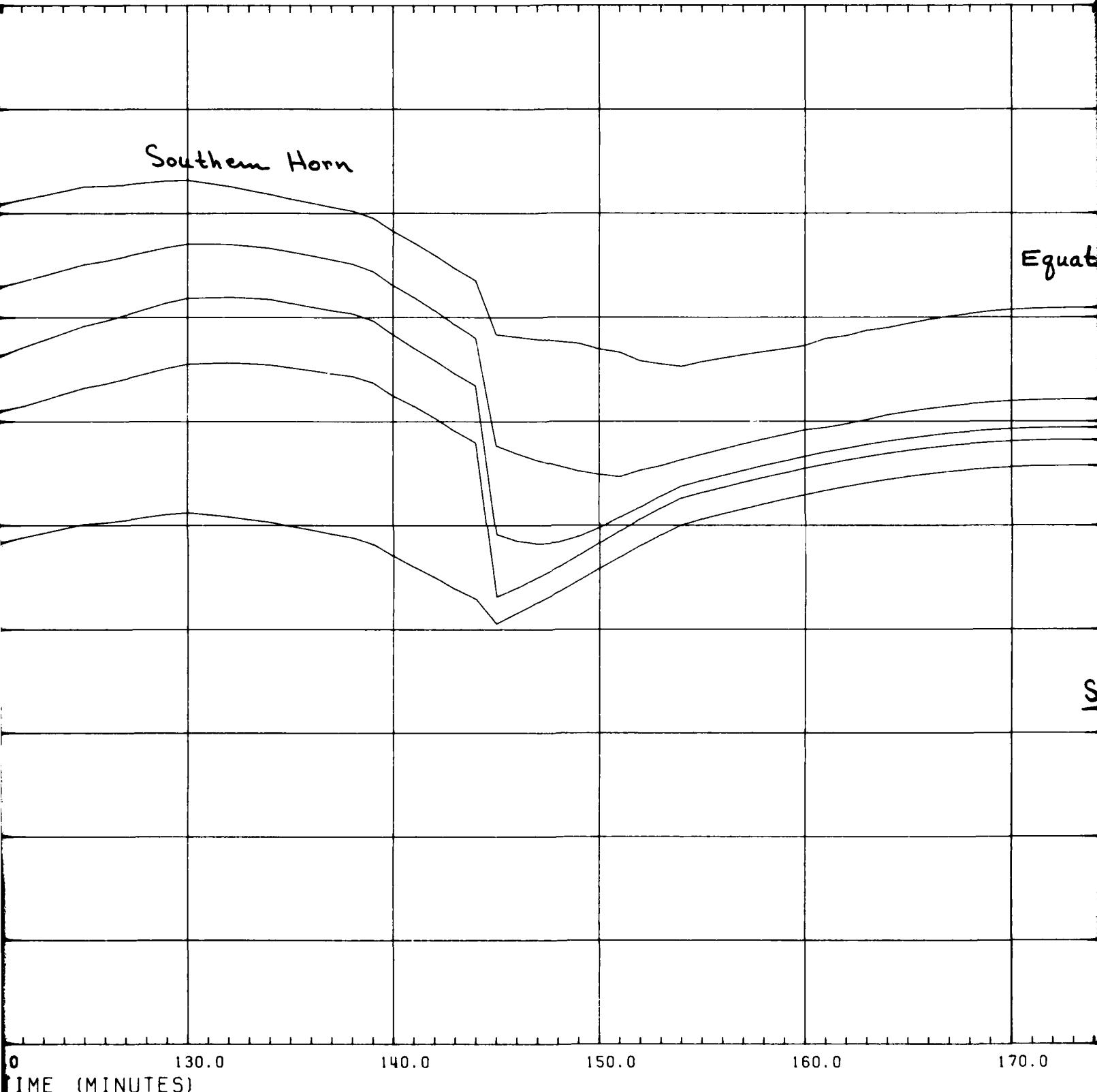
80.0 90.0 100.0 110.0 120.0
RELATIVE ORBIT TIME (MINUT)

'4

F ALUMINUM SPHERES

Southern Horn

Equat



5
North

Equatorial Region

SAA

170.0 180.0 190.0 200.0 210.0

6

Figure 153

ORBIT: NAVELEX 5
60 DGR/6389-6389 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AE17-L0
MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern Horn

STOP TIME ON TAPF = 8.933318

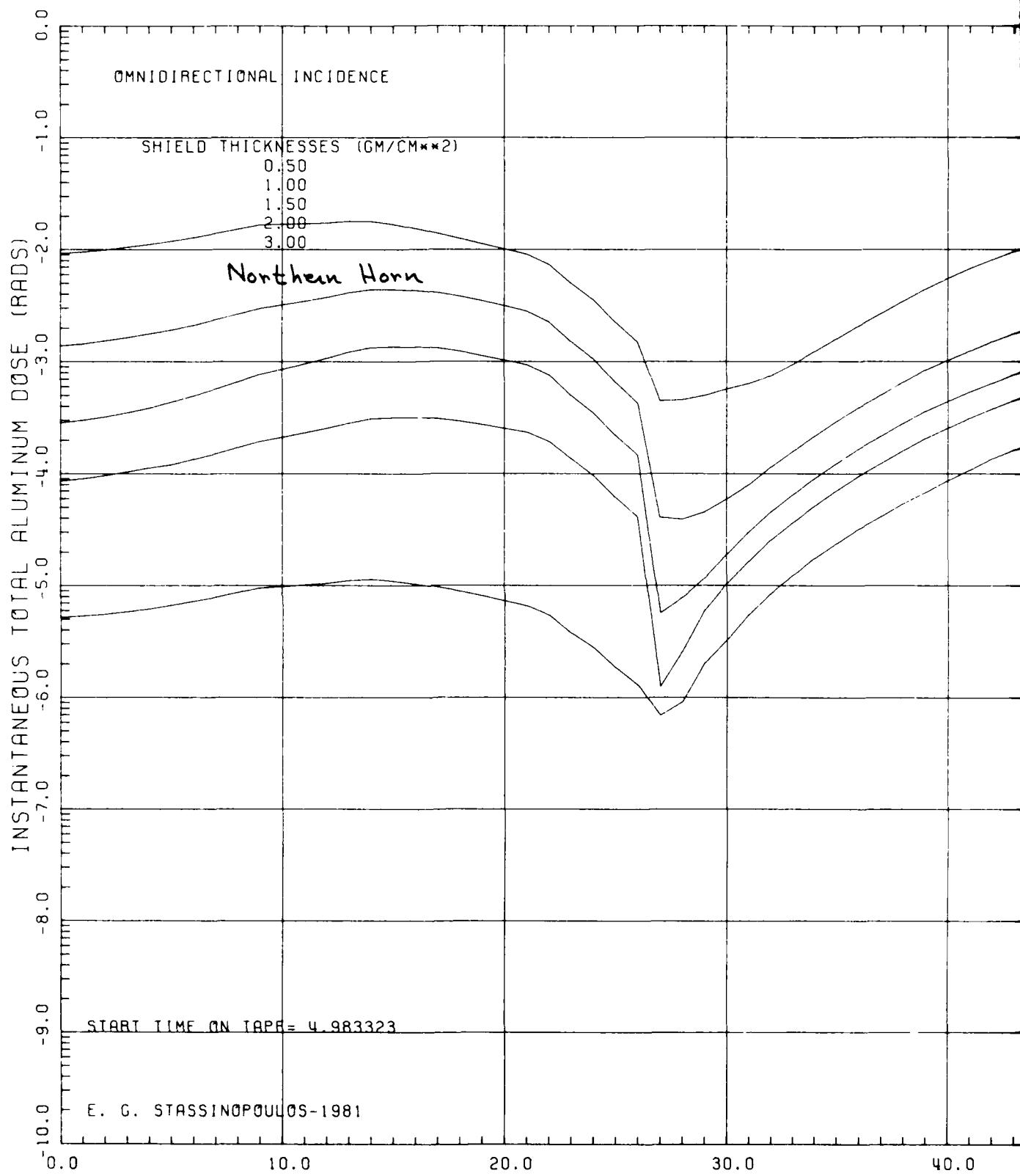
NASA-GSFC

210.0

220.0

230.0

240.0

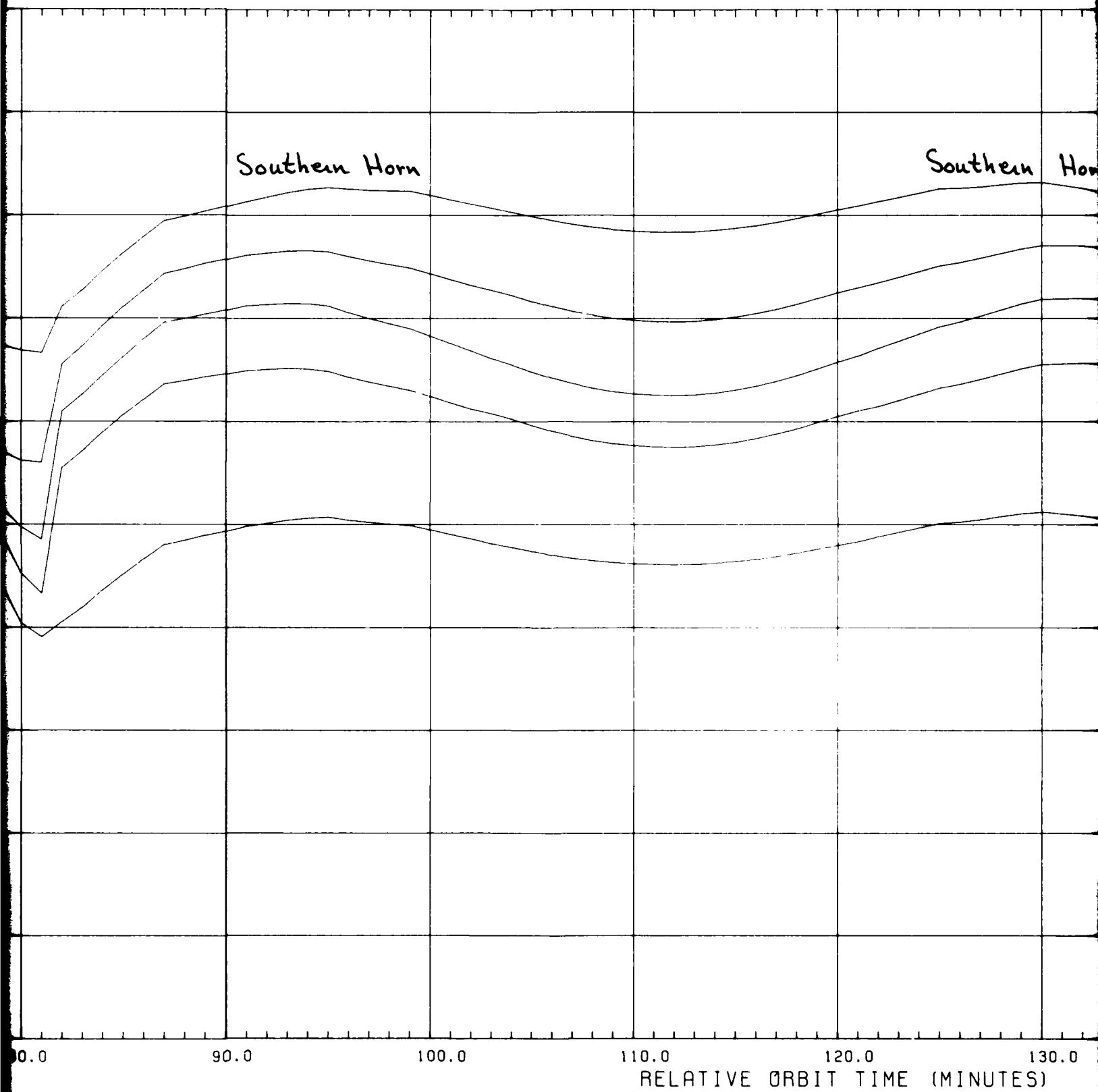


Equatorial Region

SAA

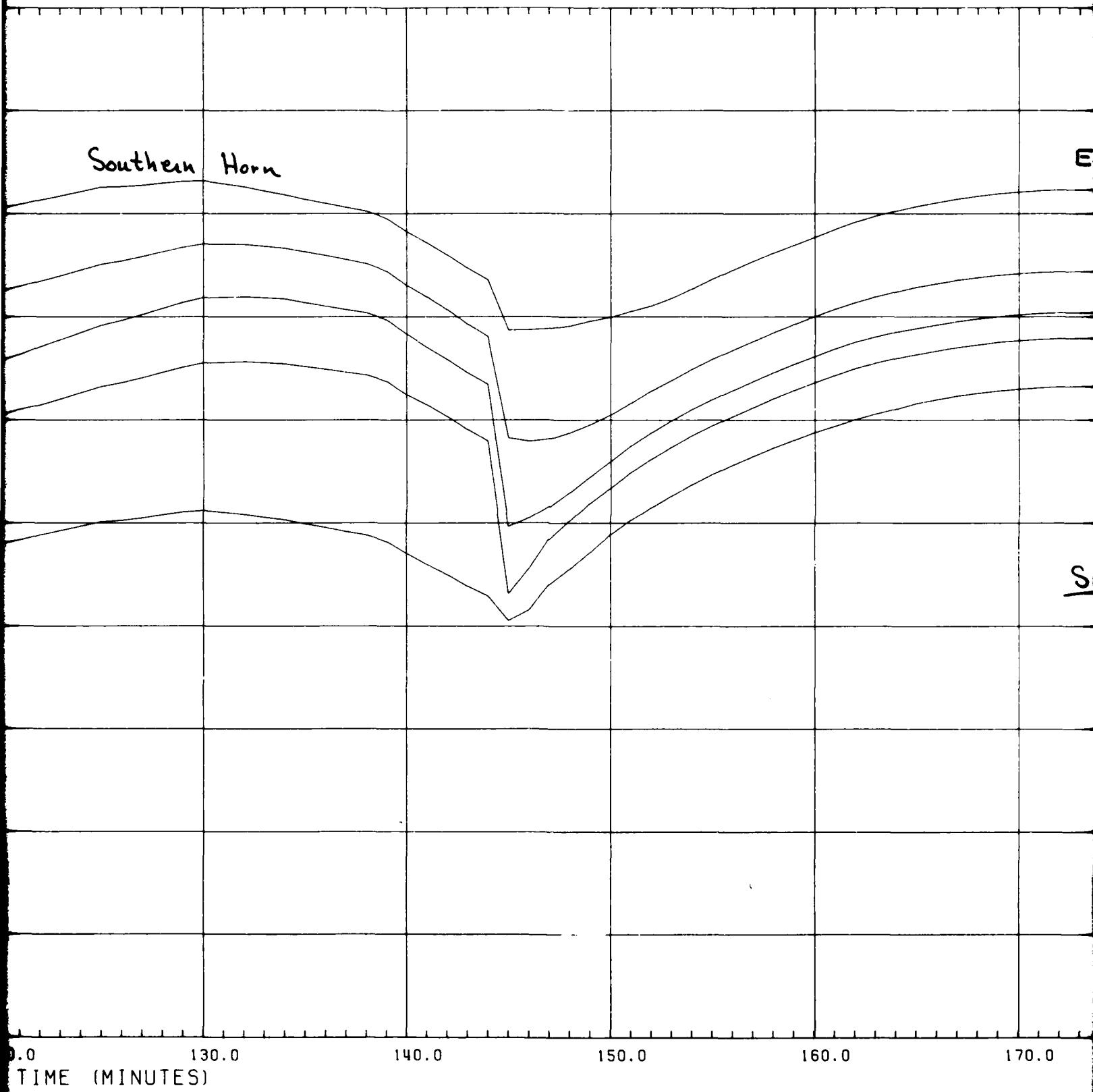
3

DOSE AT CENTER OF ALUMINUM SPHERE



4

OF ALUMINUM SPHERES



5

Equatorial Region

Northern

SAA

170.0

180.0

190.0

200.0

210.0

6

Figure 154

ORBIT: NAVELEX 5
60 DGR/6389-6389 KM

EPOCH: 1989.5

Northern Horn

MODELS:
FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AE17 L0
MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX
UN FACTORS: NOT APPLIED

STOP TIME ON TAPF = 8.933318

NASA-GSFC

210.0

220.0

230.0

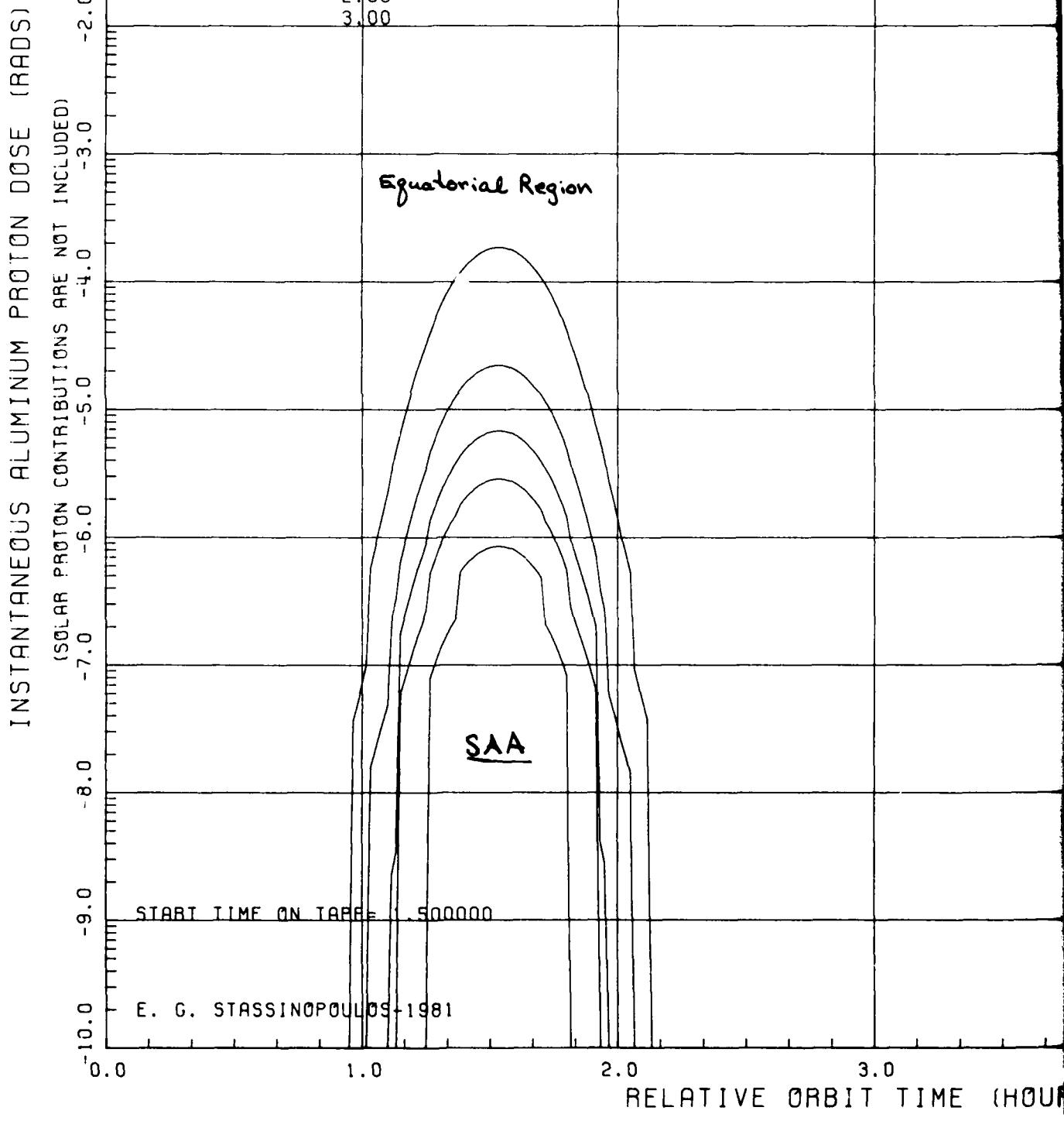
240.0

DOSE AT TRANSMISSION SURFACE OF FIN

(= DOSE IN SEMI-INFINITE ALUMINUM ME

OMNIDIRECTIONAL INCIDENCE

SHIELD THICKNESSES (GM/CM²)
 0.50
 1.00
 1.50
 2.00
 3.00



1
SURFACE OF FINITE ALUMINUM SLAB SHIELDS

2

ALUMINUM MEDIUM)

ORBIT: NAVELEX 6
60 DGR/10371-10371 KM

EPOCH: 1989.5

Figure 155

MODELS:
FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AE17-L0
MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Equatorial
Region

SAA

STOP TIME ON TAPF = 7.483318

NASA-GSFC

3.0

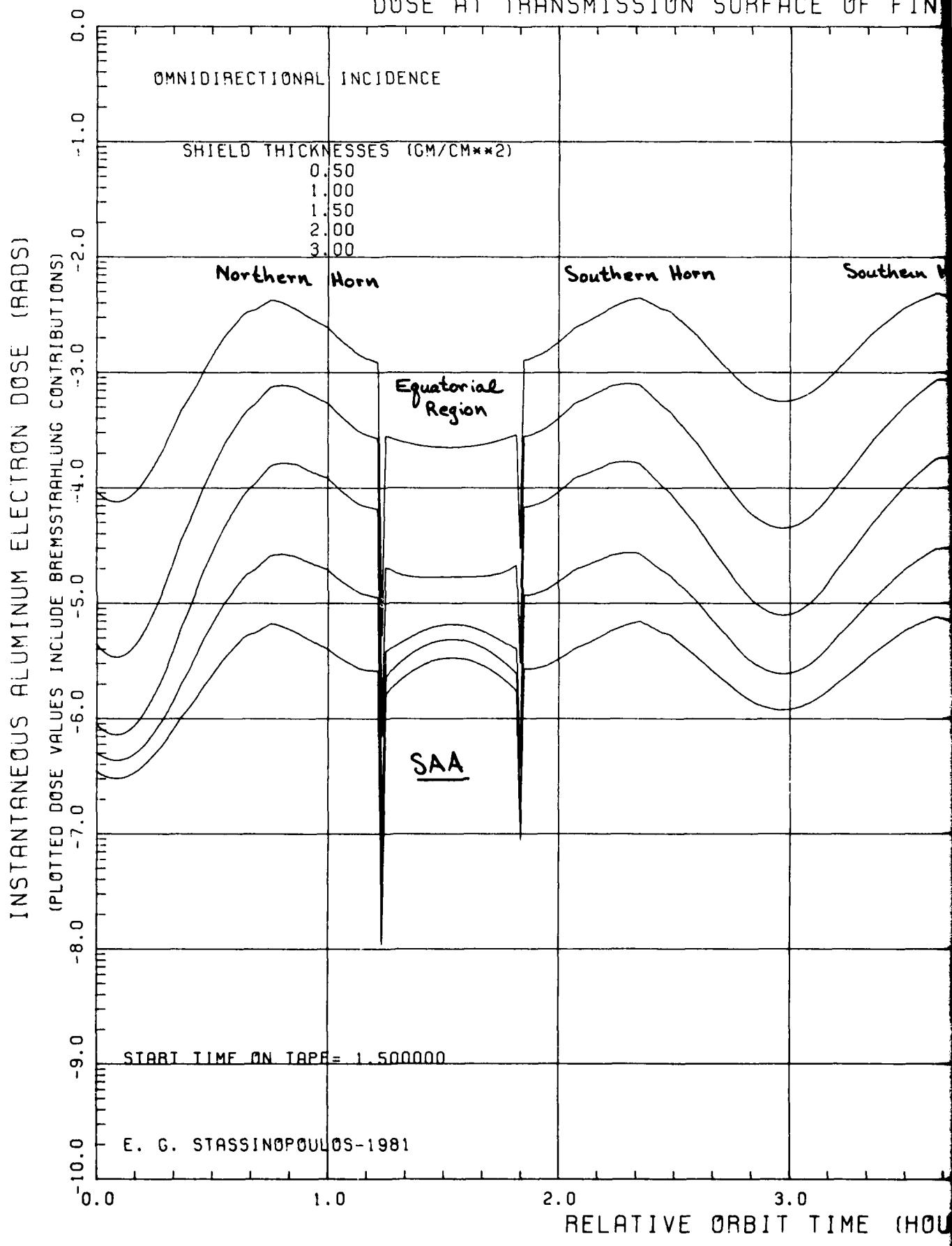
4.0

5.0

6.0

ORBIT TIME (HOURS)

DOSE AT TRANSMISSION SURFACE OF FIN



N SURFACE OF FINITE ALUMINUM SLAB SHIELDS

Figure 156

ORBIT: NAVELEX 6
60 DGR/10371-10371 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AE17-L0

MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern Horn

Southern Horn
Equatorial Region

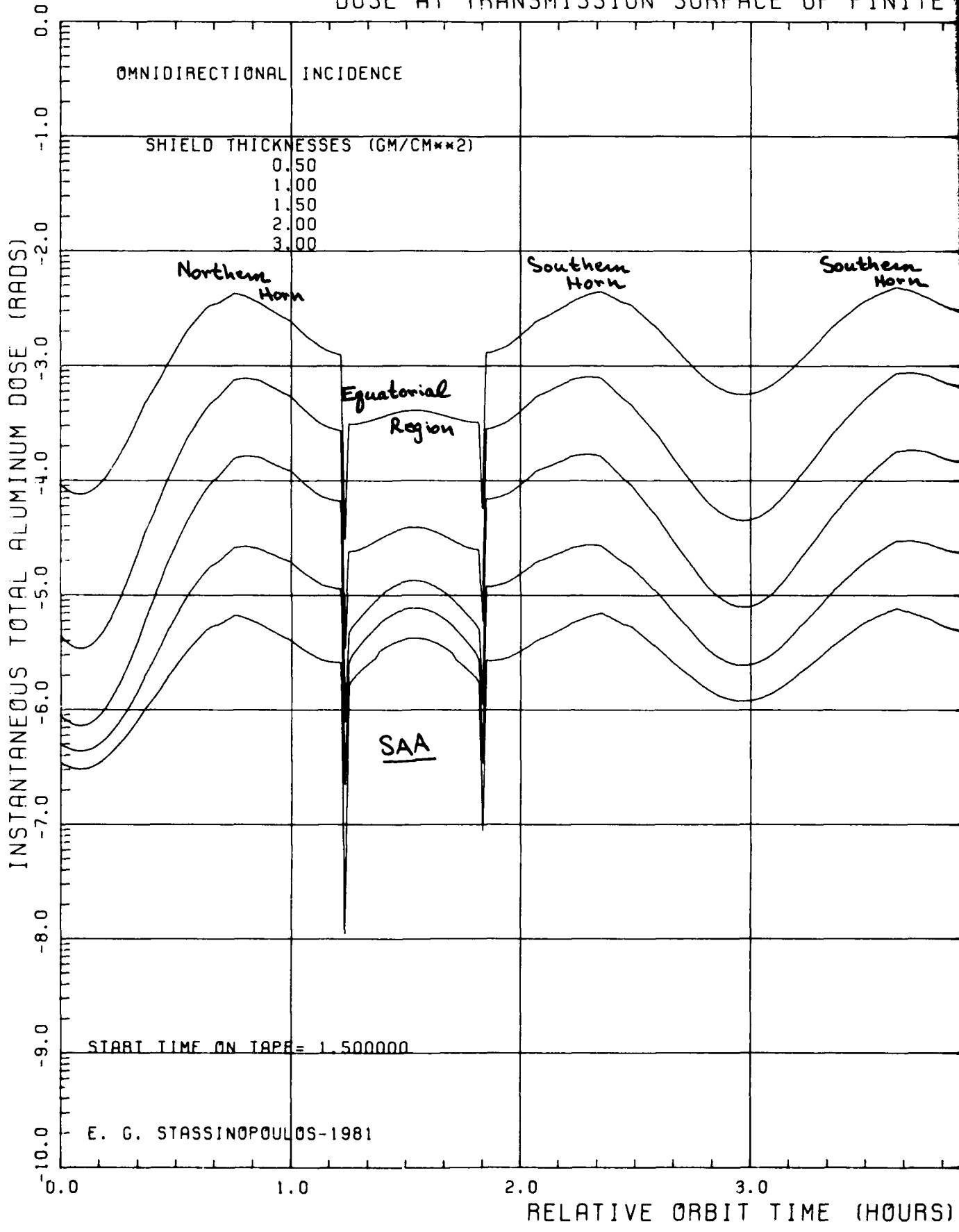
SAA

STOP TIME ON TAPE = 7.483318

NASA-GSFC

3.0 4.0 5.0 6.0
ORBIT TIME (HOURS)

DOSE AT TRANSMISSION SURFACE OF FINITE



SURFACE OF FINITE ALUMINUM SLAB SHIELDS

Figure 157

ORBIT: NAVELEX 6
60 DGR/10371-10371 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AE17 LO

MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Northern Horn

Southern Horn

Equatorial Region

SAA

STOP TIME ON TAPE = 7.483318

NASA-GSFC

3.0

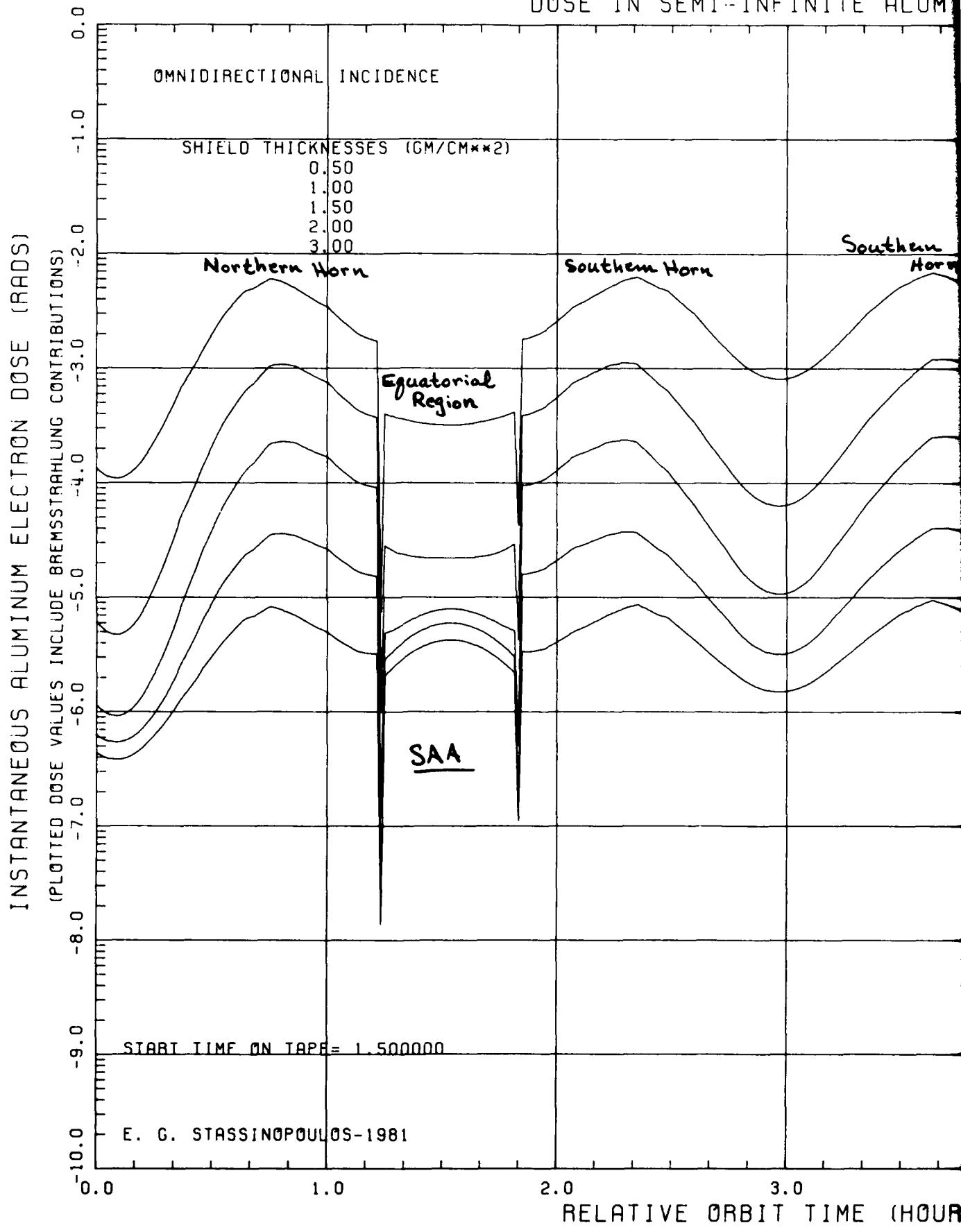
4.0

5.0

6.0

ORBIT TIME (HOURS)

DOSE IN SEMI-INFINITE ALUM



I-INFINITE ALUMINUM MEDIUM

Figure 158

ORBIT: NAVELEX 5
60 DGR/10371-10371 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-L0

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Southern
Horn

Northern
Horn

Equatorial
Region

SAA

STOP TIME ON TAPF = 7.483318

NASA-GSFC

3.0

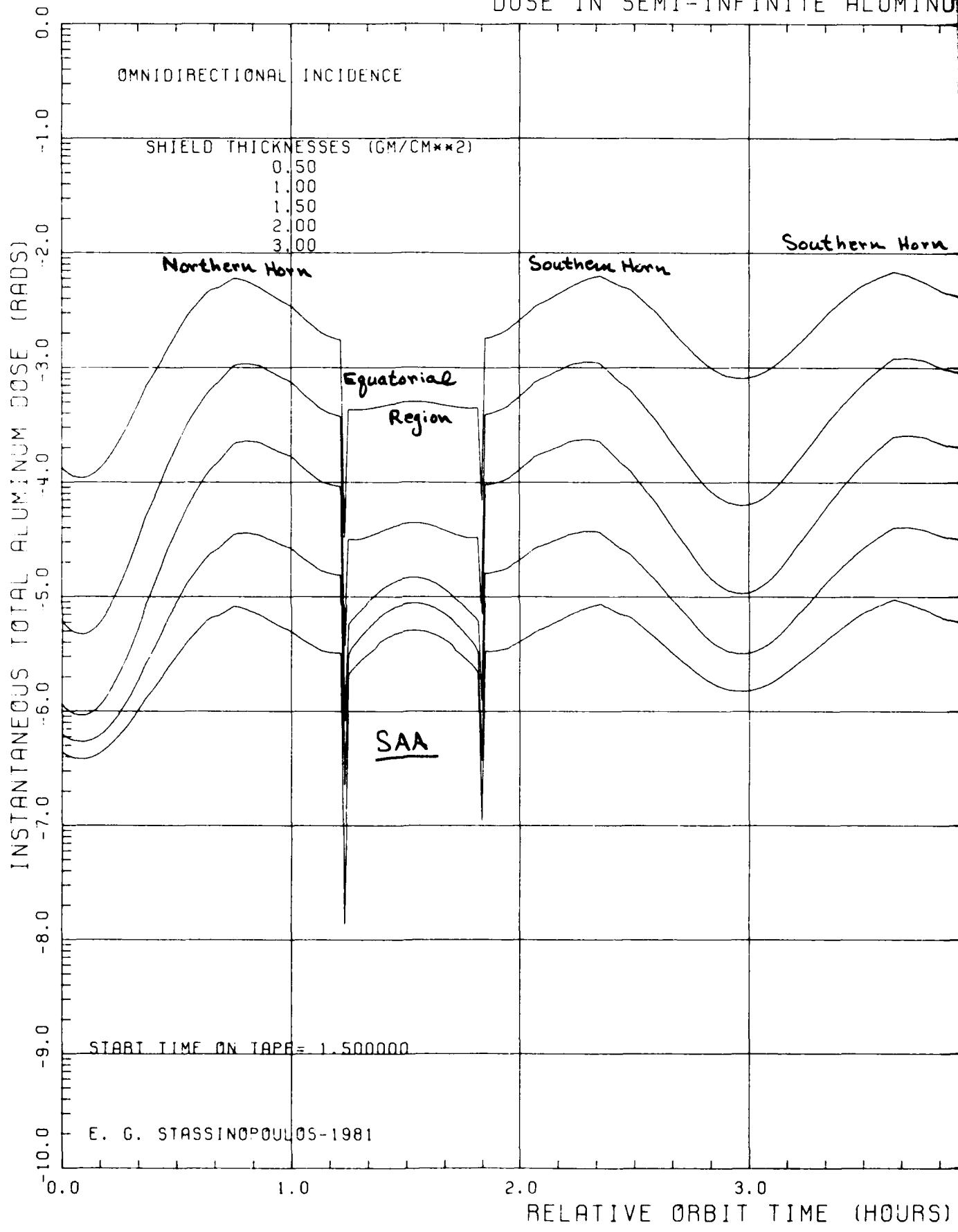
4.0

5.0

6.0

ORBIT TIME (HOURS)

DOSE IN SEMI-INFINITE ALUMINU



INFINITE ALUMINUM MEDIUM

Figure 159

ORBIT: NAVELEX 6
60 DGR/10371-10371 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AES
OUTER ZN ELEC: AEI7 LO
MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

Southern Horn

Northern Horn

Equatorial
Region

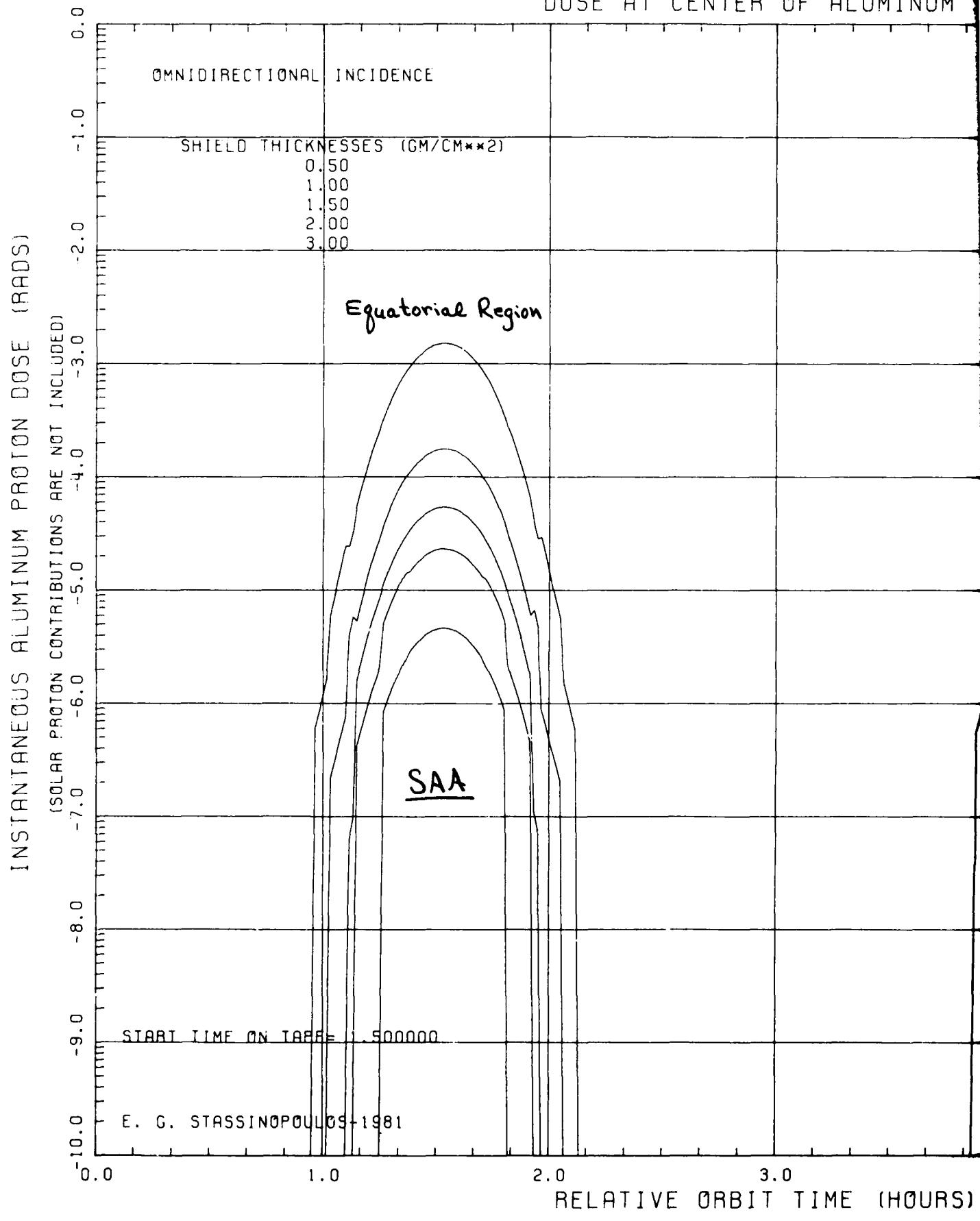
SAA

STOP TIME ON TAPE = 7.483318

NASA-GSFC

3.0 4.0 5.0 6.0
DT TIME (HOURS)

DOSE AT CENTER OF ALUMINUM



ER OF ALUMINUM SPHERES

Figure 160

ORBIT: NAVELEX 6
60 DGR/10371-10371 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17-L0

MISSION DURATION: 60.00 M0

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Equatorial Region

SAA

STOP TIME ON TPF = 7.483318

NASA-GSFC

3.0

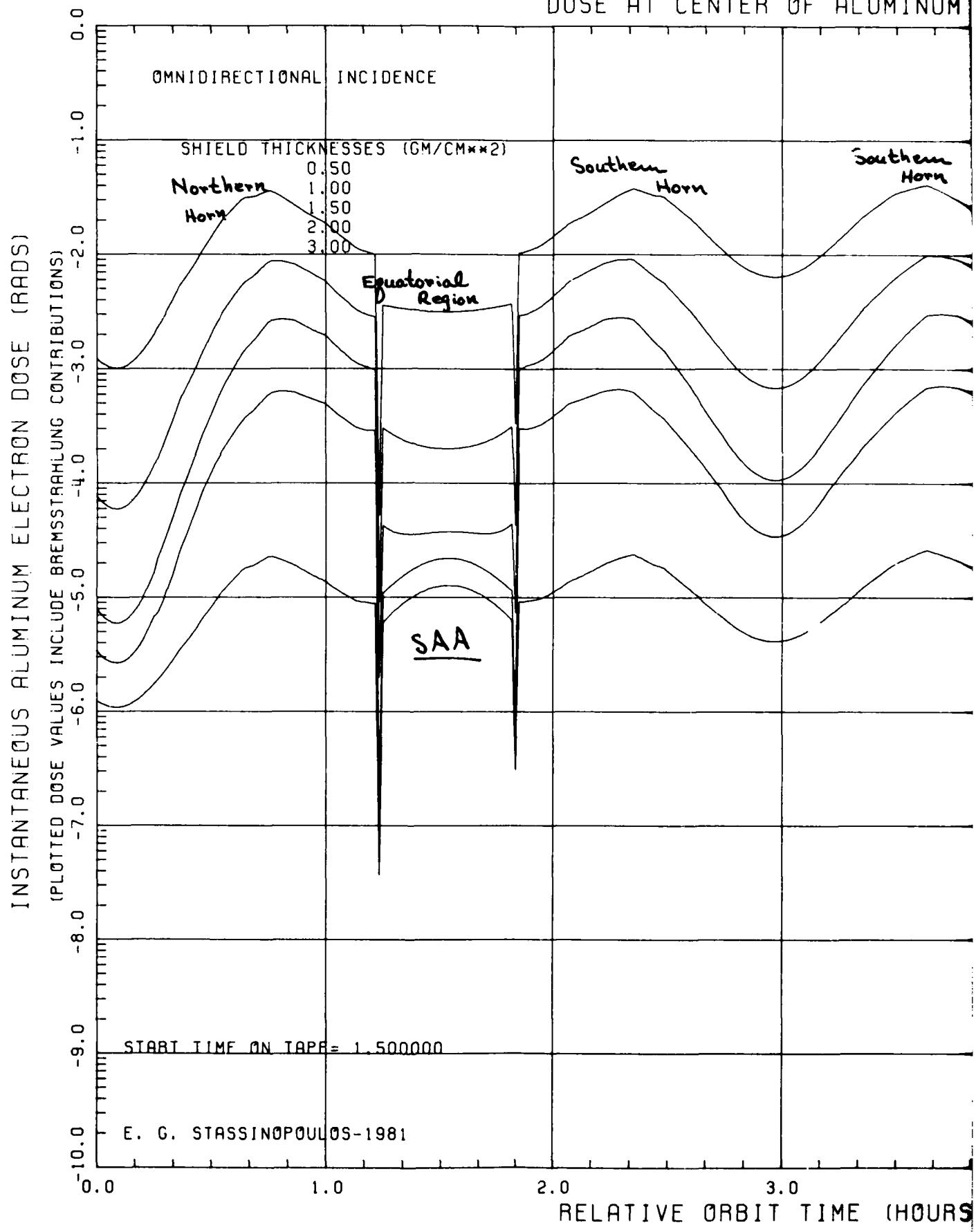
4.0

5.0

6.0

BIT TIME (HOURS)

DOSE AT CENTER OF ALUMINUM



TER OF ALUMINUM SPHERES

Figure 161

ORBIT: NAVELEX 6
60 DGR/10371-10371 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75

TRAPPED PROTONS: AP8

INNER ZN ELEC: AE6

OUTER ZN ELEC: AE17 LG

MISSION DURATION: 60.00 MO

EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Southern Horn

Northern Horn

Equatorial Region

SAA

STOP TIME ON TAPF = 7.483318

NASA-GSFC

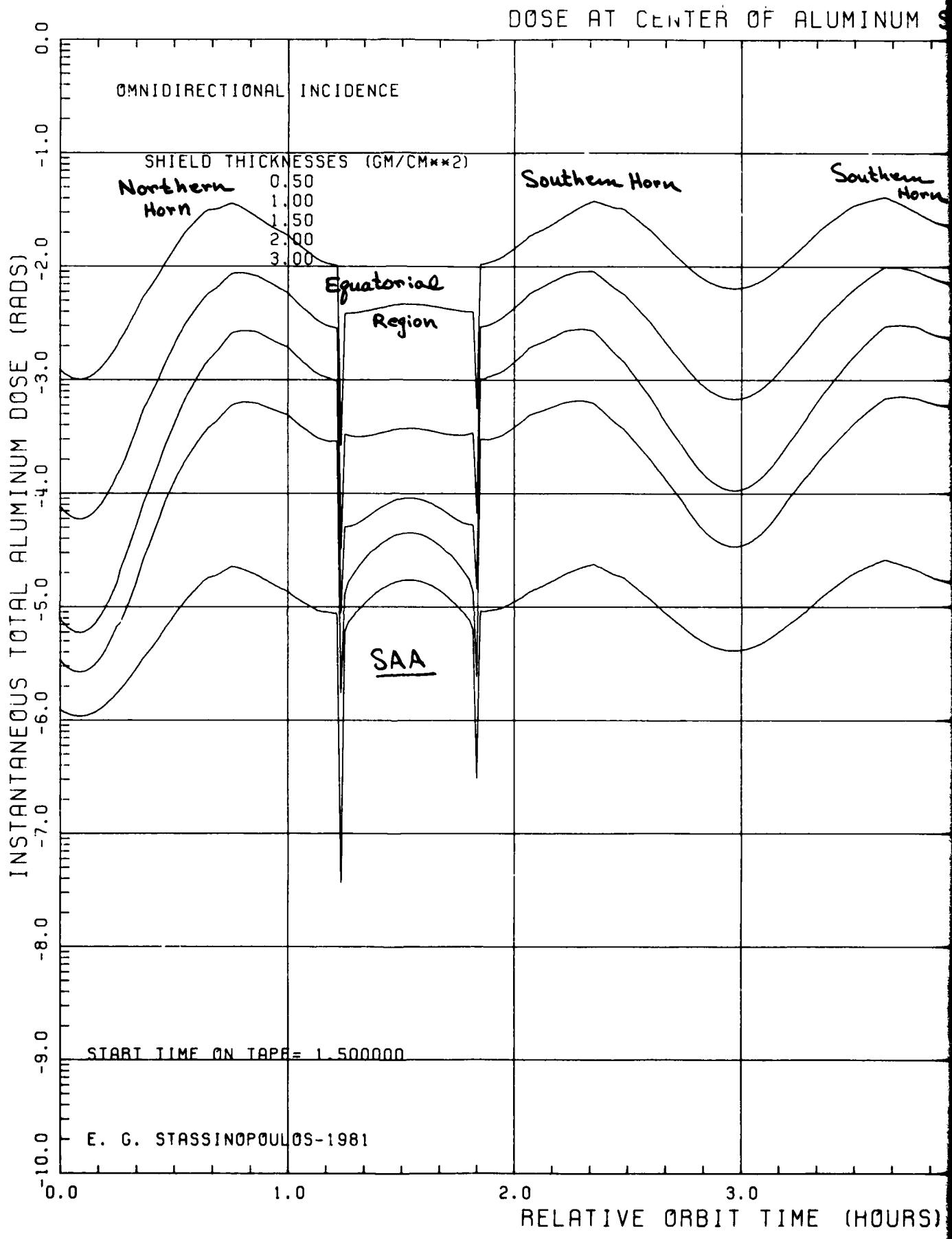
3.0

4.0

5.0

6.0

ORBIT TIME (HOURS)



OF ALUMINUM SPHERES

Figure 162

ORBIT: NAVELEX 6
60 DGR/10371-10371 KM

EPOCH: 1989.5

MODELS:

FIELD: BARR/75
TRAPPED PROTONS: AP8
INNER ZN ELEC: AE6
OUTER ZN ELEC: AE17-L0
MISSION DURATION: 60.00 MO
EVALUATION PHASE: SOLAR MAX

UN FACTORS: NOT APPLIED

Southern Horn

Northern Horn

Equatorial

Region

SAA

STOP TIME ON TAPF = 7.483318

NASA-GSFC

3.0 4.0 5.0 6.0
T TIME (HOURS)

